

# SPX Study Workshop

## LLRF R&D

ANL: Tim Berenc, Hengjie Ma, Ned Arnold, Frank Lenkszus

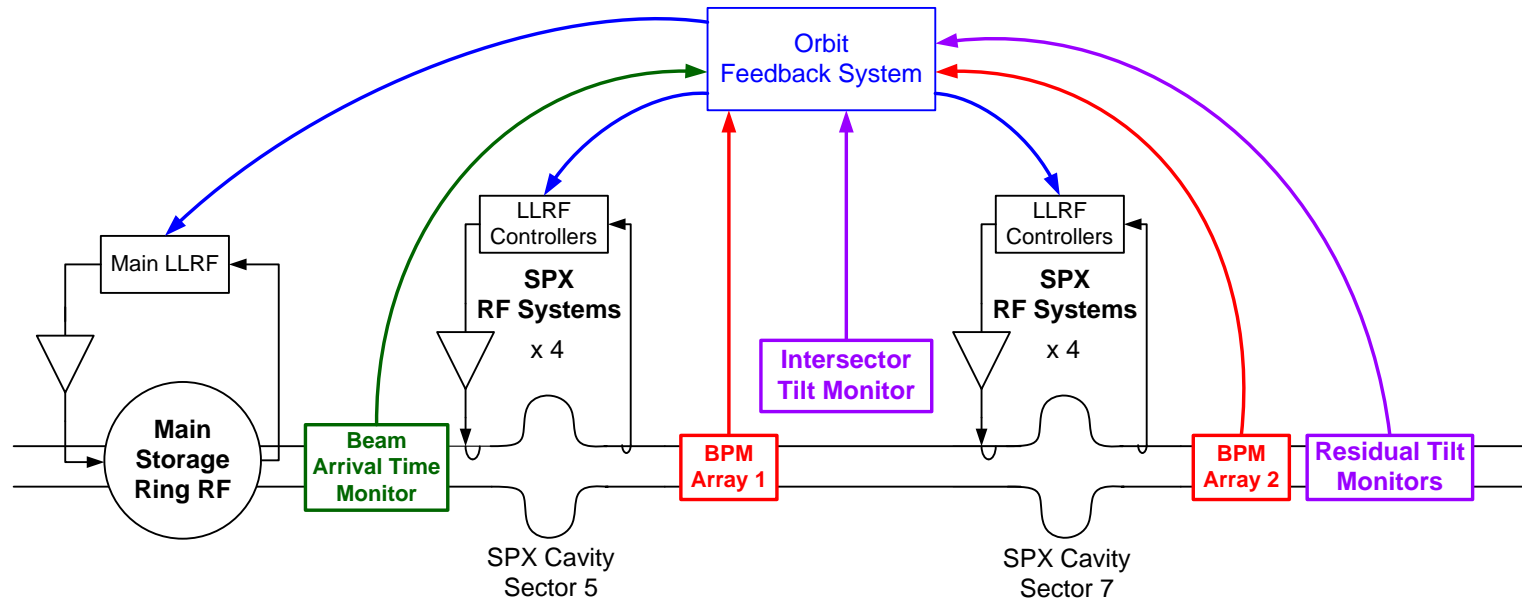
LBNL: Larry Doolittle, Gang Huang, John Byrd

July 18, 2011



# Conceptual Design Strategy

- Orbit Feedback System provides long-term stability ...  $< 100$  (200) Hz
- LLRF System on its own  $> 10$  Hz
  - 10 Hz – 100(200) Hz overlap with Orbit Feedback



**BPM Array 1:** sets phase of Sector 5

**BPM Array 2:** sets phase of Sector 7

**Intersector Tilt Monitor:** sets amplitude of Sector 5

**Residual Tilt Monitors:** sets amplitude of Sector 7

**Beam Arrival Time Monitor:** sets phase of Main Storage Ring RF

# Conceptual RF Control Architecture

## ■ Single Klystron per cavity with digital LLRF + Analog Front End

### – Want fast independent control of each cavity

- *Deflecting cavity beam loading is a function of offset and tilt – not expected to be the same cavity to cavity or sector to sector (i.e., electrical alignment errors)*
- *Microphonics not expected to be common mode, especially between sectors*

## ■ Phase Reference, LO (& CLK) distributed centrally to keep phase noise common mode

### – Provisions for both *coax-based* and *LBNL phase stabilized fiber* reference

- *Orbit feedback eliminates long-term drift concerns*
- Coax provides superior short-term noise, fiber provides superior long-term noise to alleviate control effort of orbit feedback and is needed for synchronizing user laser
- Comparison of short-term noise of *fiber link* vs. *coax* needs to be measured

## ■ Receiver Chain Drift Compensation via Calibration Tone

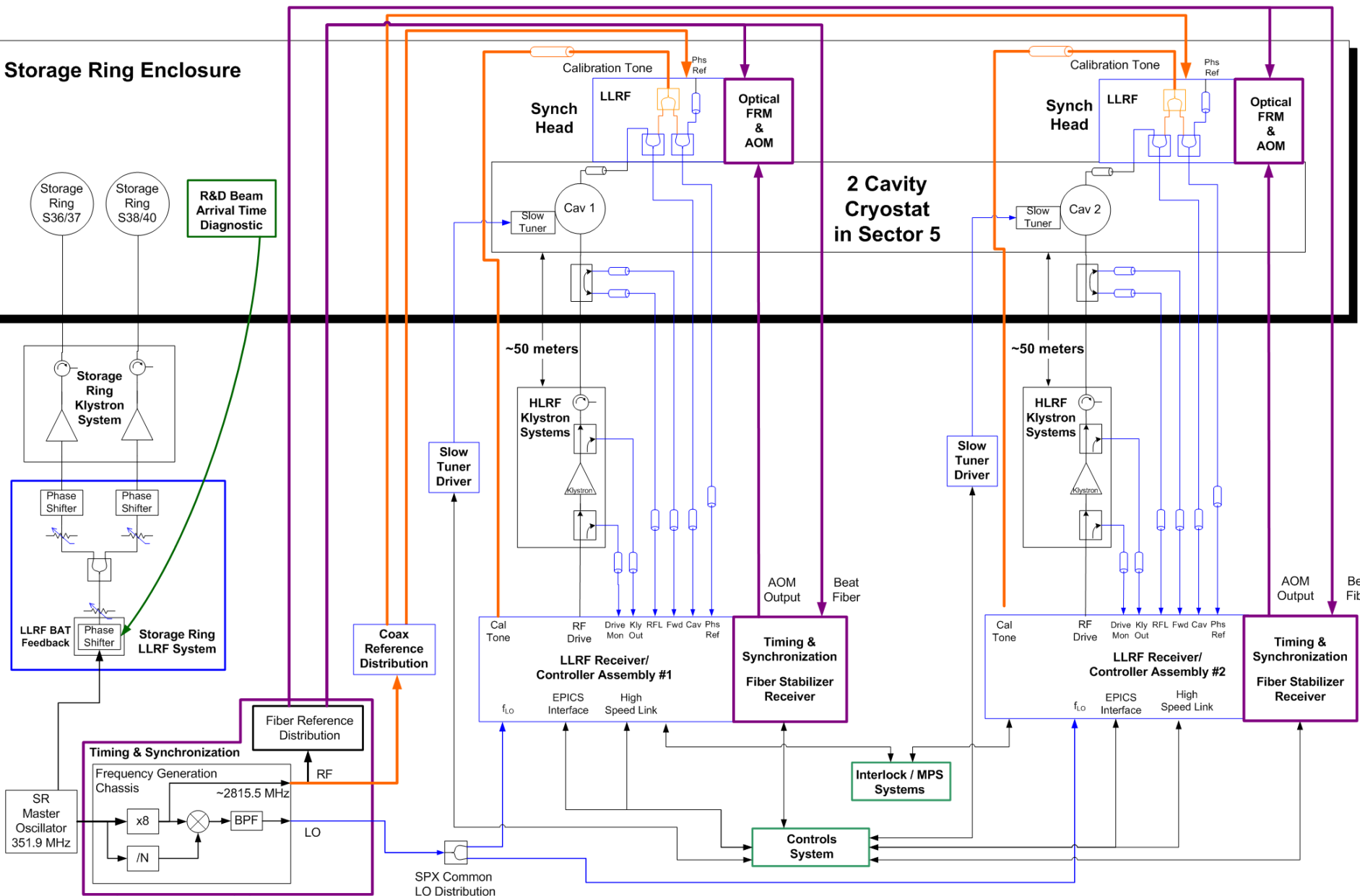
## ■ Sector to Sector Control derived from beam-based Feedback

## ■ Beam Arrival Time Feedback to Main Storage Ring RF to lock beam to Master Oscillator



# R&D System Concept (1 Sector, 2 cavities)

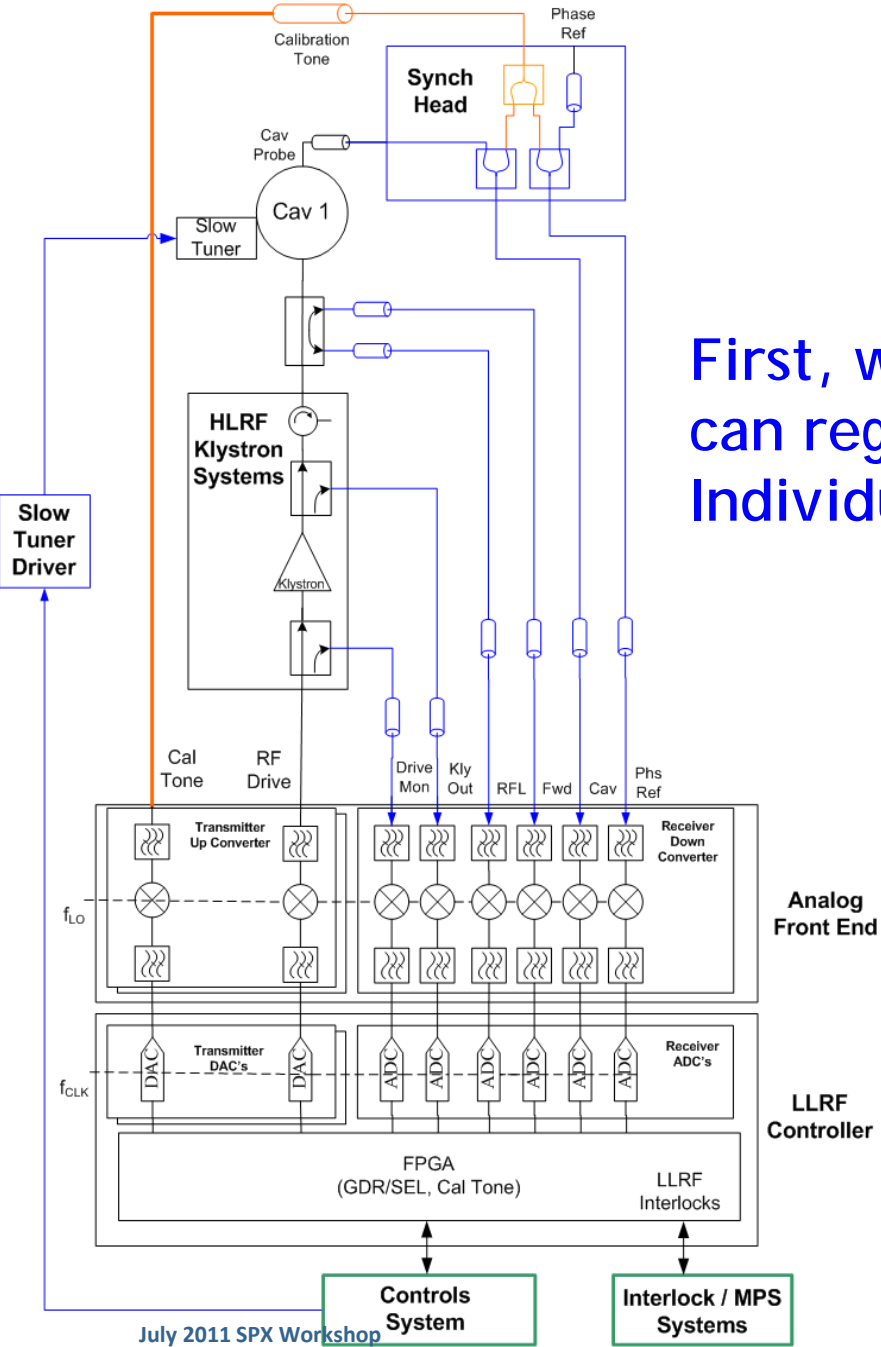
## Storage Ring Enclosure



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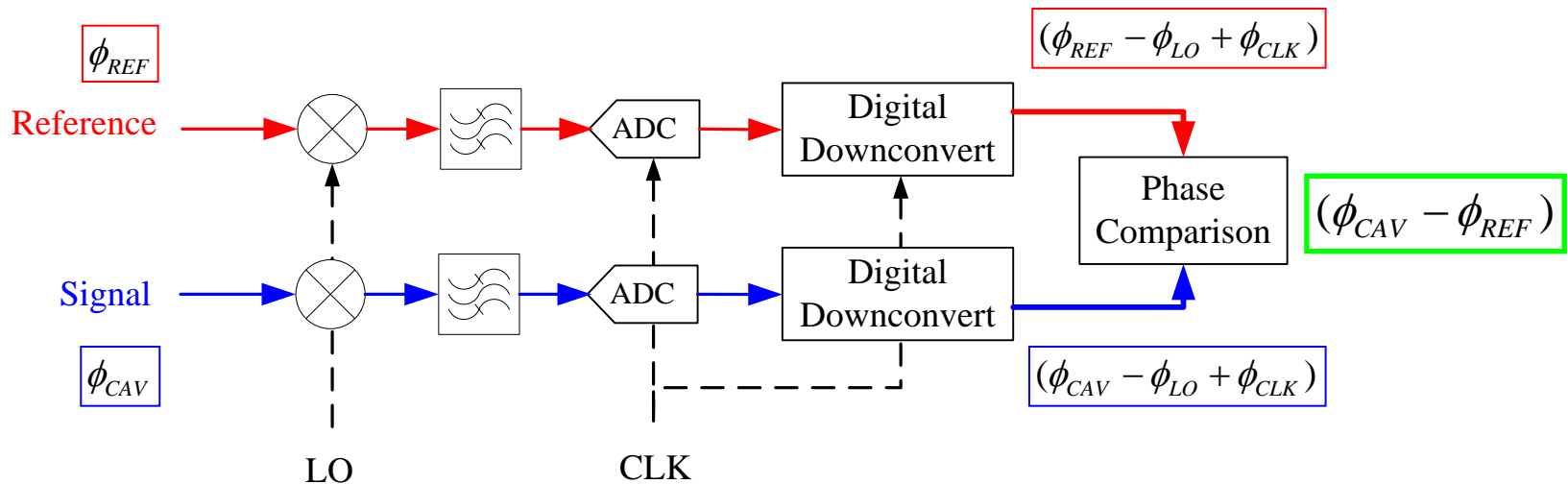


First, we will need to demonstrate that we can regulate the fields at the Individual Cavity Level ...

