



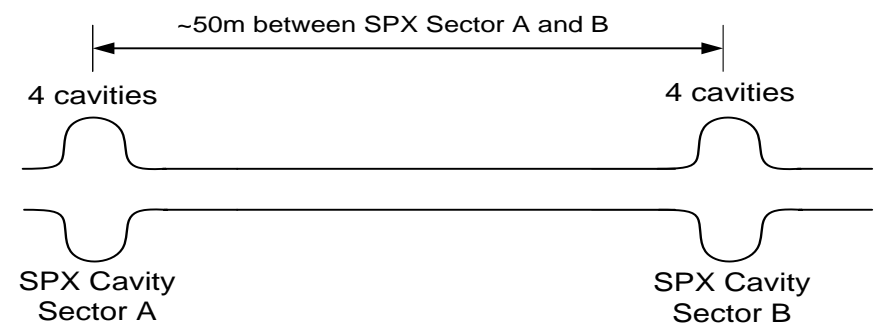
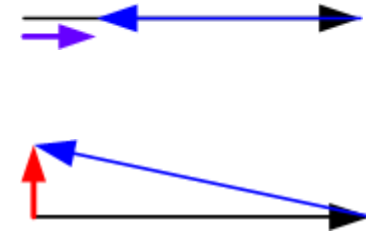
SPX Workshop

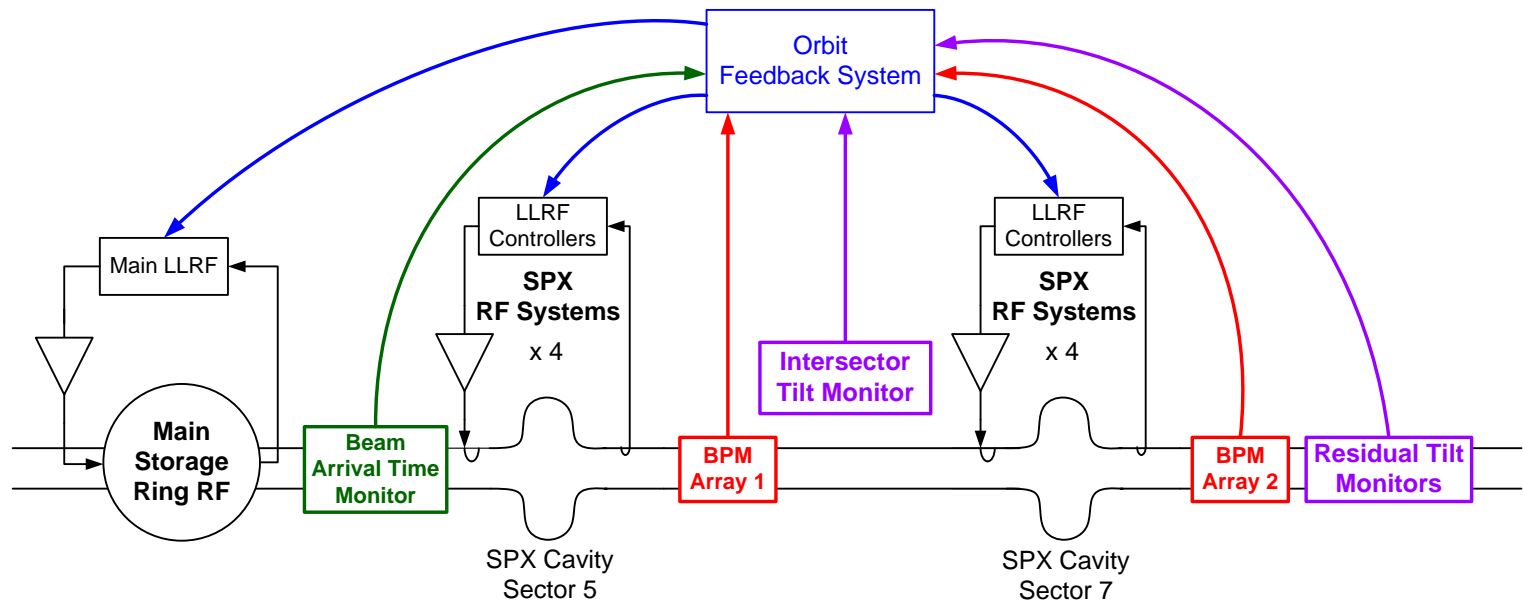
Prelude to Discussion on Error Budgets

July 18, 2011
T. Berenc

Performance Requirements

	Specification name	Rms Value	Driving requirement
Common Mode	Common-mode voltage variation	$< 1\%$	Keep intensity and pulse length variation under 1% rms
	Common-mode phase variation	$< 4.0^\circ$	Keep intensity variation under 1% rms
Differential Mode	Voltage mismatch between sectors	$< 1.1\%$	Keep rms emittance variation under 10% of nominal 40 pm
	Phase error between sectors	$< 0.18^\circ$	Keep rms beam motion under 10% of beam size/divergence