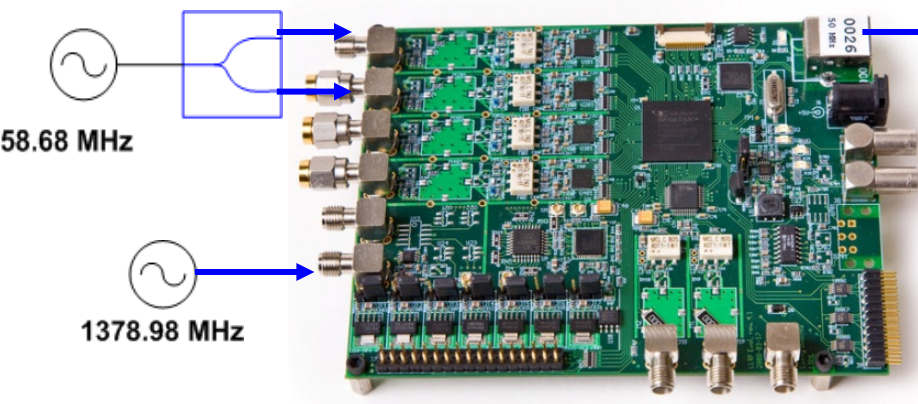


# Strategy #1 - Regulate to a Designated Phase Reference

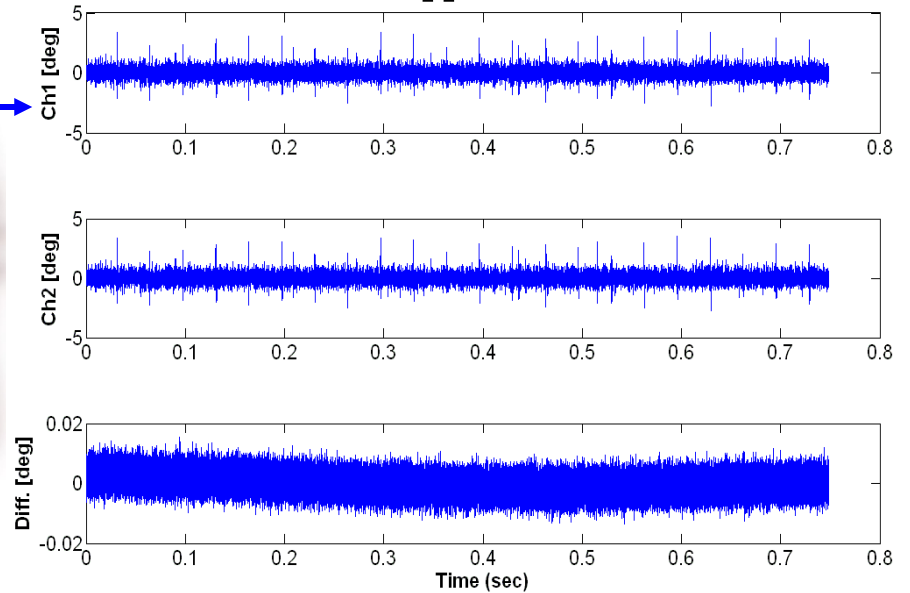
- Don't let the LO assume the role of the phase reference
- Phase is a Differential Measurement
- Mixers preserve phase information
- In theory, common mode LO and clock noise cancels



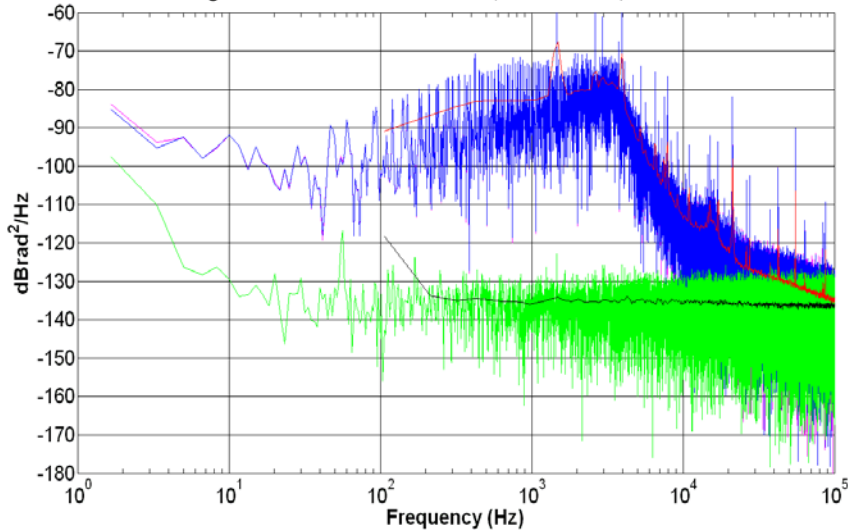
# LLRF4 Board - Input Differential Phase Noise



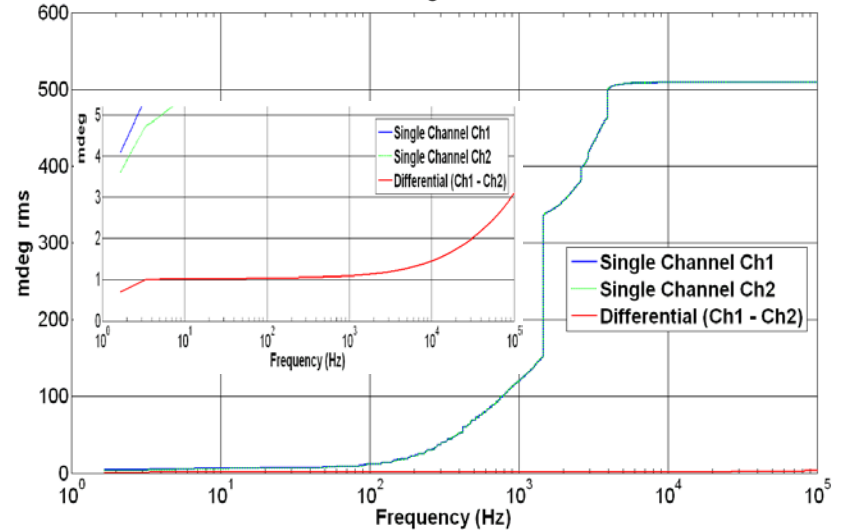
DataSet test\_0\_00\*.bin from 6/10/2011



LLRF4 Single Channel vs. Phase Diff. PSD, IF=58.68MHz, CIKIN=1378.98MHz

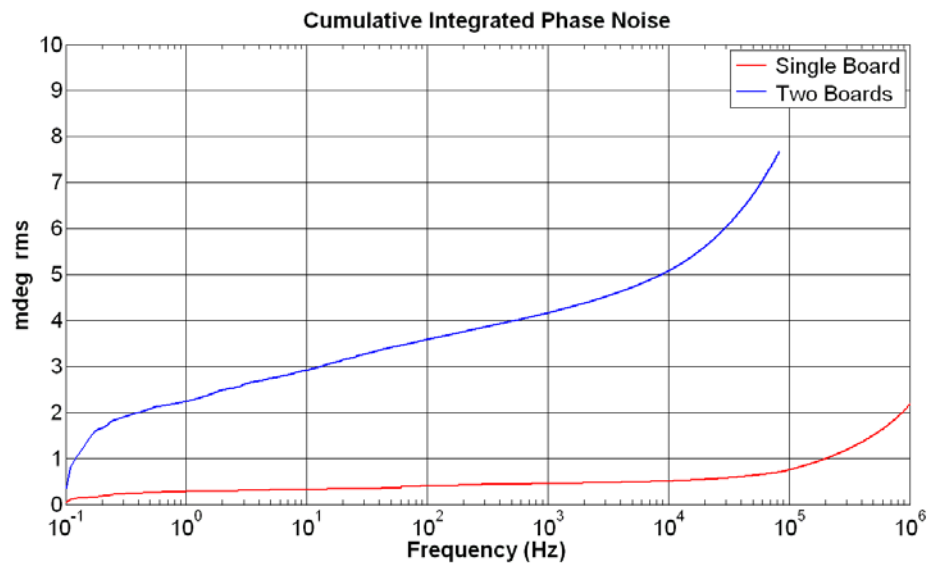
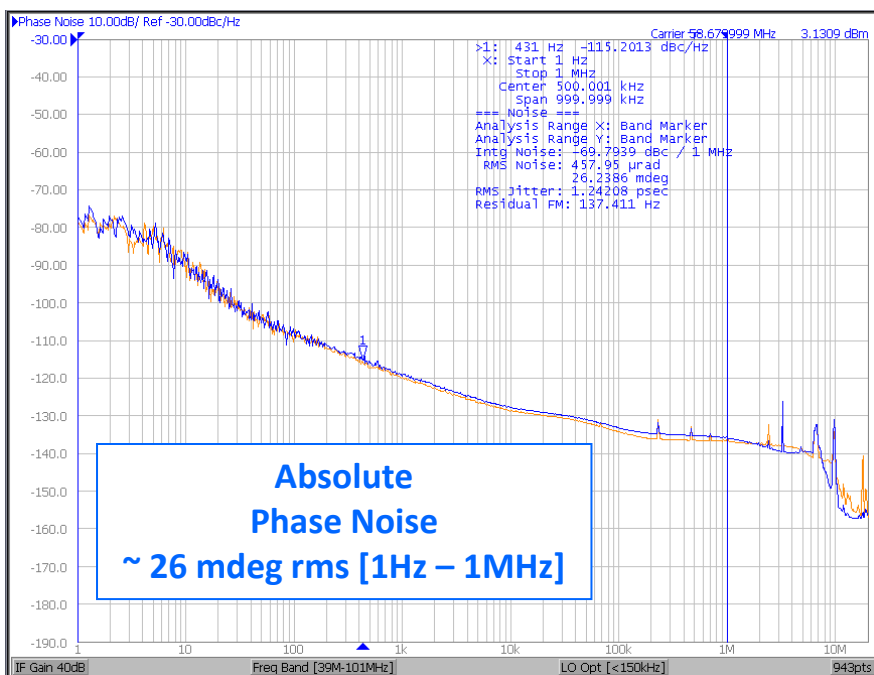
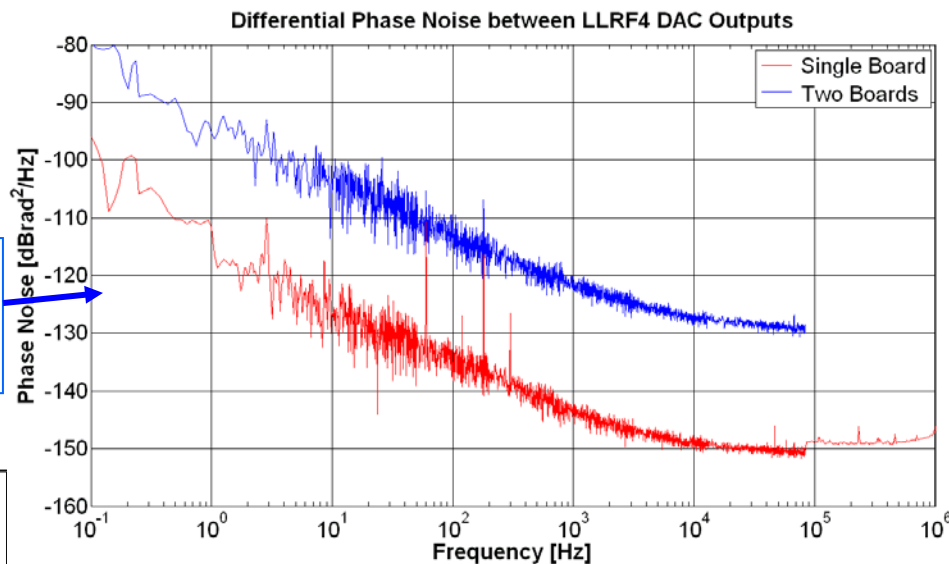
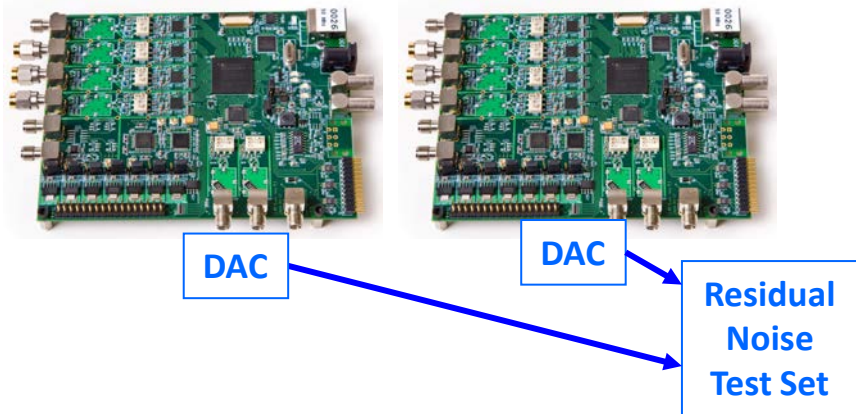


Cumulative Integrated Phase Noise



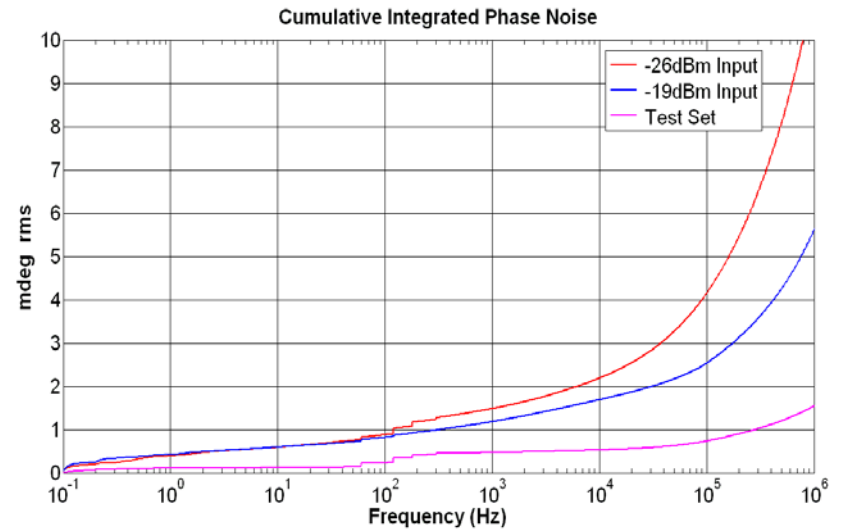
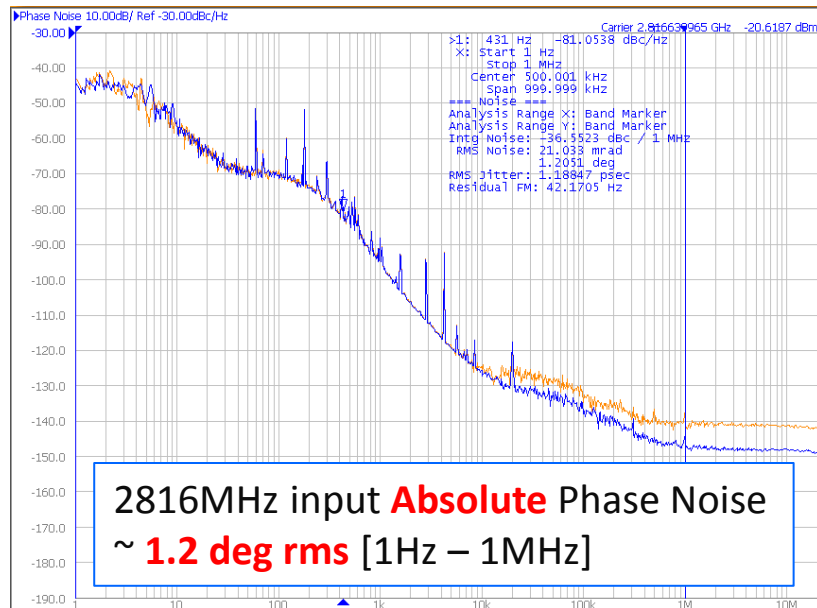
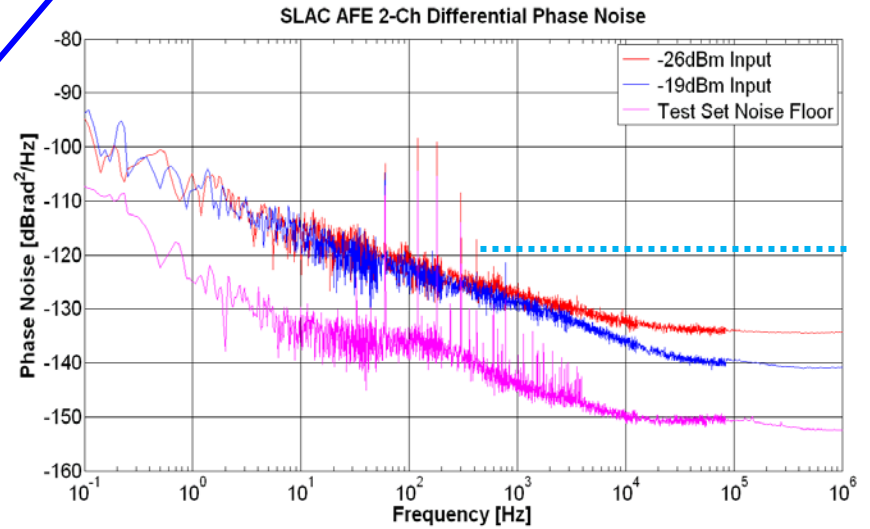


# LLRF4 Board - Output Phase Noise

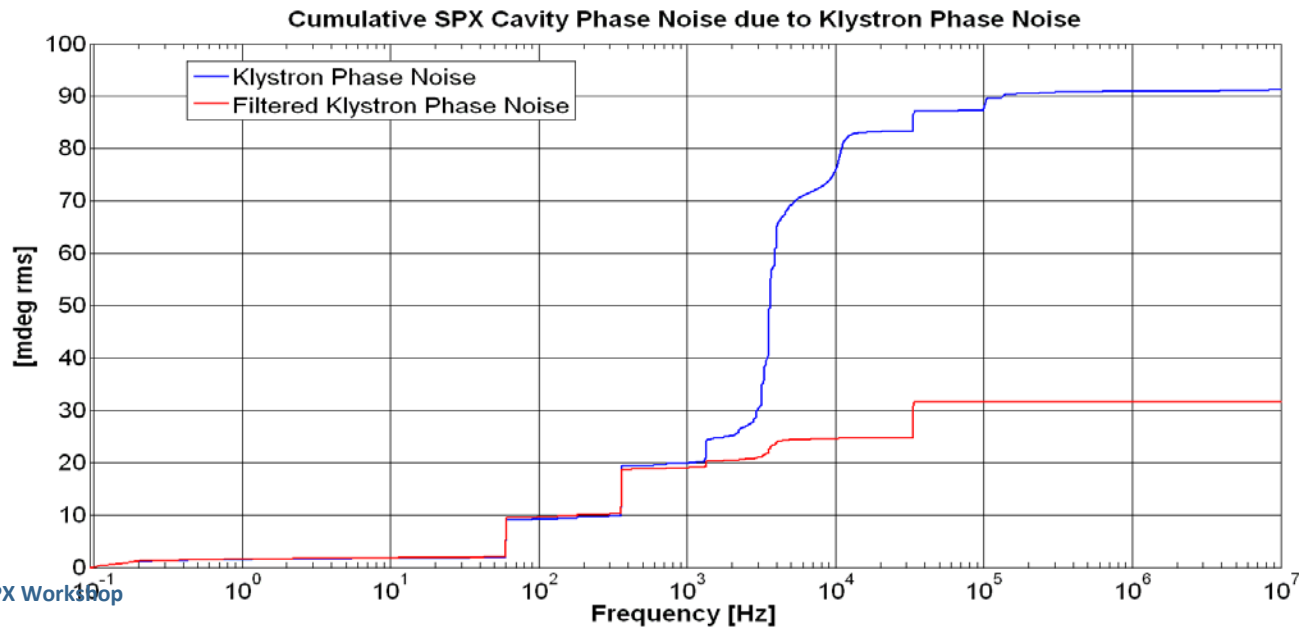
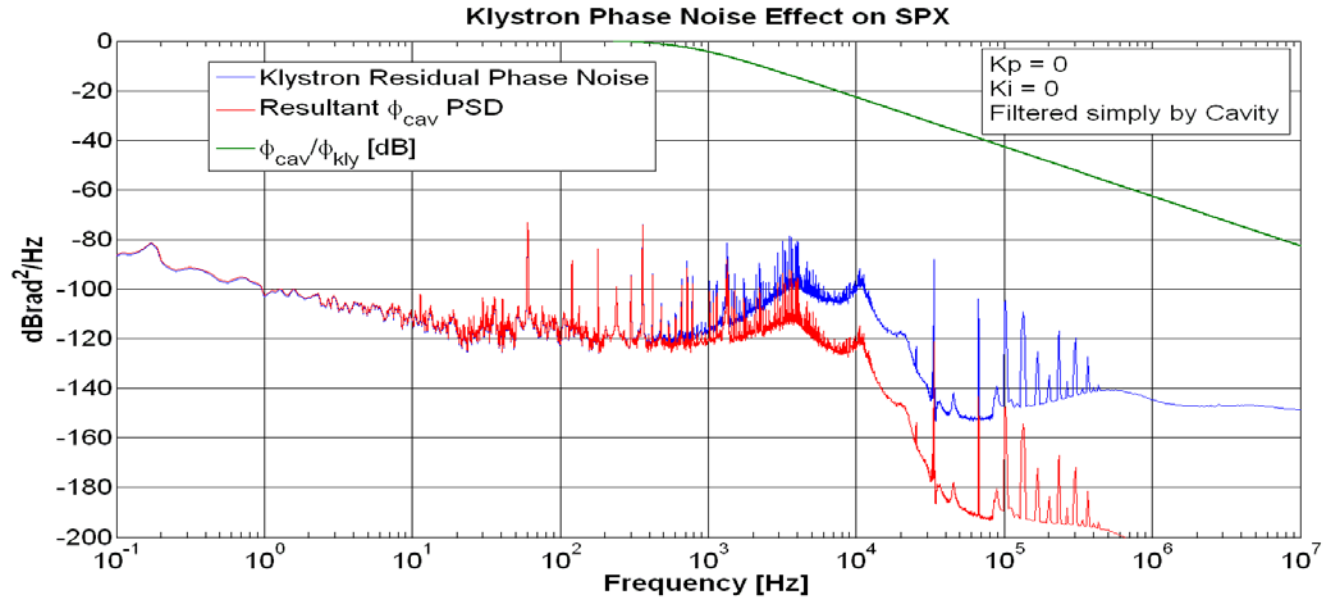


# Analog Front End - Differential Phase Noise

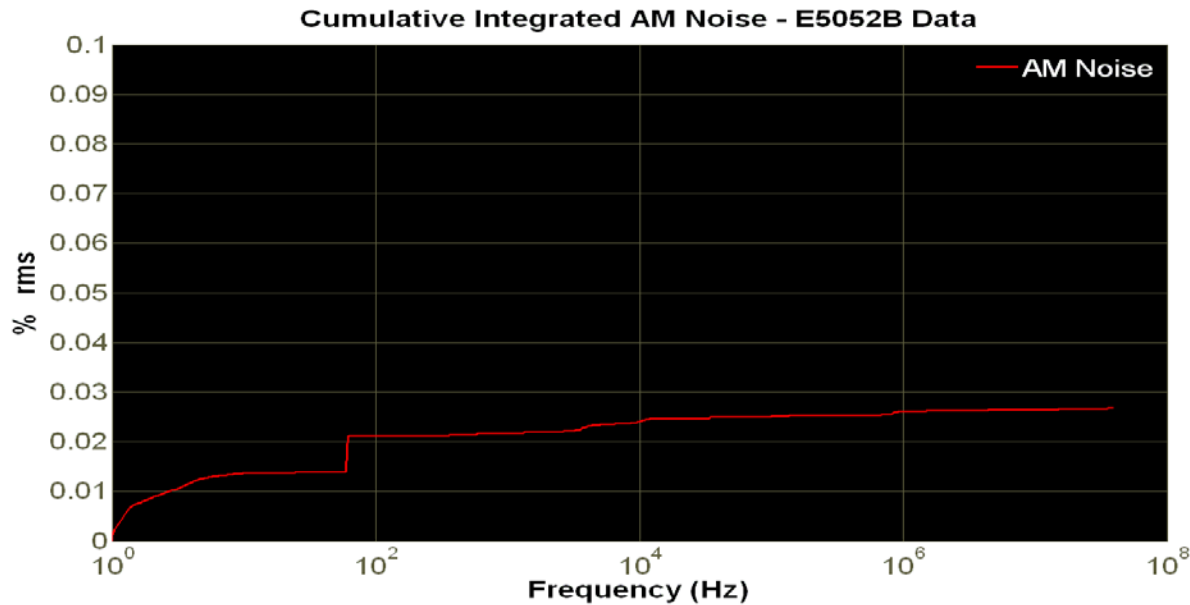
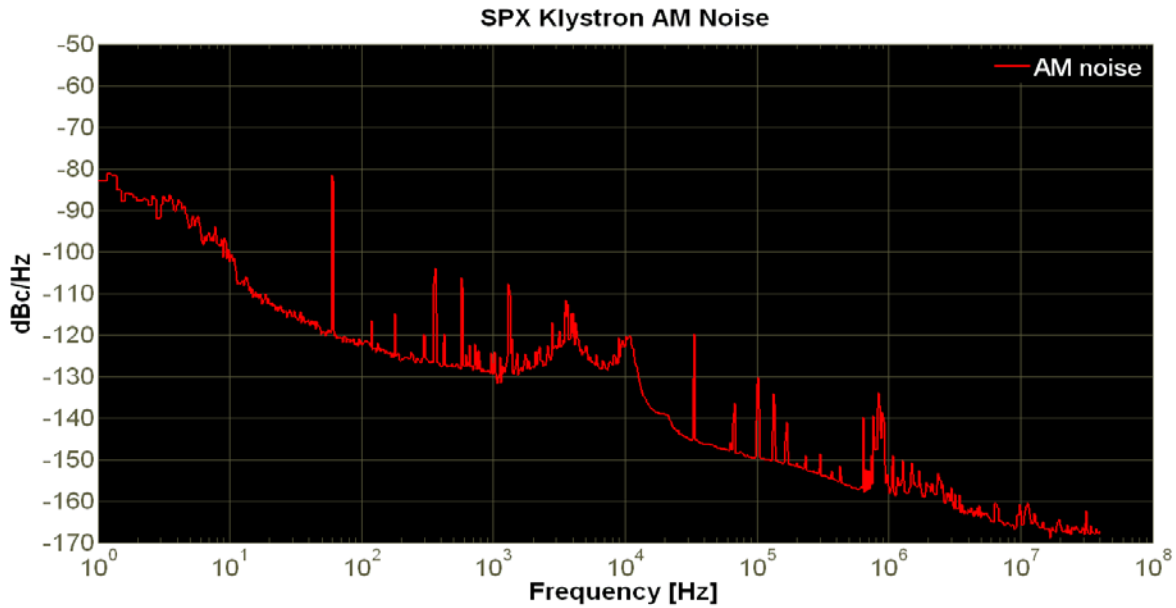
## Differential Phase Noise at IF Frequency