BPM Array 1: sets phase of Sector 5

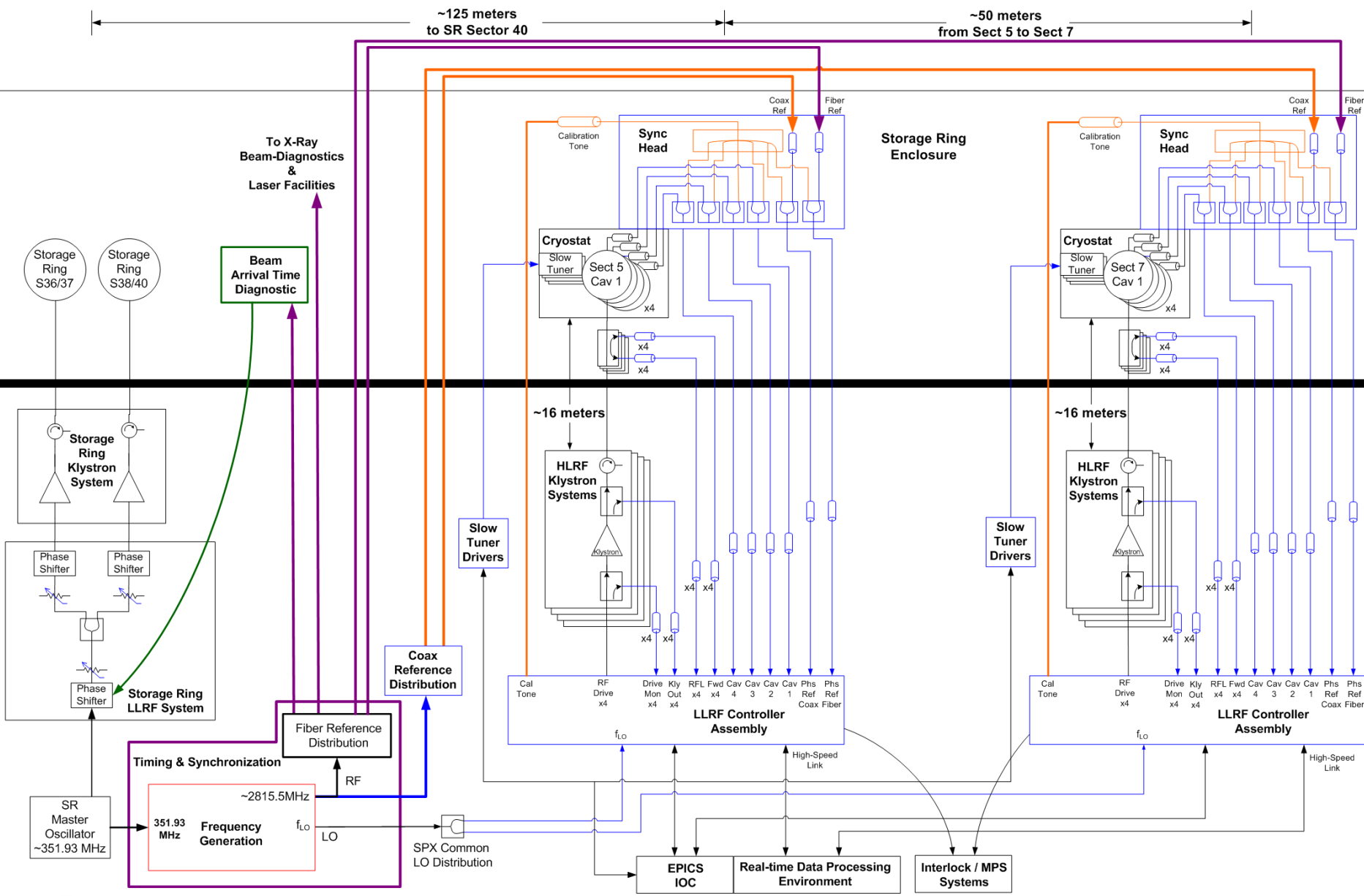
BPM Array 2: sets phase of Sector 7

Intersector Tilt Monitor: sets amplitude of Sector 5

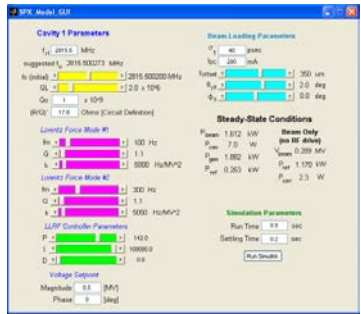
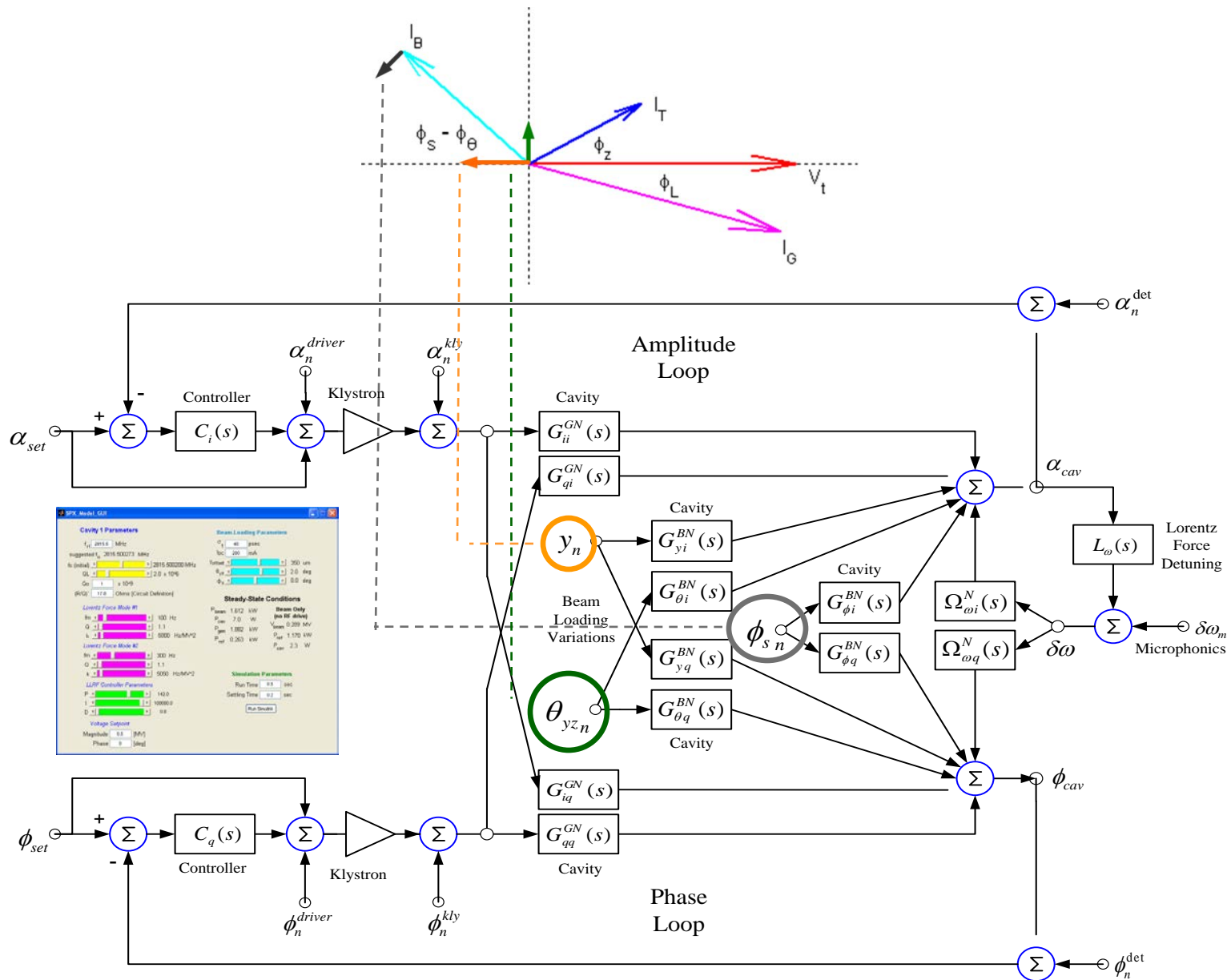
Residual Tilt Monitors: sets amplitude of Sector 7

Beam Arrival Time Monitor: sets phase of Main Storage Ring RF

Production System Concept (2 Sectors, 4 cav/sector)