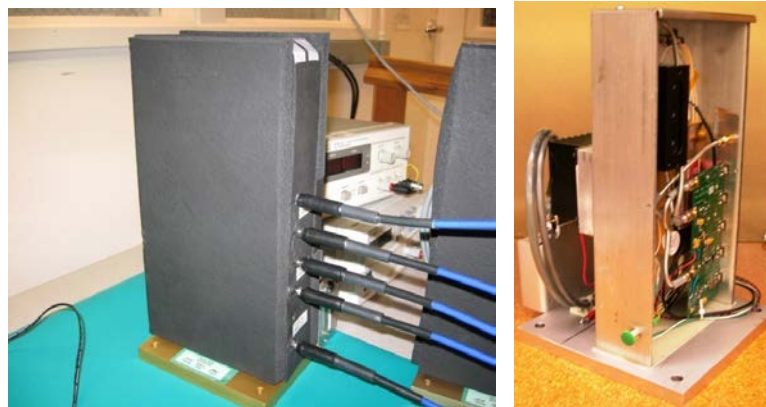
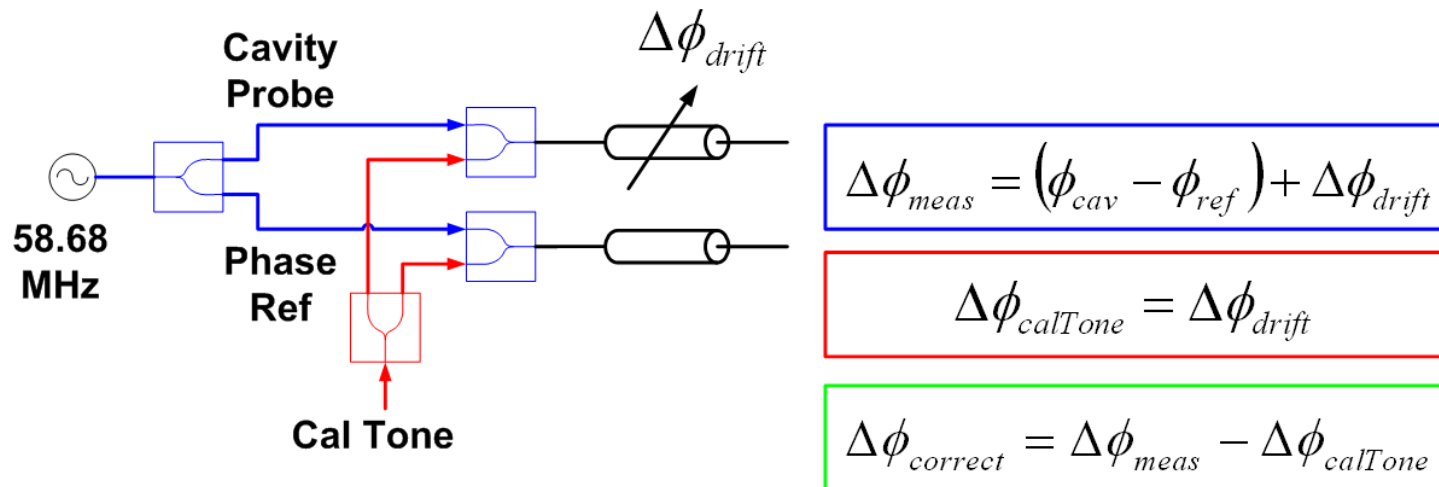
# Klystron Residual Noise Measurements



# Klystron AM Noise Measurements



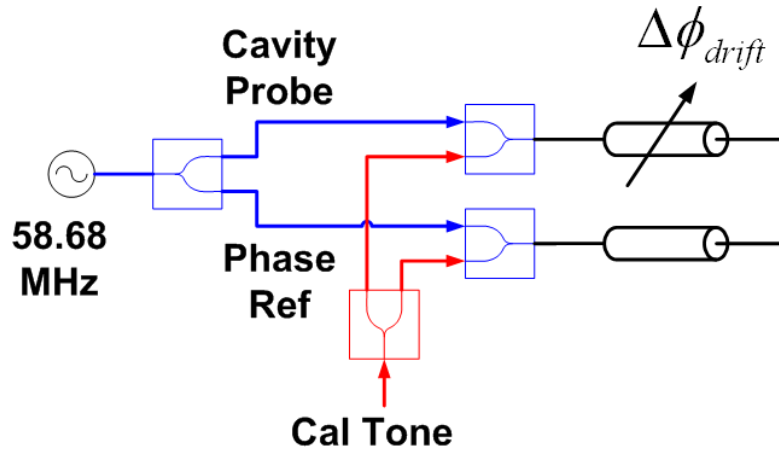
## Strategy #2 - Incorporate CW Drift Compensation<sup>[1]</sup>



LBNL "Synch Head" example (2-channel version)

[1] "Signal Processing for High Precision Phase Measurements", G. Huang, L. Doolittle, J. Staples, R. Wilcox, J. Byrd, Proceedings of BIW10

# Demonstration of CW Drift Compensation

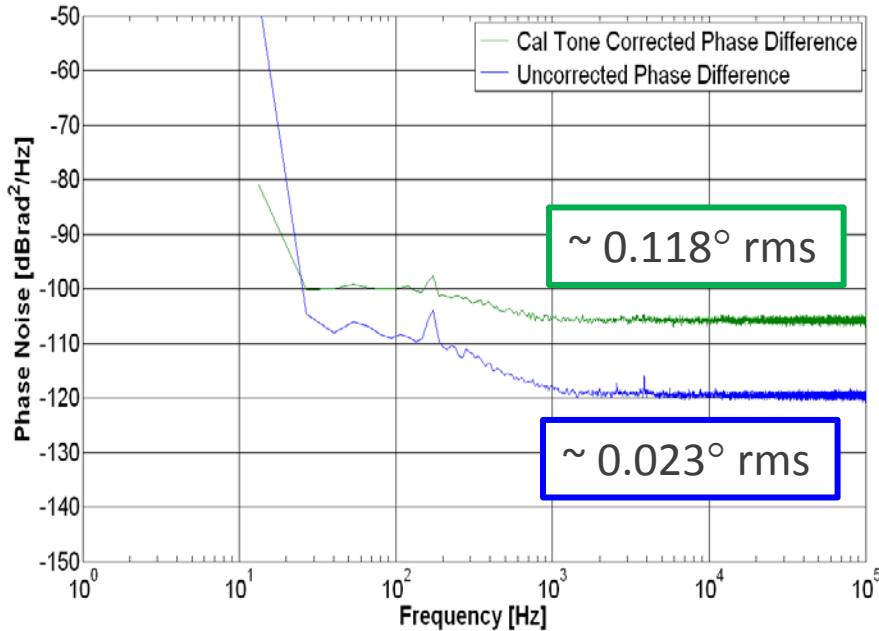


$$\Delta\phi_{meas} = (\phi_{cav} - \phi_{ref}) + \Delta\phi_{drift}$$

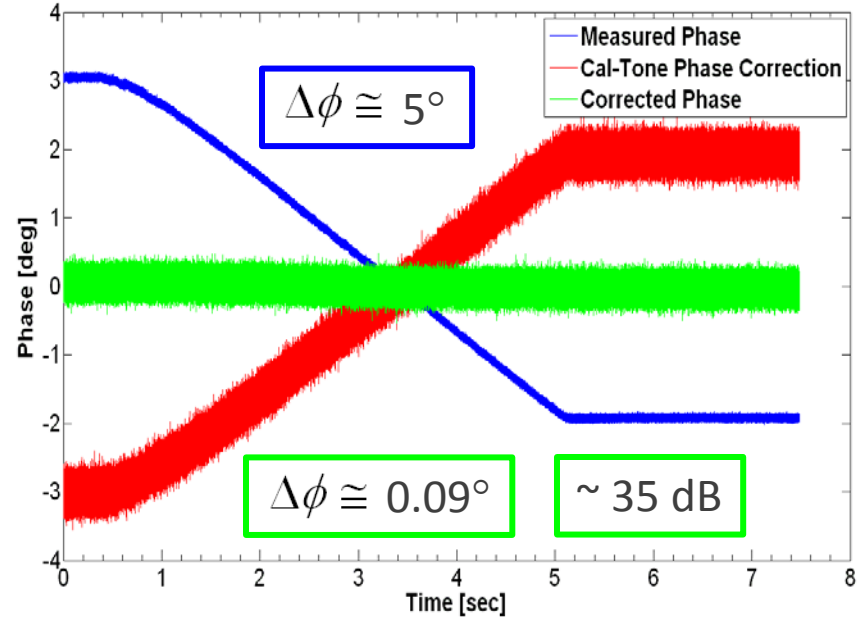
$$\Delta\phi_{calTone} = \Delta\phi_{drift}$$

$$\Delta\phi_{correct} = \Delta\phi_{meas} - \Delta\phi_{calTone}$$

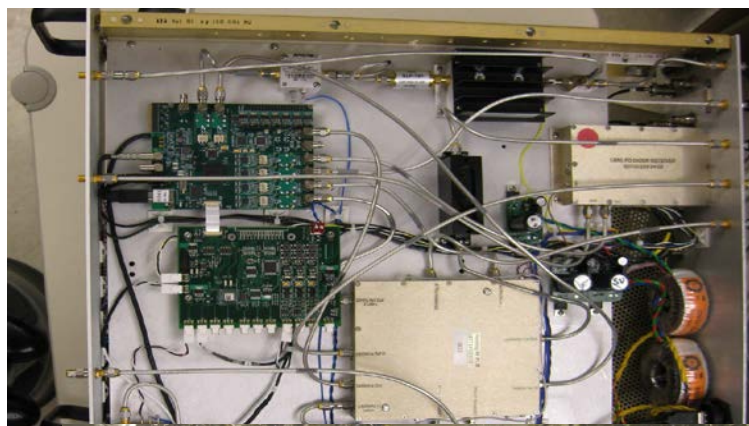
LLRF4 Differential Phase Noise with & w/o Cal Tone Process



LLRF4 Cal-Tone Process Example Measurement at IF=58.68MHz

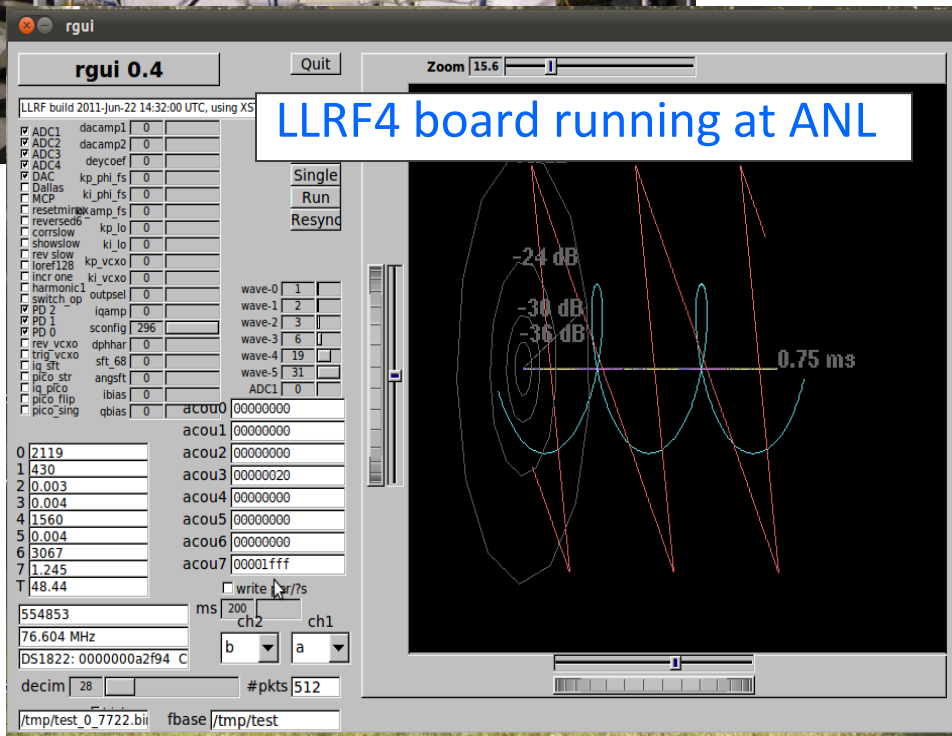


# Single Cavity Testing at ANL scheduled for 2/2012



LLRF4 based system to support LLRF & Timing R&D 10/2011

- Delivery of first LLRF4 system for LLRF control
- Report on differential stability study between 2 high Q cavity emulator systems



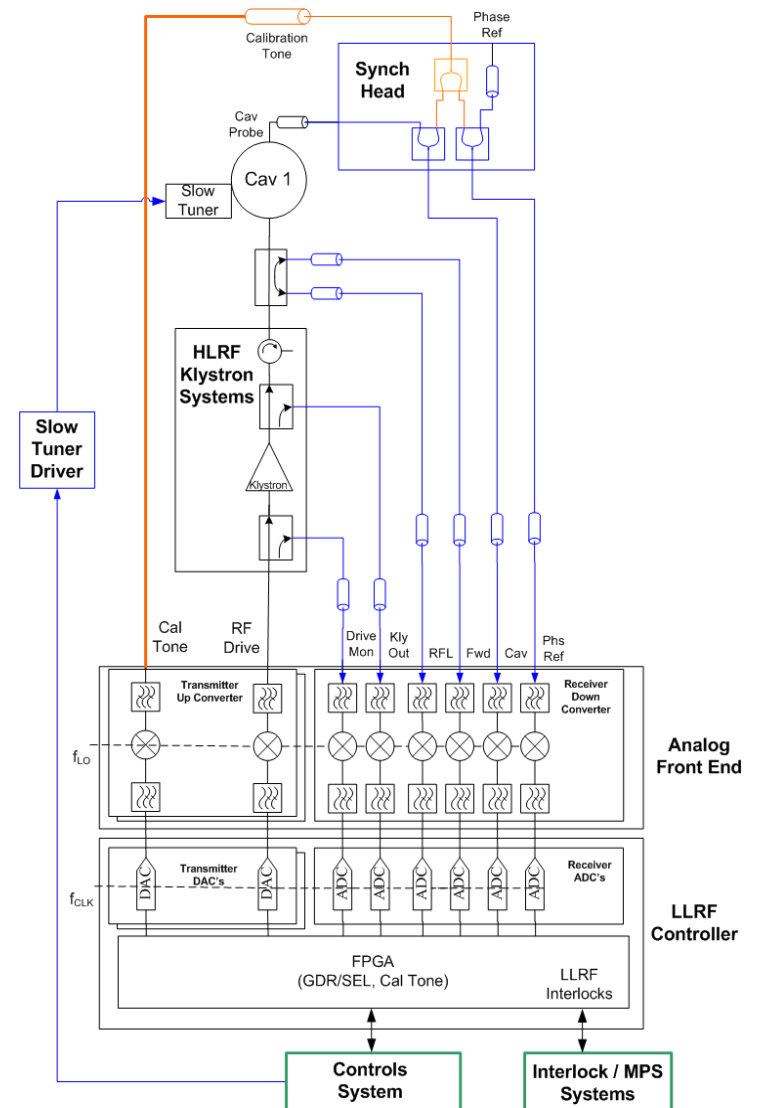
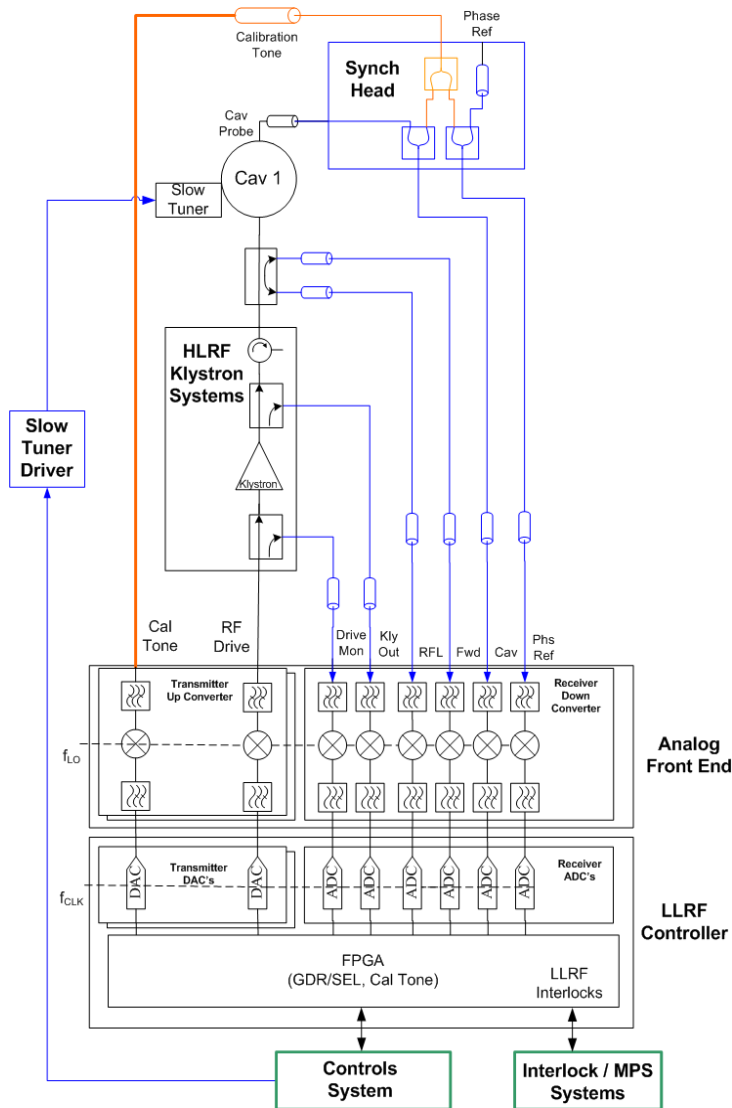
LLRF4 board running at ANL



JLab Stepper Motor Driver will be used for the Slow Tuner

- Delivery estimated 1/2012

# Then, we need to demonstrate that we can achieve the differential specs between 2 cavities

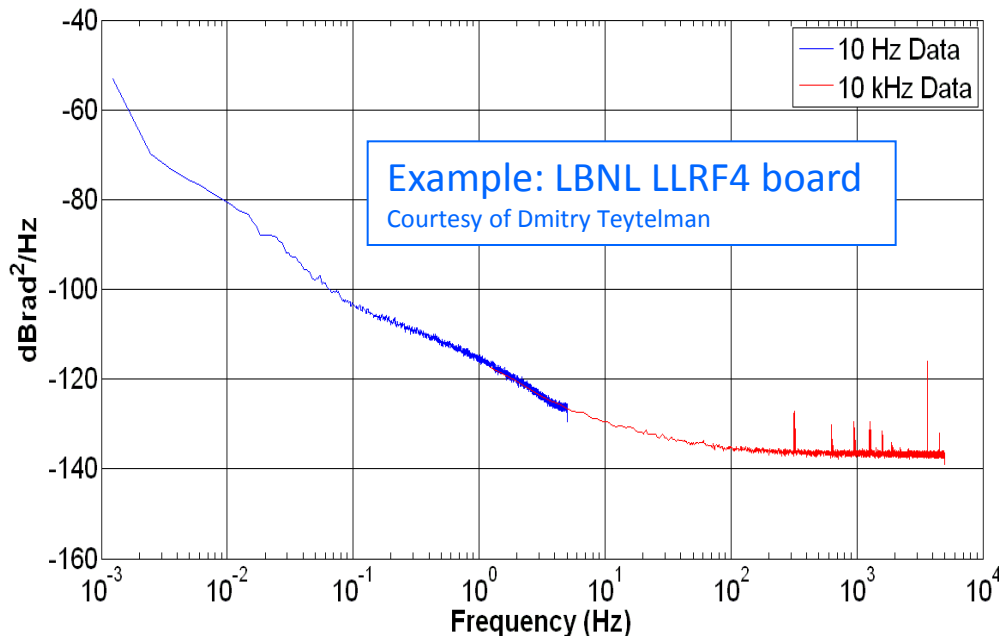




# How to achieve 0.18° rms Differential Phase ??

- Digital LLRF receiver noise floors show capability at least > 1Hz
- Beam-based feedback strategy planned for < 100(200) Hz
- LBNL drift compensation schemes provide long term stability
- Deflecting cavity system noise performance will be measured in R&D
  - Need to explore microphonics, beam-loading & cavity alignment concepts

LLRF4 Phase Noise PSD



$$S_{\phi}(f) \cong b_0 + \frac{b_1}{f} + \frac{b_2}{f^2}$$

$$b_0 = 1.585 \cdot 10^{-14} \text{ rad}^2/\text{Hz}$$

$$b_1 = 1.585 \cdot 10^{-12} \text{ rad}^2$$

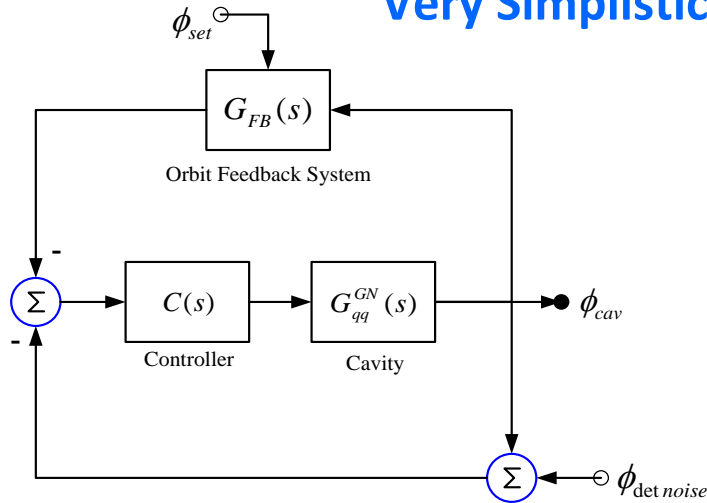
$$b_2 = 6.31 \cdot 10^{-13} \text{ rad}^2\text{Hz}$$

$$\sigma_{\phi} = \sqrt{\int_{f_{\min}}^{f_{\max}} S_{\phi}^{cav}(f) df}$$

0.0072 deg RMS  
1Hz to 1MHz

# How to achieve 0.18° rms Differential Phase ??

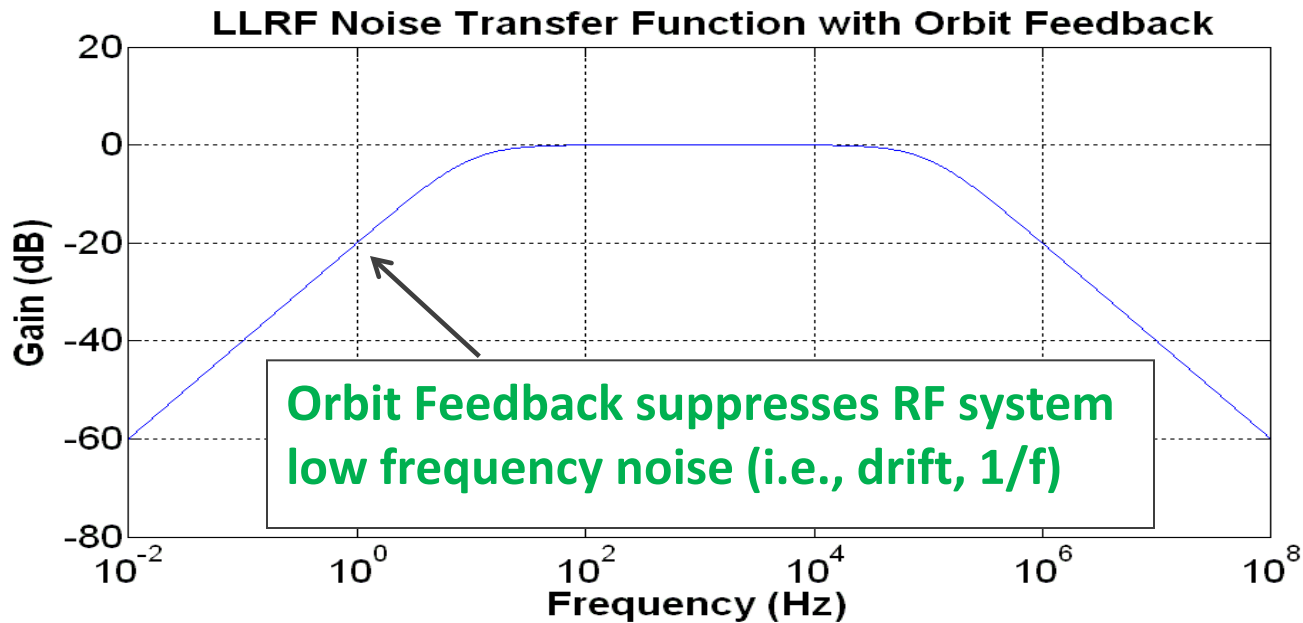
## Very Simplistic First Order Orbit Feedback concept



Assume: 
$$G_{FB}(s) = \frac{K_p^{RTFB} \sigma_{RTFB}}{s}$$

$$N_{FB}(s) = \frac{\phi_{cav}(s)}{\phi_{detnoise}(s)} = \frac{C(s)G_{qq}^{GN}(s)}{1 + C(s)G_{qq}^{GN}(s)[1 + G_{FB}(s)]}$$

$$= \frac{K_p \sigma_{cav} s}{s^2 + K_p \sigma_{cav} s + K_p^{RTFB} K_p \sigma_{RTFB} \sigma_{cav}}$$