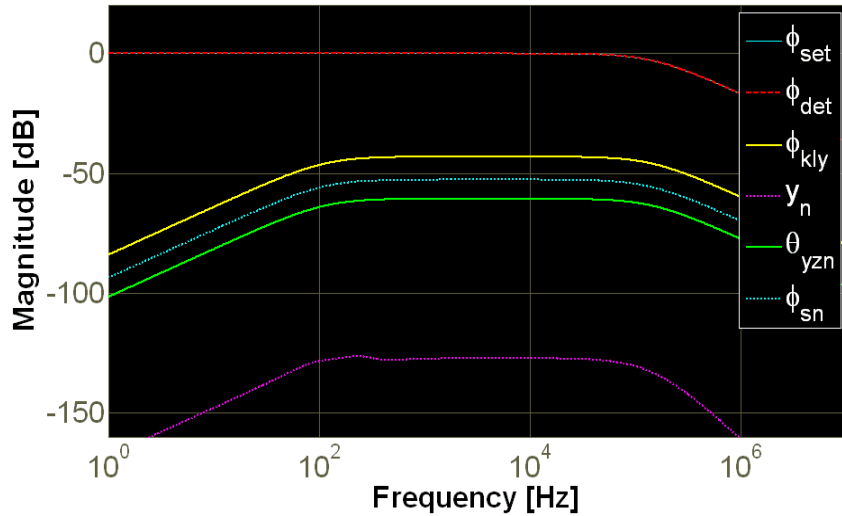


Dynamic small signal model for individual crab cavity

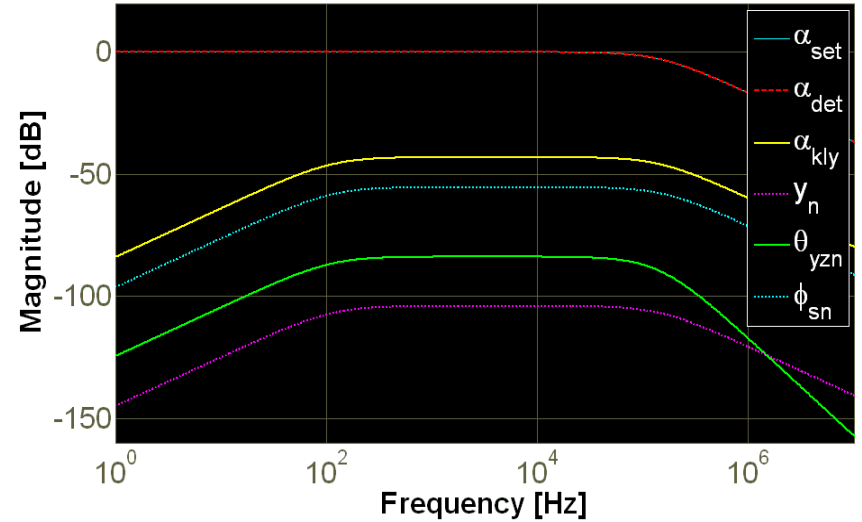


- Example Transfer Functions from single cavity small signal model

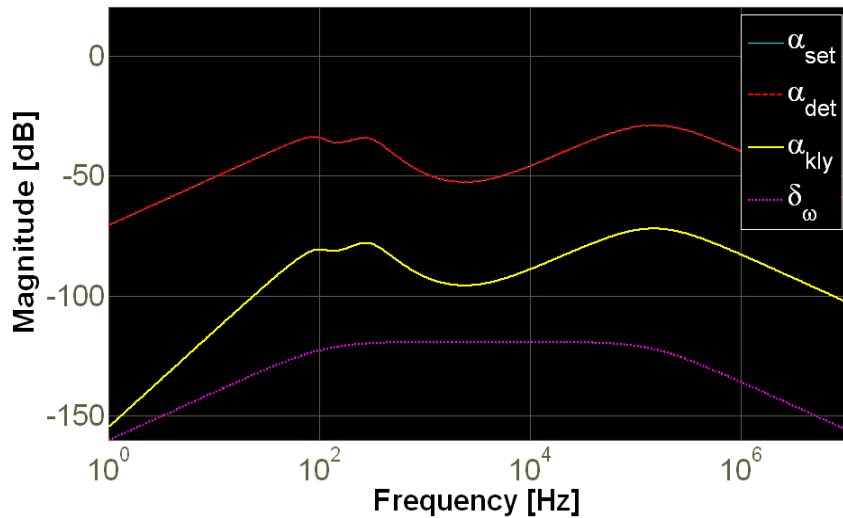
Phase Transfer Functions



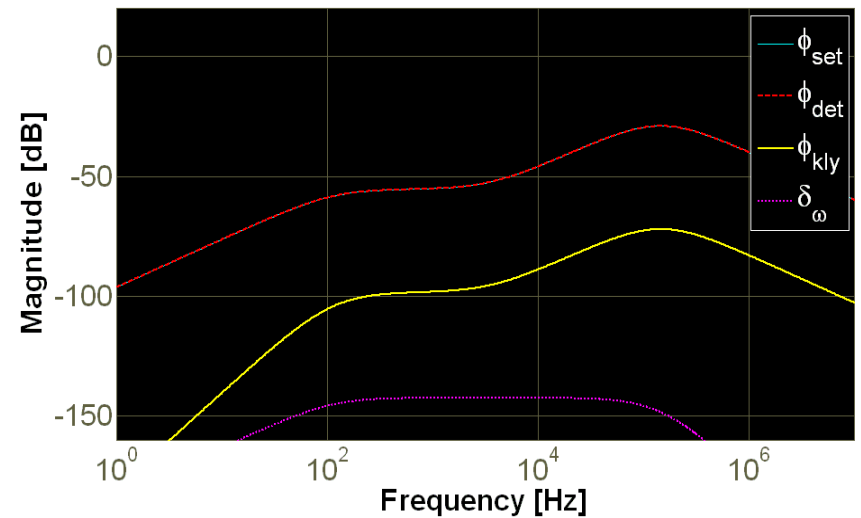
Amplitude Transfer Functions



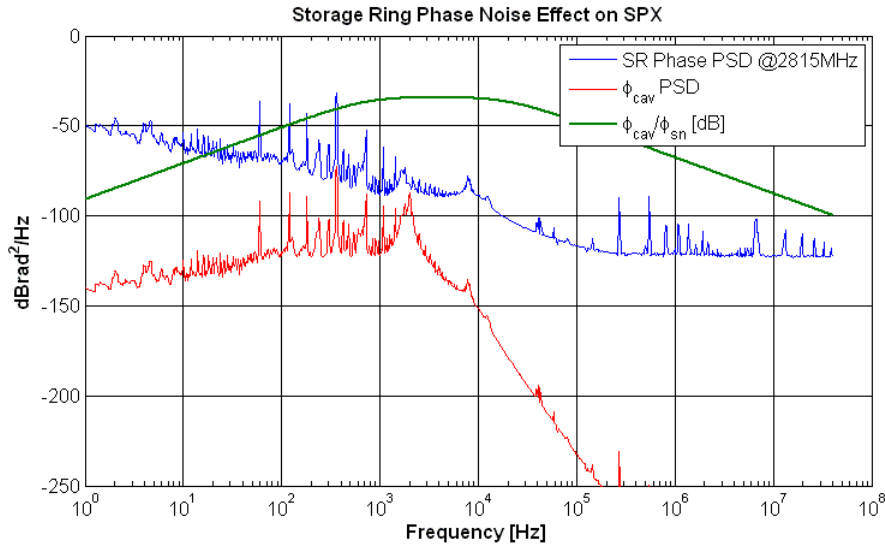
Phase Transfer Functions



Amplitude Transfer Functions