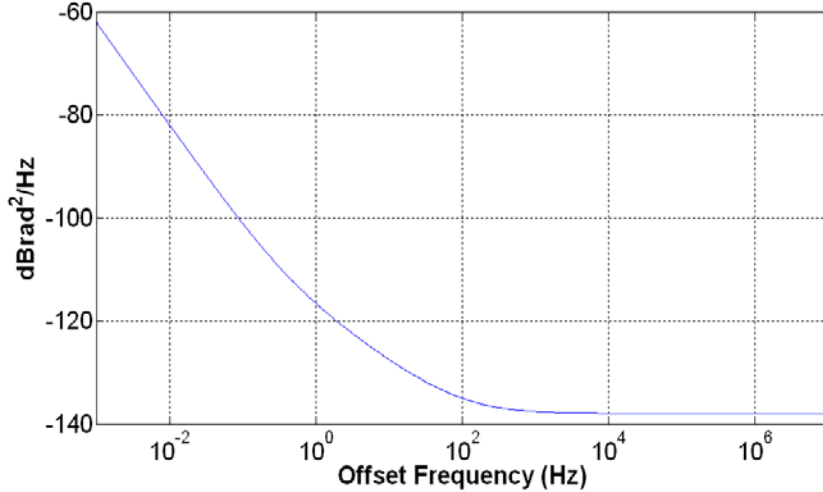


# How to achieve 0.18° rms Differential Phase ??

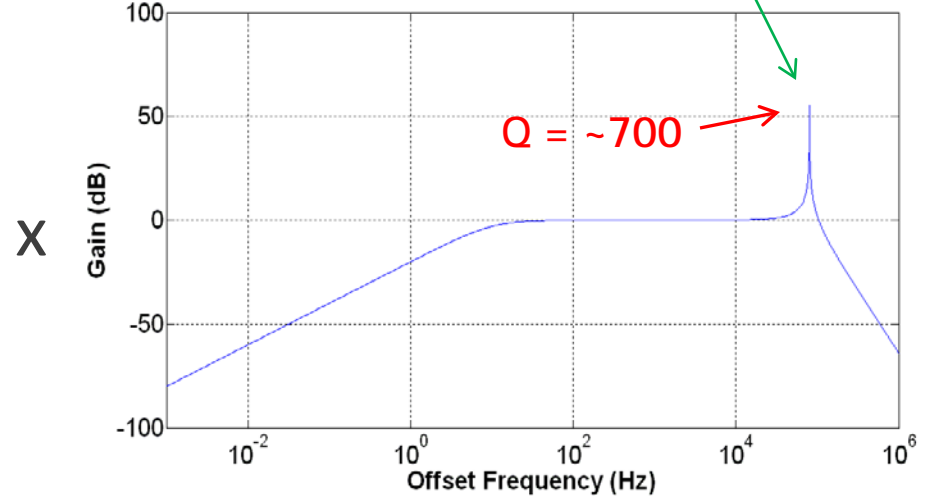
$$S_{\phi}^{cav\ effective}(f) = S_{\phi}^{LLRF} \cdot |N_{RTFB}(s) \cdot \beta_N(s)|^2$$

← Beam Orbit Transfer Function

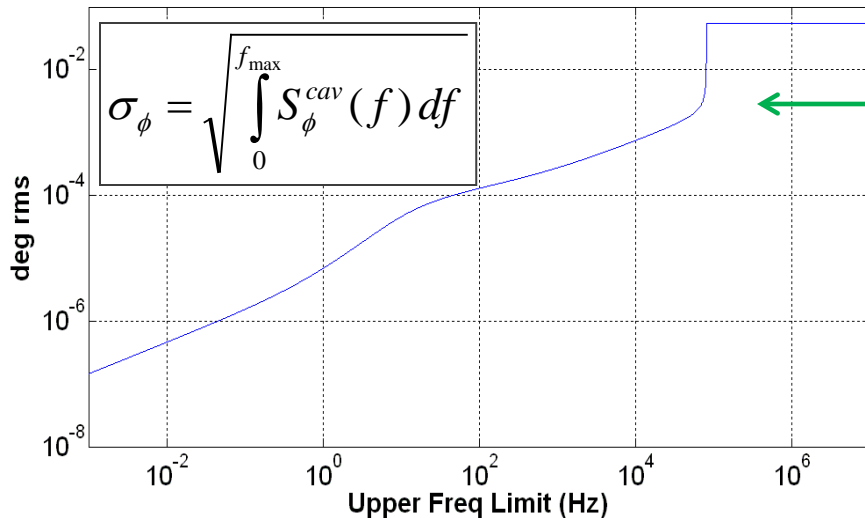
LLRF Detector Phase Noise Spectrum



Effective LLRF Detector Noise Transfer Function



Cumulative Integral of Effective Phase Noise



← 0.054 deg RMS w Betatron Tune

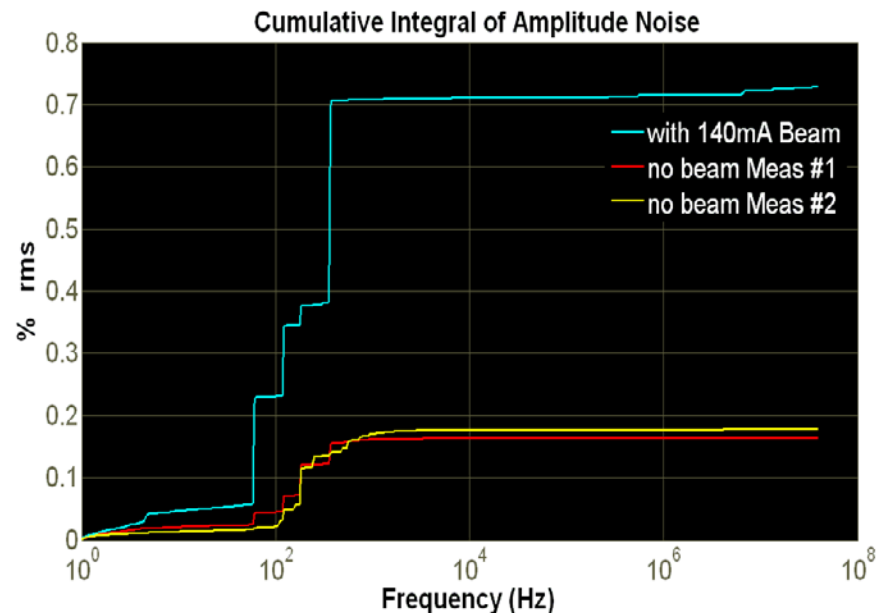
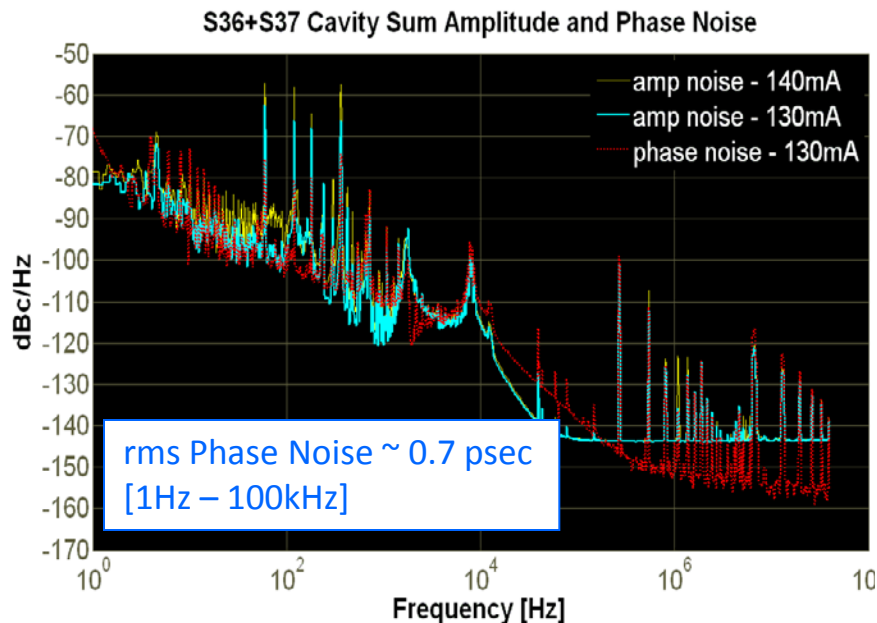
← 0.0034 deg RMS w/o Betatron Tune

Expect lower Q when including existing transverse feedback system

Will study the need for:  
narrow-band beam-based feedback near the betatron resonance

# Common Mode Phase Considerations

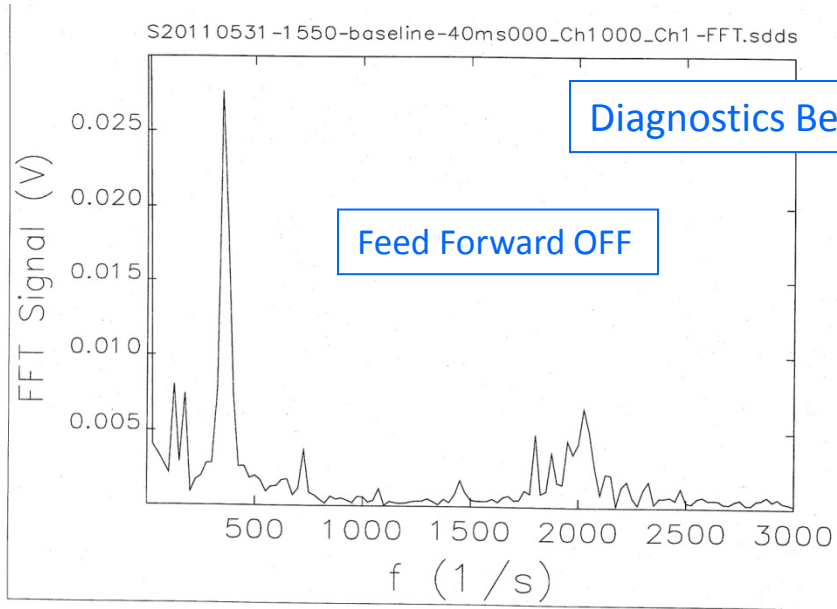
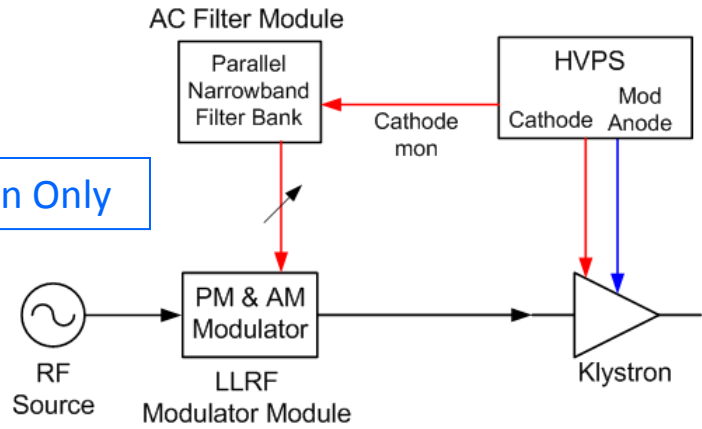
- $4.0^\circ$  rms =  $\sim 4$  psec rms common mode spec
  - Existing beam jitter
    - Initial diagnostic studies show  $\sim 2.7$  psec rms beam jitter
    - Beam physics simulations based upon rf measurements of AM and PM noise resulted in 1.7 psec rms
    - Extensive studies of main 352 MHz rf system noise have been taking place (APSU\_1417419, APSU\_1416636, APSU\_1416055, APS\_1414611)
  - Planning on beam arrival time feedback to main 352 MHz



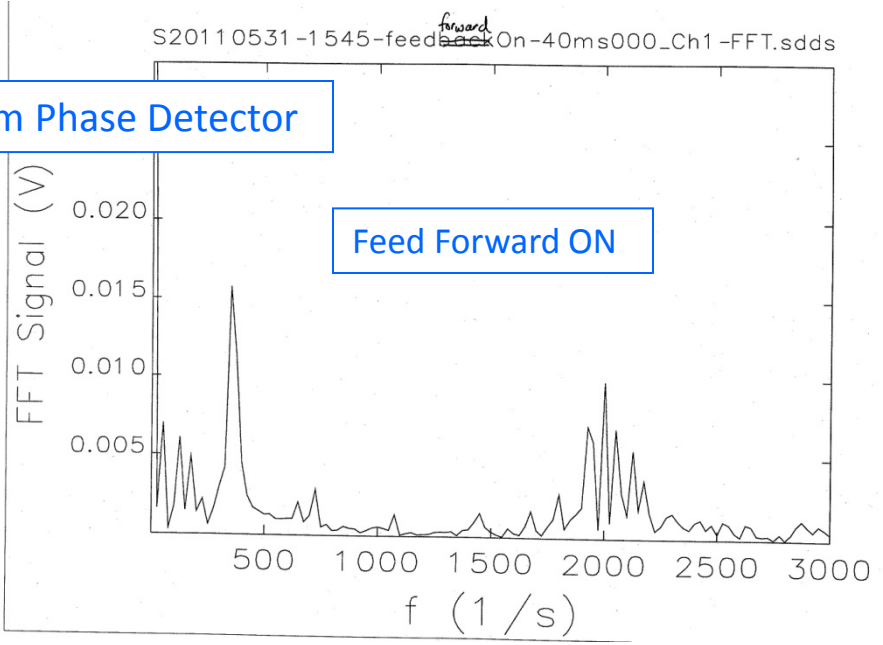
# Challenges and Strategy - 4° Common Mode Phase Spec

Have recently experimented with 360Hz Feed-Forward correction of Kly HVPS induced noise

AM suppression at 1 Station Only



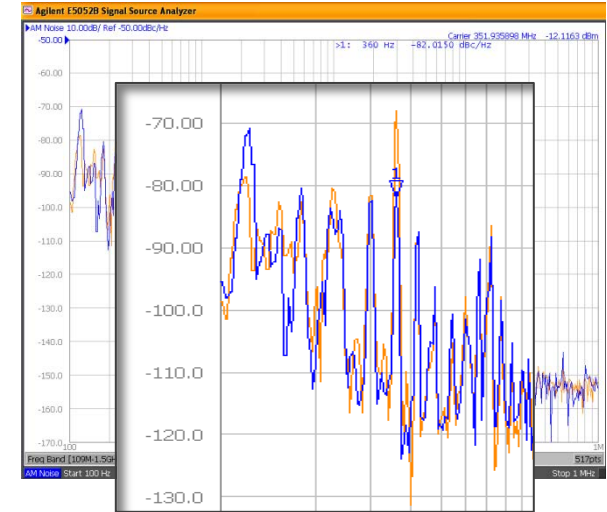
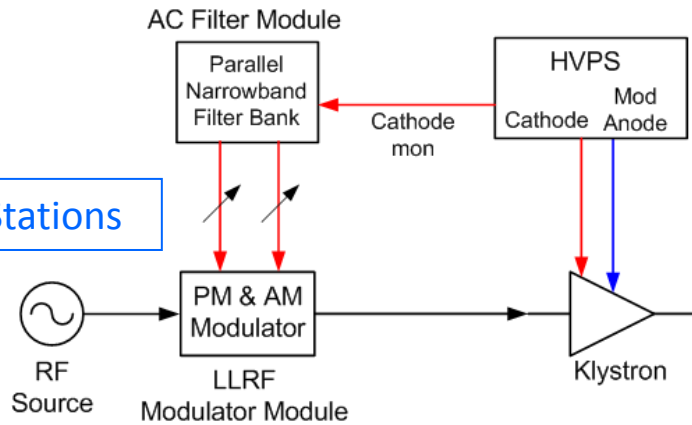
Diagnostics Beam Phase Detector



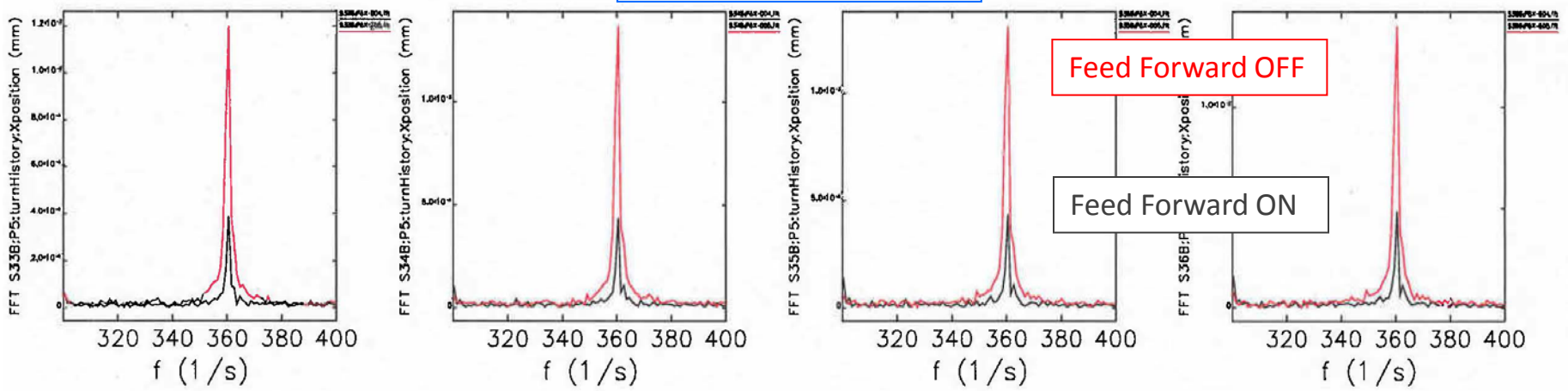
# Challenges and Strategy - 4° Common Mode Phase Spec

Have recently experimented with 360Hz Feed-Forward correction of Kly HVPS induced noise

AM & PM suppression at Both Stations



Horizontal BPM Data



# R&D Scope - Technical Description

# Major Challenges

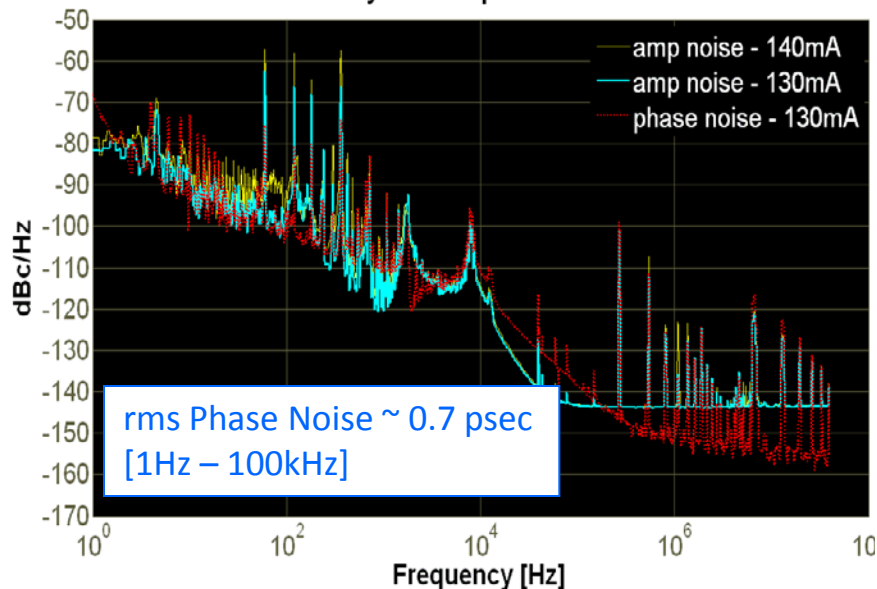




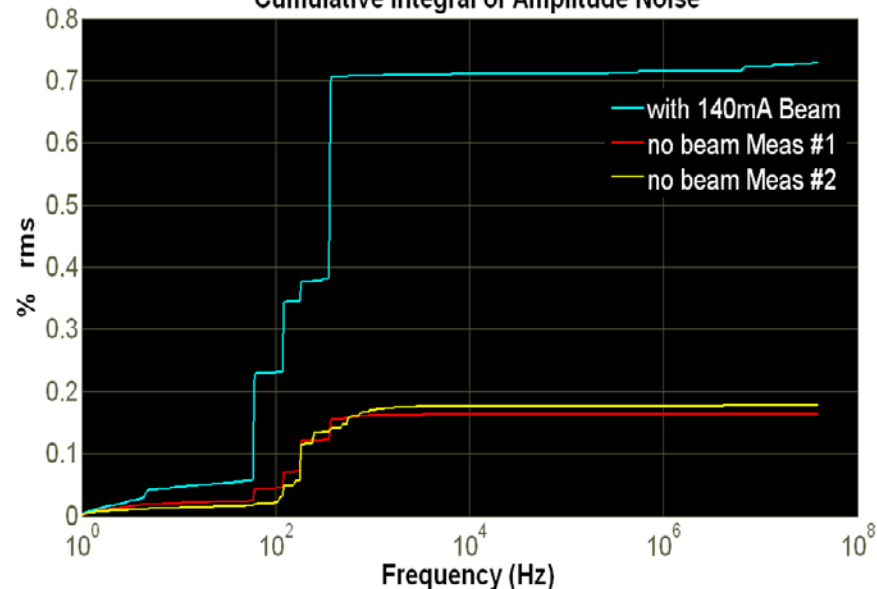
# Challenges and Strategy - 4° Common Mode Phase Spec

- 4.0° rms = ~4 psec rms common mode spec
  - Existing beam jitter
    - Initial diagnostic studies show only ~2.7 psec rms beam jitter
    - Beam physics simulations based upon rf measurements of AM and PM noise resulted in 1.7 psec rms
    - Extensive studies of main 352 MHz rf system noise have been taking place (APSU\_1417419, APSU\_1416636, APSU\_1416055, APS\_1414611)
  - Planning on beam arrival time feedback to main 352 MHz

S36+S37 Cavity Sum Amplitude and Phase Noise

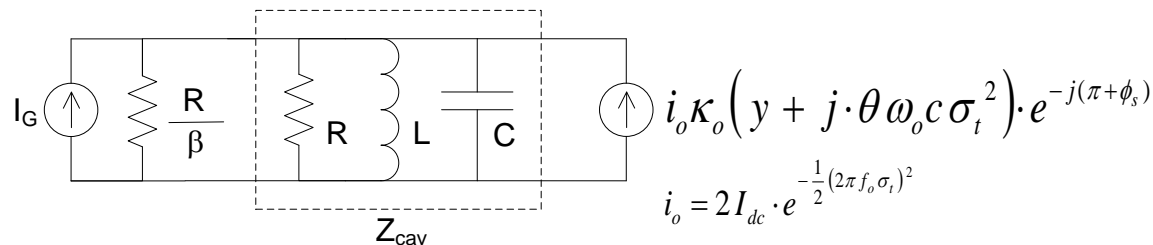


Cumulative Integral of Amplitude Noise

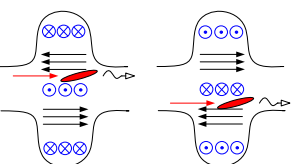


# Challenges and Strategy - Tools

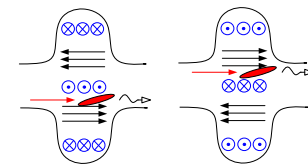
Have Beam-Loaded Deflecting Cavity Model, both static ...



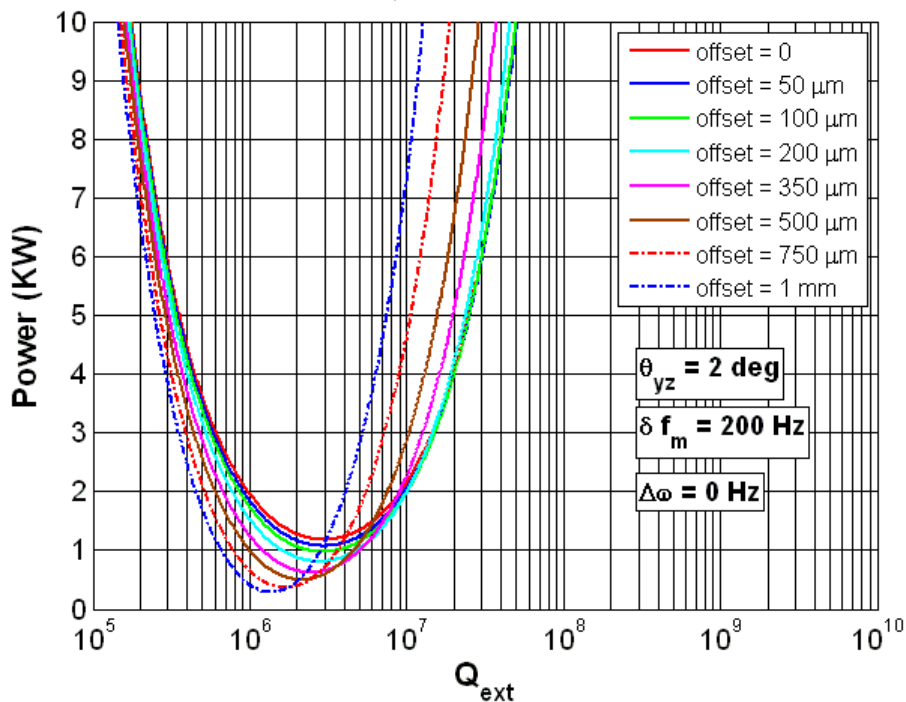
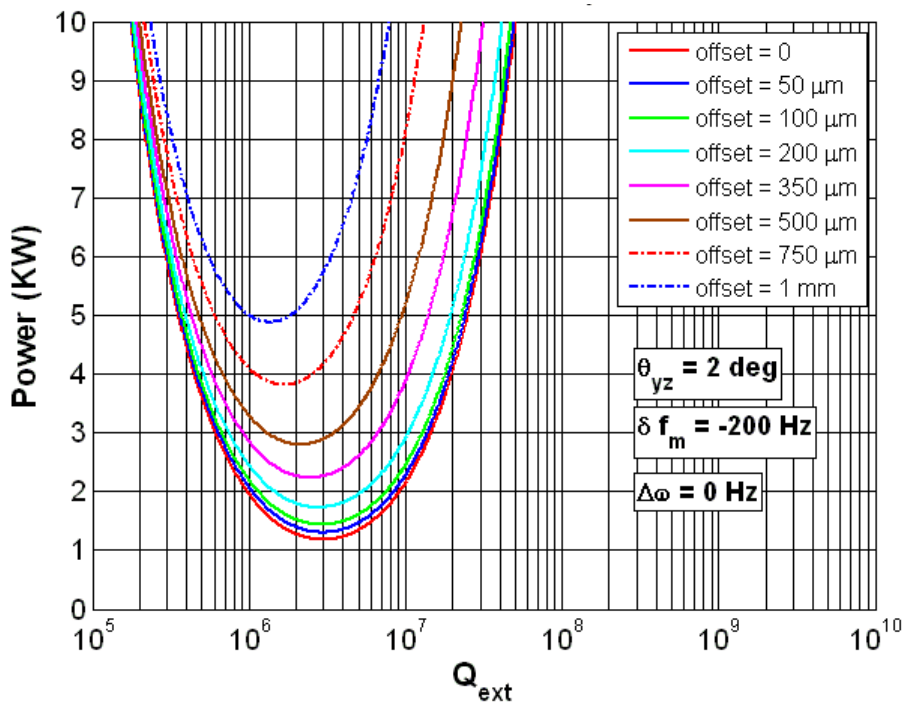
$$P_g^+ = \frac{V_t^2}{8\beta(R/Q)'Q_o} \cdot \left[ \left( \beta + 1 + \frac{P_B}{P_{cav}} \right)^2 + \left( 2Q_o \frac{(\Delta f + \delta f_m)}{f_r} + \frac{P_B}{P_{cav}} \tan \phi_s \right)^2 \right]$$