Motivation for Cavity Electrical Alignment Adjust

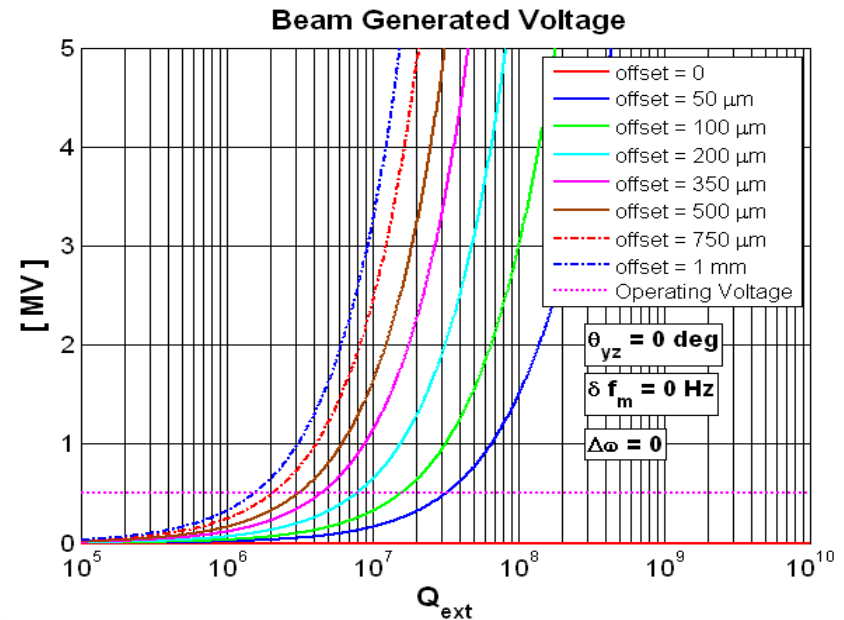
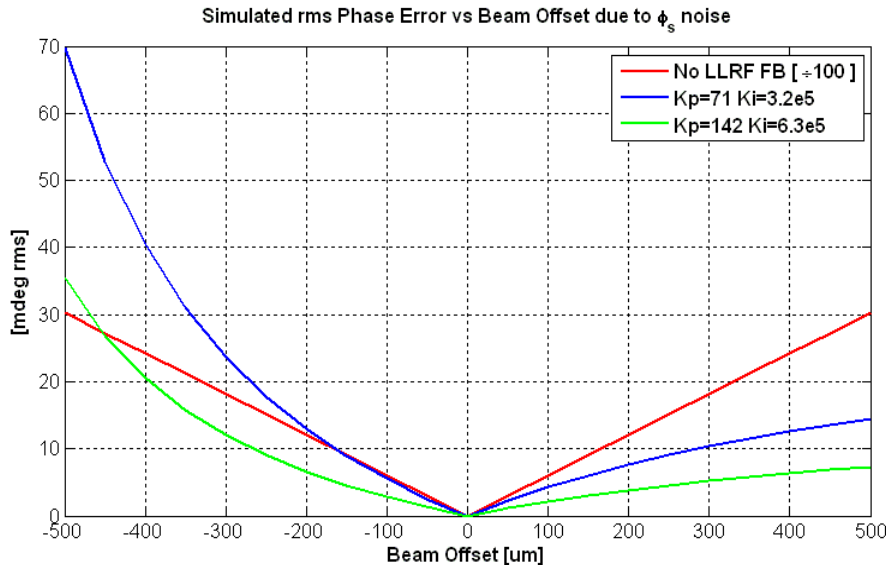


Beam Loading is proportional to offset
 Cavity-to-cavity alignment errors cause differential beam-loading that will lead to differential phase noise

Standard cavity-to-cavity alignment = 500 μ m
 Beyond APS-U, 4MV => 0.07deg spec

Need measurements of beam jitter at 150mA
 Means to reduce effect:

improve cavity alignment, go to lower QL,
 reduce Storage Ring AM & PM noise



Initial Error Budgeting

$$\sigma_{tot} = \sqrt{\sigma_1^2 + \sigma_2^2 + \dots}$$

$$\sigma_n^2 = \int_{f_{min}}^{f_{max}} S_n(f) |H_n(f)|^2 df$$

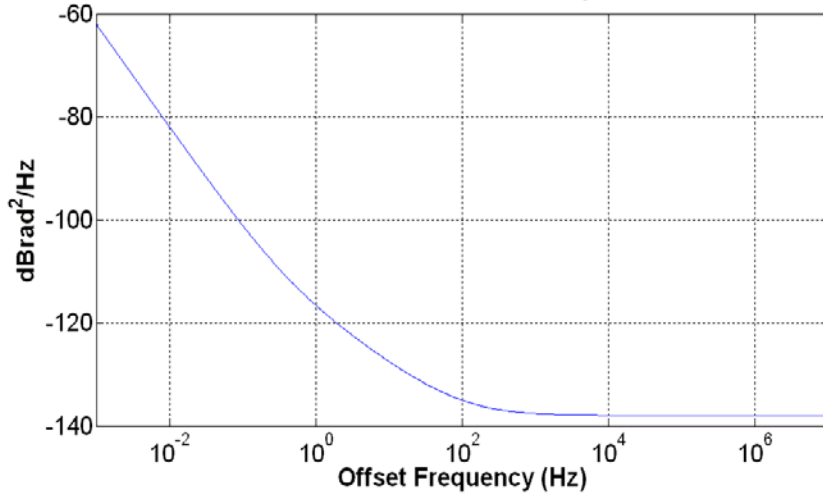
		PHASE				AMPLITUDE			
		Common Mode [deg rms]		Differential [deg rms]		Common Mode [% rms]		Differential [% rms]	
		4		0.18		1		1.1	
Total Budget		2.31	3.27	0.10	0.15	0.58	0.82	0.64	0.90
Error/Noise Source ^[4]	< 10Hz [deg rms]	[10Hz-200kHz] [deg rms]	< 10Hz [deg rms]	[10Hz-200kHz] [deg rms]	< 10Hz [% rms]	[10Hz-200kHz] [% rms]	< 10Hz [% rms]	[10Hz-200kHz] [% rms]	
1	SPX Frequency Generation Chassis		0.5097		0.039		0.226		0.249
2	Phase Ref. Distribution		0.5097		0.039				
3	LO Distribution		0.5097			0.226		0.249	
4	LLRF Controller		0.5097		0.040		0.226		0.249
5	Cavity Field Probe Cabling		0.5097		0.039		0.226		0.249
6	Klystron + Driver Amp		0.5097		0.040		0.226		0.249
7	Microphonics		0.5097		0.039		0.226		0.249
8	Beam-Loading Offset Noise		0.5097		0.039		0.226		0.249
9	Beam-Loading Tilt Noise		0.5097		0.039		0.226		0.249
10	Storage Ring Beam Jitter		2.7		0.039		0.226		0.249
11	Beam-Loading Synchronous Phase Noise (other than Storage Ring beam jitter ??)		0.5097		0.039		0.226		0.249
12	Beam Arrival Time Feedback Process		0.5097		0.039		0.226		0.249
13	AM-to-PM Cross Modulation		0.5097		0.039				
14	PM-to-AM Cross Modulation						0.226		0.249
15	Orbit Feedback Process [outside SPX zone] (differential phase correction)				0.039				
16	Orbit Feedback Process [inside SPX zone] (common mode phase correction)		0.5097						
17	Residual Tilt Feedback [outside SPX zone] long-term differential amplitude correction								0.249
18	Intersector Tilt Feedback Process [inside SPX zone] common mode amplitude set-point						0.226		
# of processes		14		14		13		13	

Example Calculation for a Single Line Item

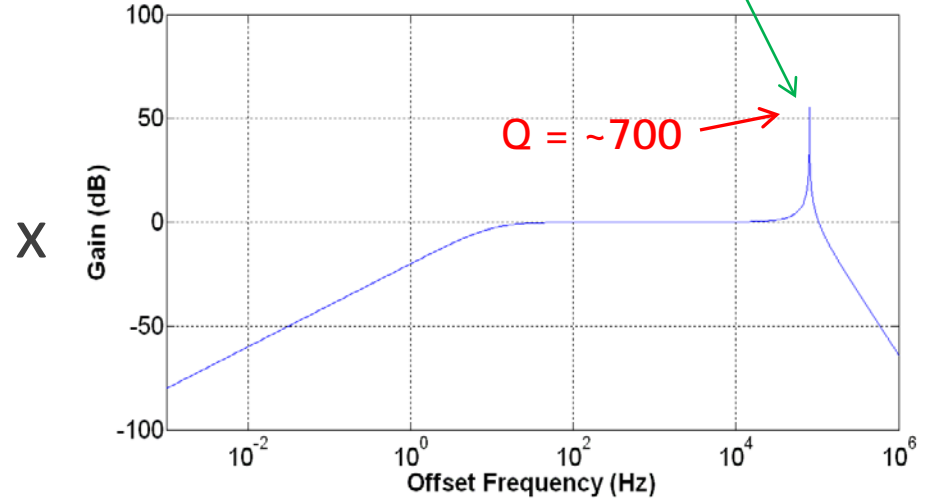
$$S_{\phi}^{cav\ effective}(f) = S_{\phi}^{LLRF} \cdot |N_{RTFB}(s) \cdot \beta_N(s)|^2$$

Beam Orbit Transfer Function

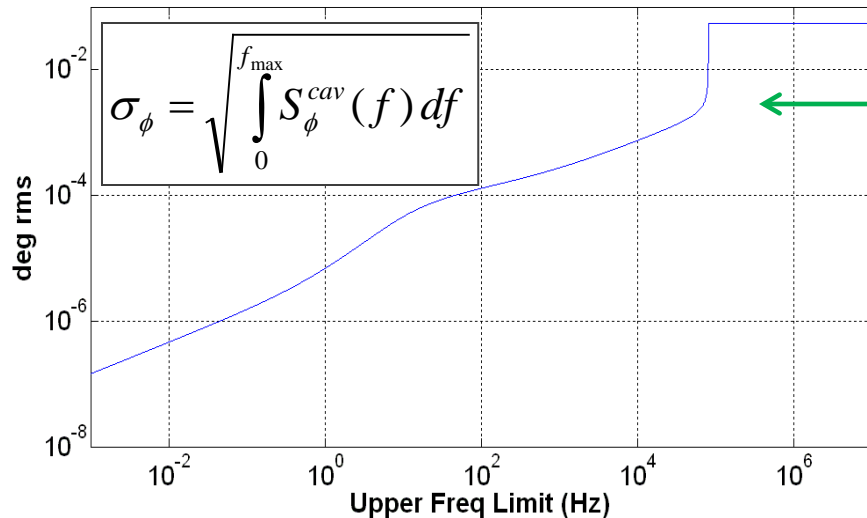
LLRF Detector Phase Noise Spectrum



Effective LLRF Detector Noise Transfer Function



Cumulative Integral of Effective Phase Noise



0.054 deg RMS w Betatron Tune

0.0034 deg RMS w/o Betatron Tune

Expect lower Q when including existing transverse feedback system

Will study the need for:
narrow-band beam-based feedback near the betatron resonance

Potential Topics To Discuss...

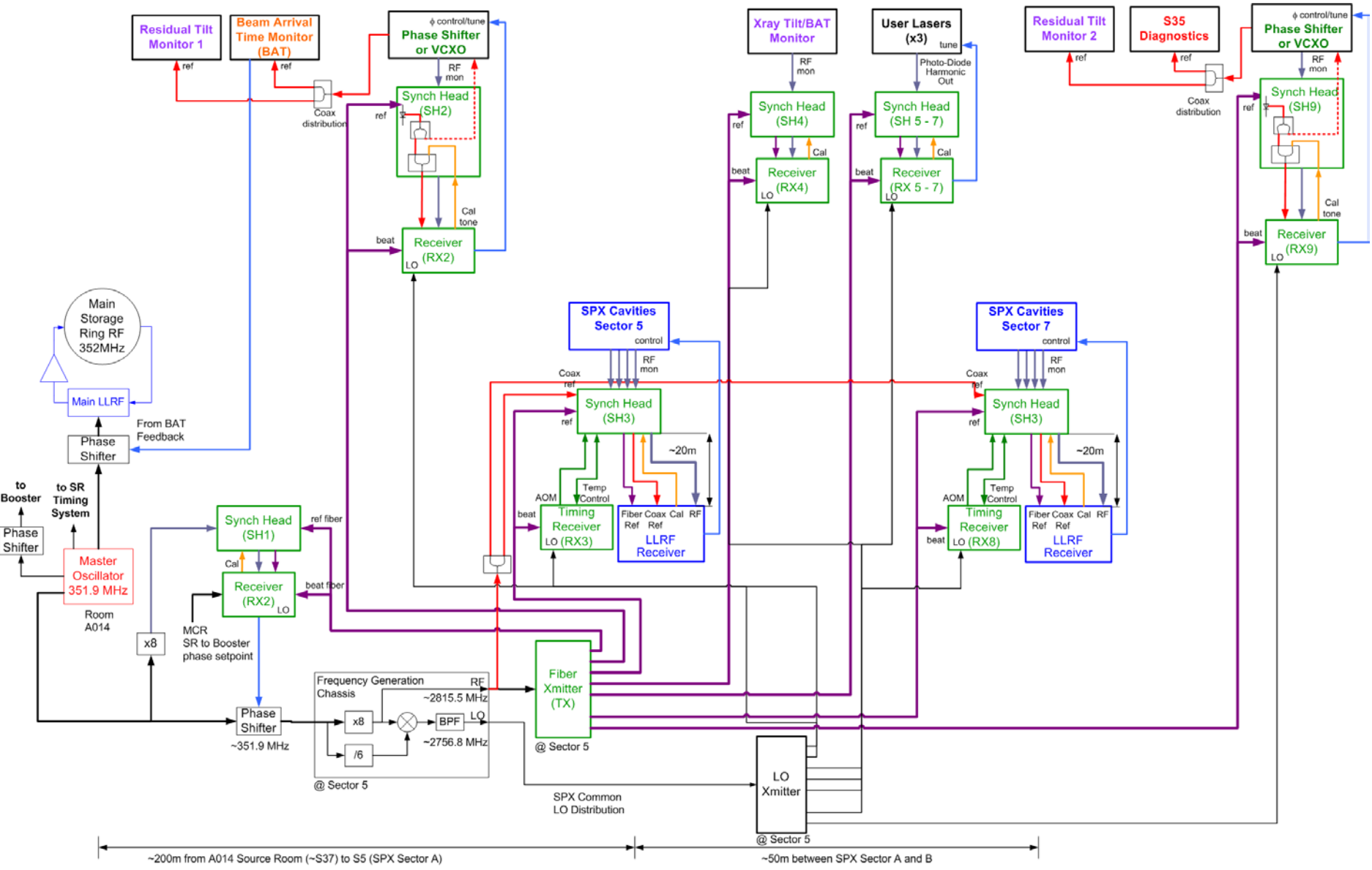
- Identify additional processes and noise sources
- Ways to a practical allocation of error budgets across frequency bands and systems
- Cavity alignment tolerance
- Interaction with orbit feedback and influence of bunch by bunch feedback on betatron tune Q

Blank Worksheet

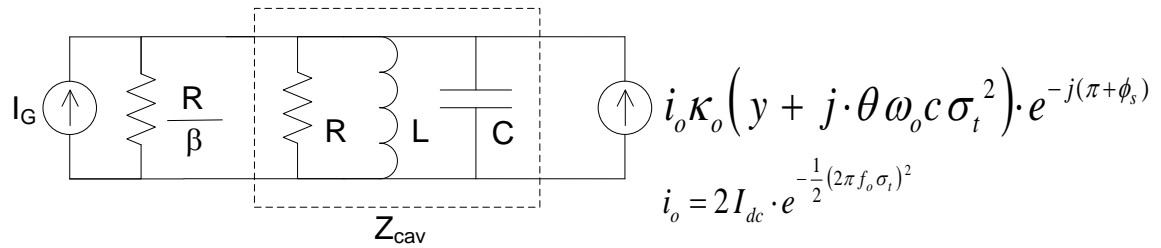
		PHASE				AMPLITUDE			
		Common Mode [deg rms]		Differential [deg rms]		Common Mode [% rms]		Differential [% rms]	
Total Budget		4		0.18		1		1.1	
Error/Noise Source ^[4]		< 10Hz [deg rms]	[10Hz-200kHz] [deg rms]	< 10Hz [deg rms]	[10Hz-200kHz] [deg rms]	< 10Hz [% rms]	[10Hz-200kHz] [% rms]	< 10Hz [% rms]	[10Hz-200kHz] [% rms]
1	SPX Frequency Generation Chassis								
2	Phase Ref. Distribution								
3	LO Distribution								
4	LLRF Controller								
5	Cavity Field Probe Cabling								
6	Klystron + Driver Amp								
7	Microphonics								
8	Beam-Loading Offset Noise								
9	Beam-Loading Tilt Noise								
10	Storage Ring Beam Jitter								
11	Beam-Loading Synchronous Phase Noise (other than Storage Ring beam jitter ??)								
12	Beam Arrival Time Feedback Process								
13	AM-to-PM Cross Modulation					N/A	N/A	N/A	N/A
14	PM-to-AM Cross Modulation	N/A		N/A					
15	Orbit Feedback Process [outside SPX zone] (differential phase correction)	N/A				N/A	N/A		
16	Orbit Feedback Process [inside SPX zone] (common mode phase correction)					N/A	N/A		
17	Residual Tilt Feedback [outside SPX zone] long-term differential amplitude correction	N/A		N/A		N/A			
18	Intersector Tilt Feedback Process [inside SPX zone] common mode amplitude set-point	N/A		N/A					
	# of processes		14		14		13		13

Backup Slides

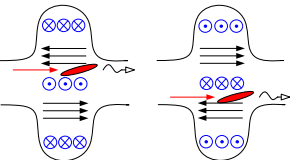




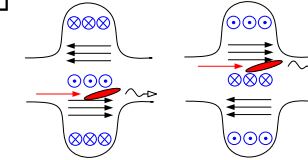
Deflecting Cavity Beam Loading



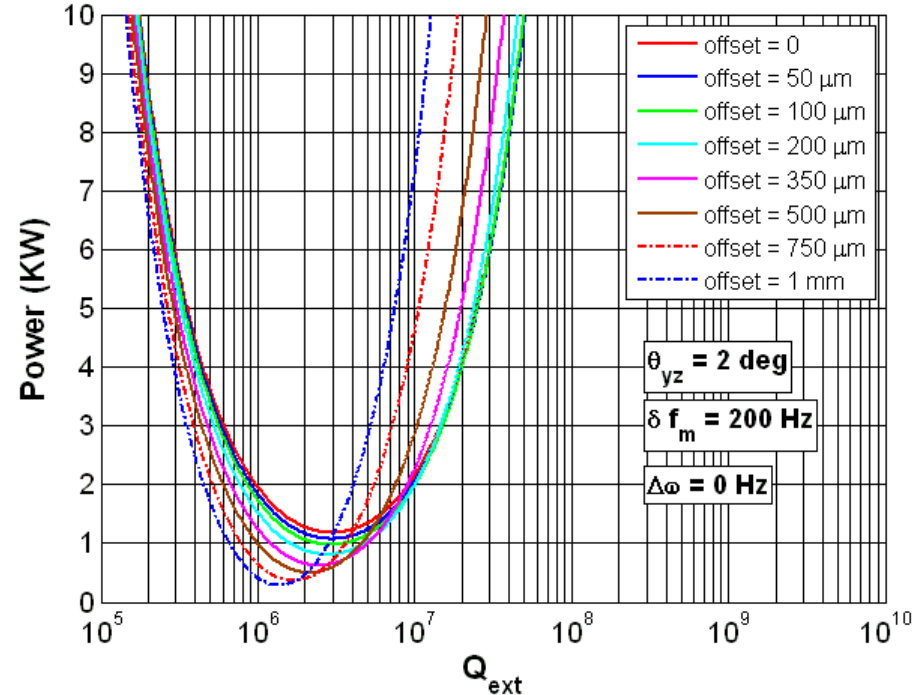
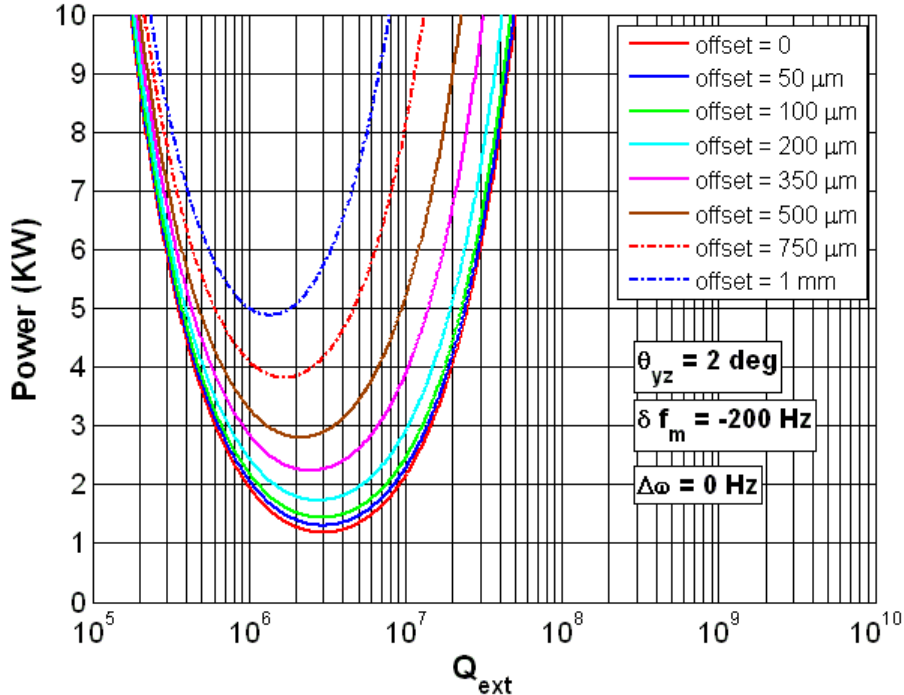
$$P_s^+ = \frac{V_t^2}{8\beta(R/Q)'Q_o} \cdot \left[\left(\beta + 1 + \frac{P_B}{P_{cav}} \right)^2 + \left(2Q_o \frac{\Delta f + \delta f_m}{f_r} + \frac{P_B}{P_{cav}} \tan \phi_s \right)^2 \right]$$



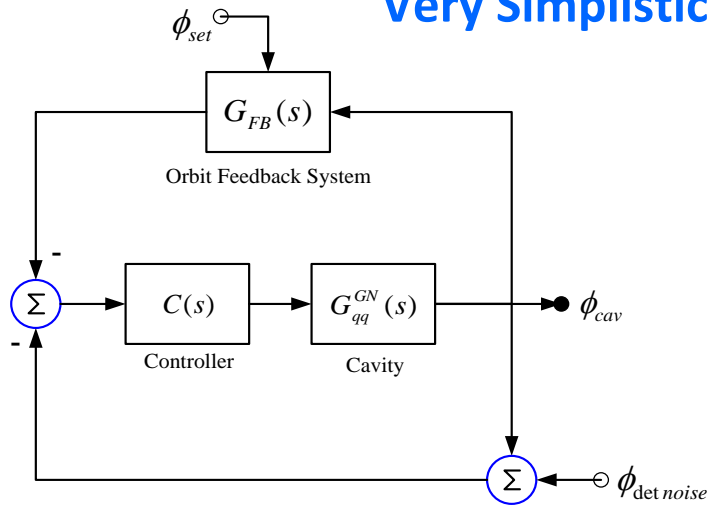
$V_t \cdot y > 0$



$V_t \cdot y < 0$



Very Simplistic First Order Orbit Feedback concept

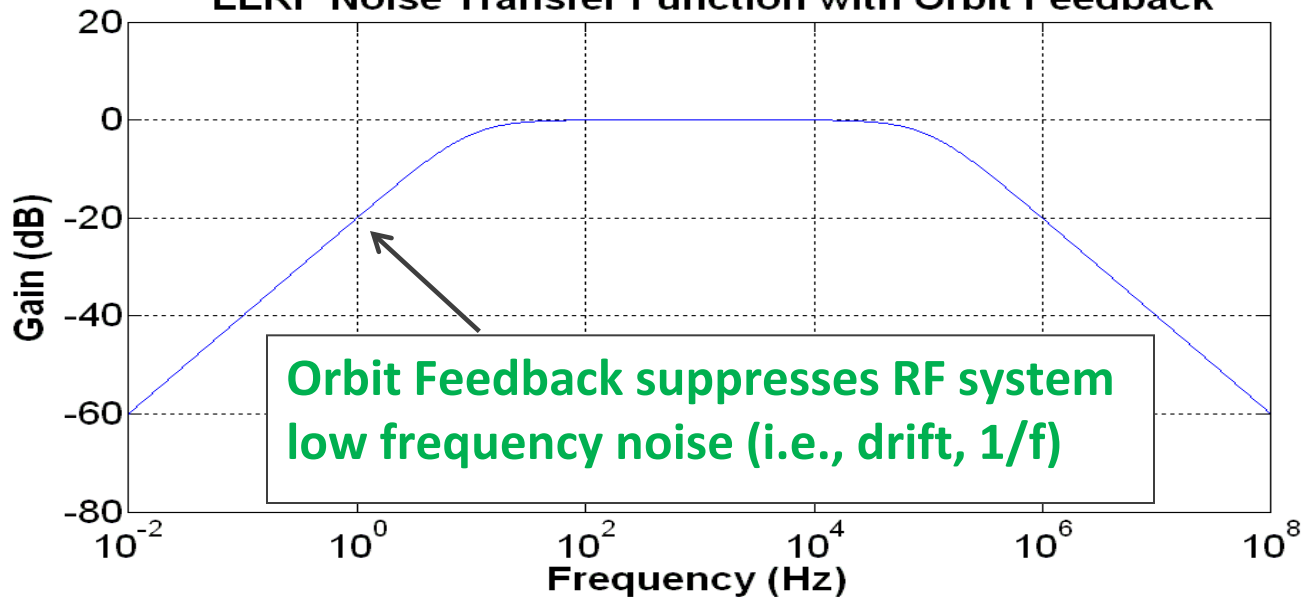


Assume:
$$G_{FB}(s) = \frac{K_p^{RTFB} \sigma_{RTFB}}{s}$$

$$N_{FB}(s) = \frac{\phi_{cav}(s)}{\phi_{detnoise}(s)} = \frac{C(s)G_{qq}^{GN}(s)}{1 + C(s)G_{qq}^{GN}(s)[1 + G_{FB}(s)]}$$

$$= \frac{K_p \sigma_{cav} s}{s^2 + K_p \sigma_{cav} s + K_p^{RTFB} K_p \sigma_{RTFB} \sigma_{cav}}$$

LLRF Noise Transfer Function with Orbit Feedback

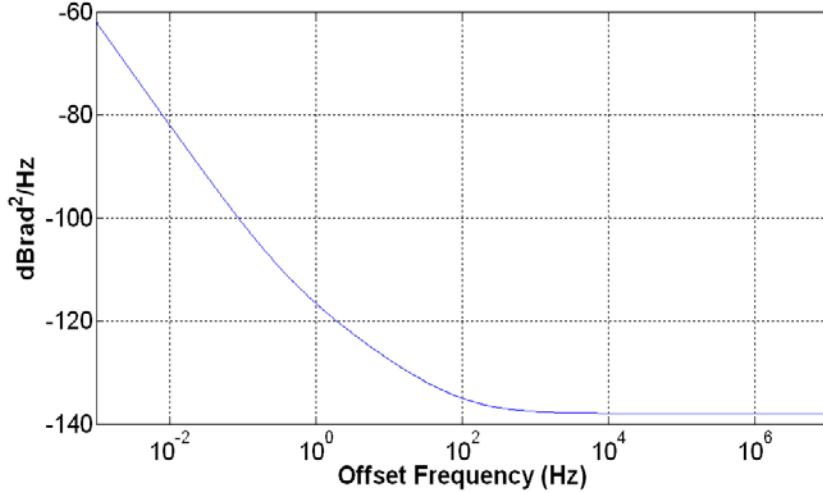


How to achieve 0.18° rms Differential Phase ??

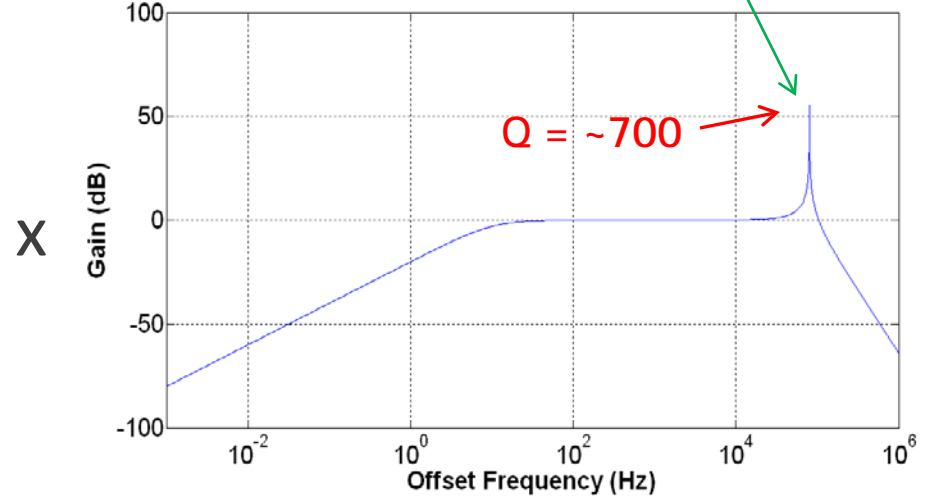
$$S_{\phi}^{cav\ effective}(f) = S_{\phi}^{LLRF} \cdot |N_{RTFB}(s) \cdot \beta_N(s)|^2$$

Beam Orbit Transfer Function

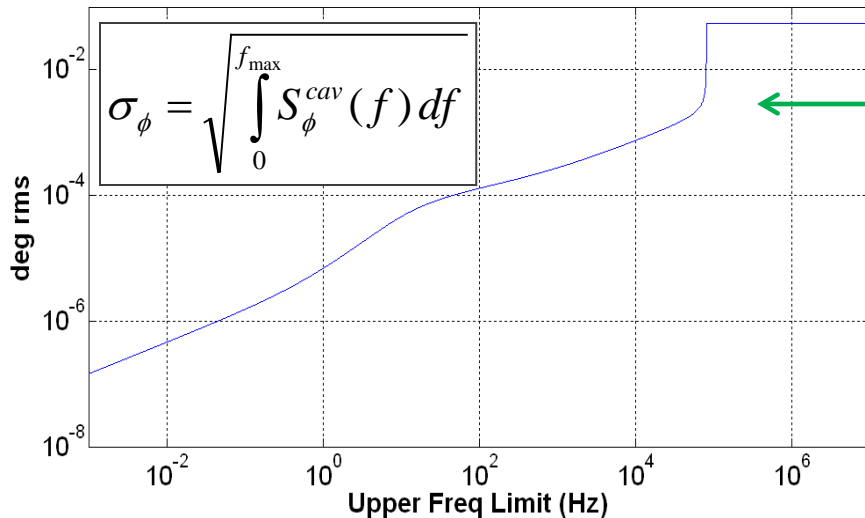
LLRF Detector Phase Noise Spectrum



Effective LLRF Detector Noise Transfer Function



Cumulative Integral of Effective Phase Noise



0.054 deg RMS w Betatron Tune

0.0034 deg RMS w/o Betatron Tune

Expect lower Q when including existing transverse feedback system

Will study the need for:
narrow-band beam-based feedback near the betatron resonance