$V_t \cdot y > 0$



$V_t \cdot y < 0$



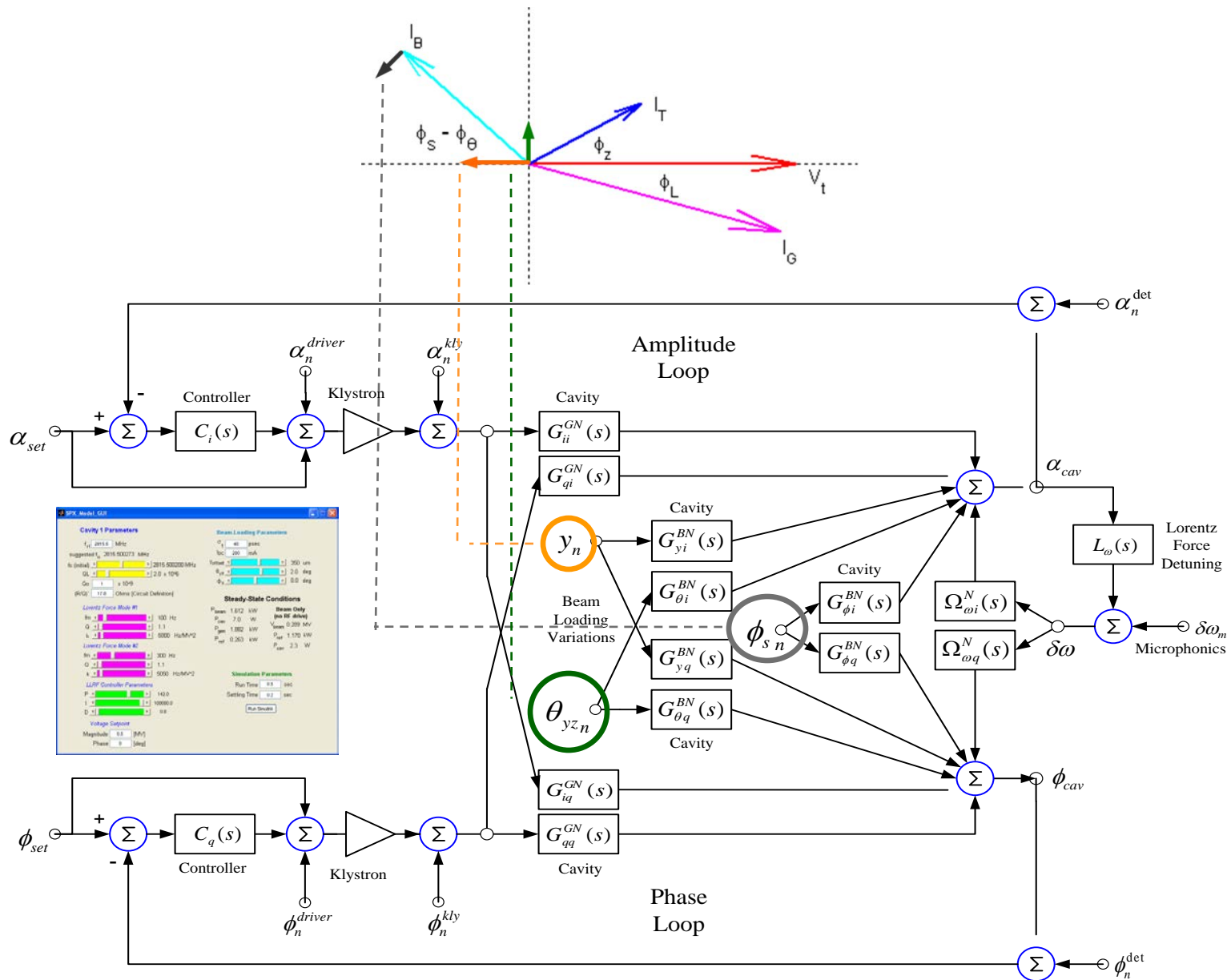
# Summary

- Extensive studies of main 352 MHz RF system noise have been taking place
  - Simulations from rf measurements show  $\sim 1.7$  psec rms beam jitter
  - Beam diagnostics measurements show  $\sim 2.7$  psec rms
- Planning on beam-based feedback to relax LLRF long-term drift and  $1/f^x$  noise
  - LBNL phase stable ref. & drift compensation will relax orbit control effort
- Plan to use digital LLRF control technology
  - LLRF4 based system to support R&D 2-cavity system
  - Preliminary Engineering provisions in schedule allow for lessons learned from LLRF4 with transition into Final Engineering.
- Have excellent tools (both theoretical models and measurement equipment) to track, measure, and ensure system performance
- Have an **EXCELLENT** LLRF Team capable of success
  - Collaboration with LBNL creates the synergy necessary for success

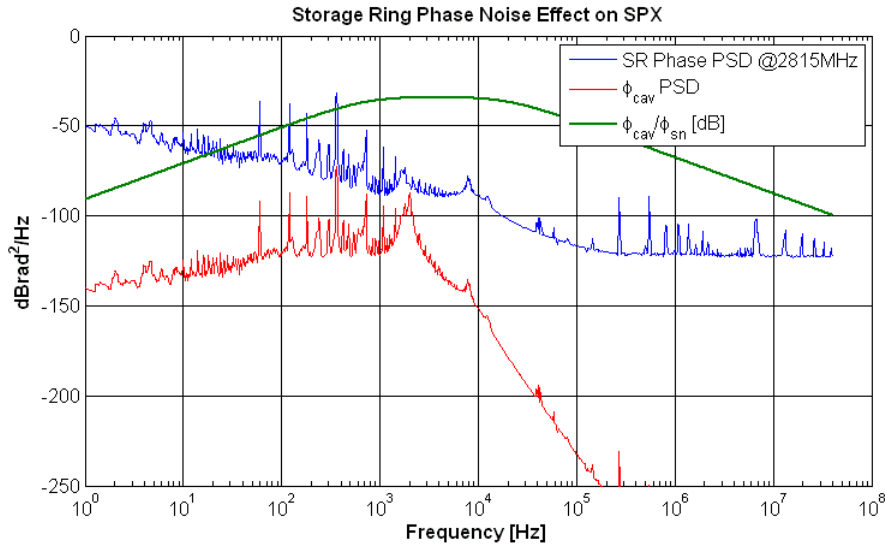
# Backup Slides



# Dynamic small signal model for individual crab cavity



# Motivation for Cavity Electrical Alignment Adjust

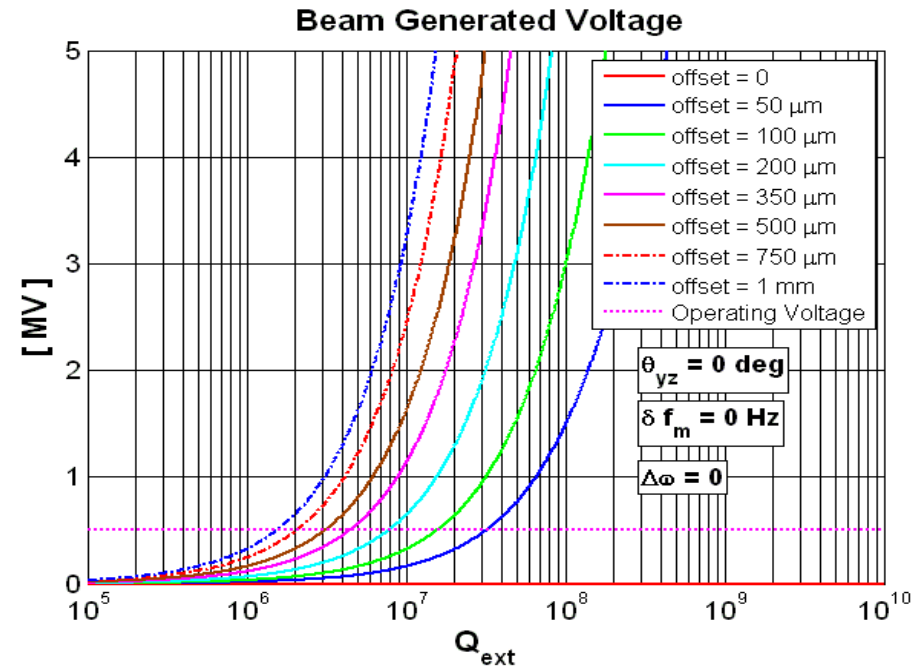
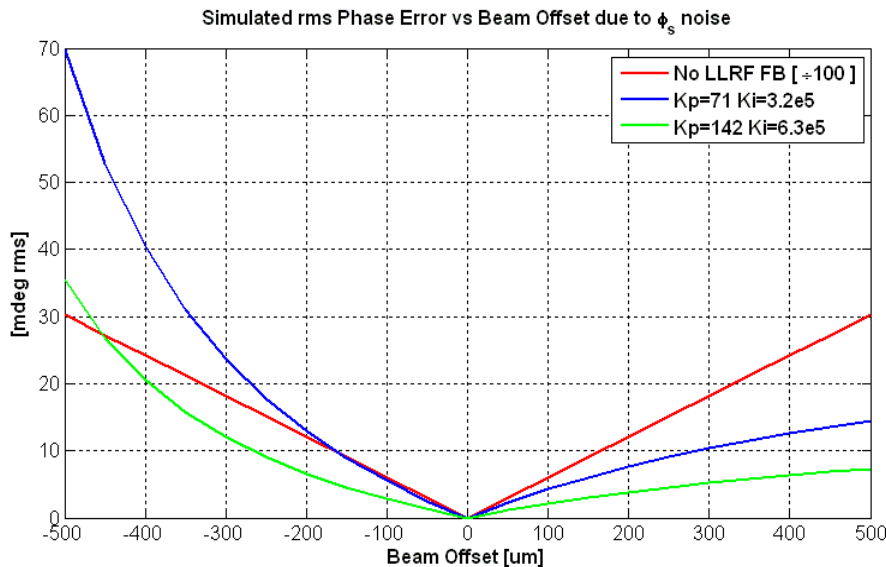


**Beam Loading is proportional to offset  
Cavity-to-cavity alignment errors cause  
differential beam-loading that will lead to  
differential phase noise**

**Standard cavity-to-cavity alignment = 500um  
Beyond APS-U, 4MV => 0.07deg spec**

**Means to reduce effect:**

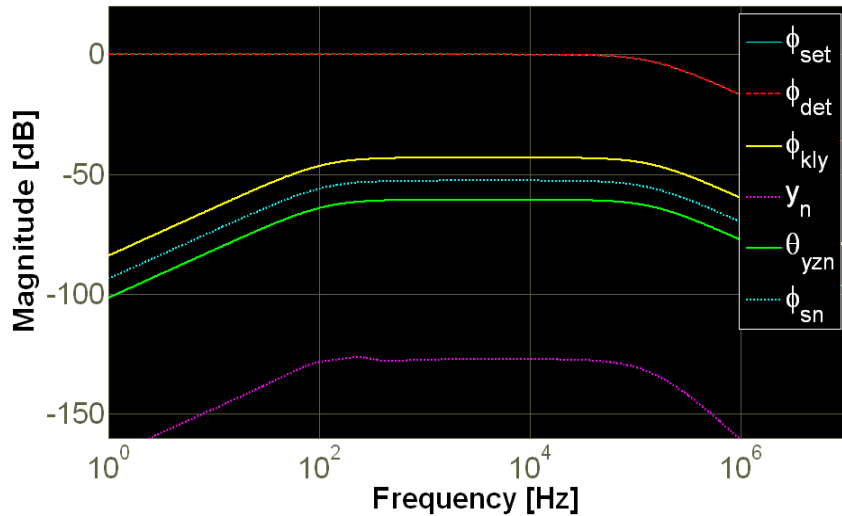
**improve cavity alignment, go to lower QL,  
reduce Storage Ring AM & PM noise**



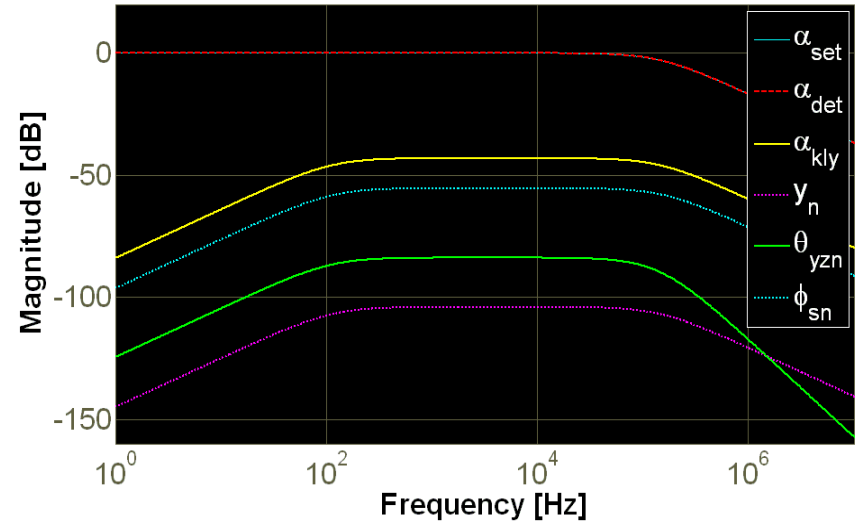
# Challenges and Strategy - Tools

- ... and dynamic small signal model will help track system noise & error budgets

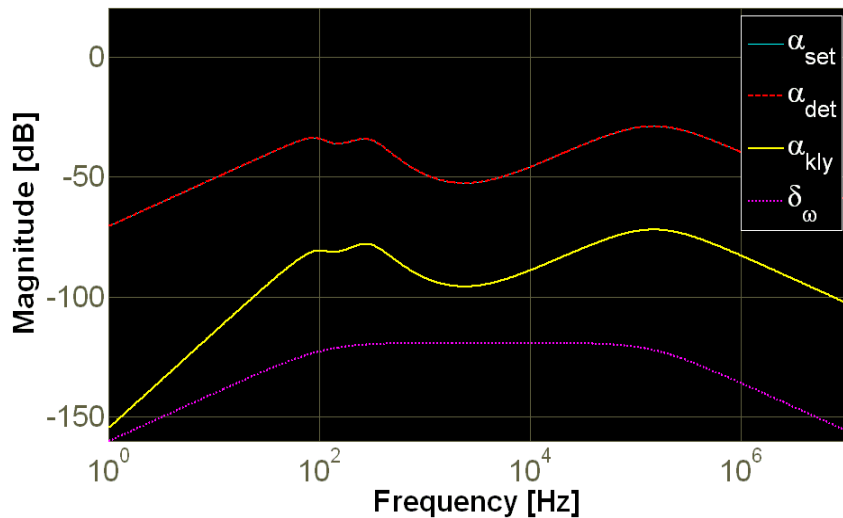
Phase Transfer Functions



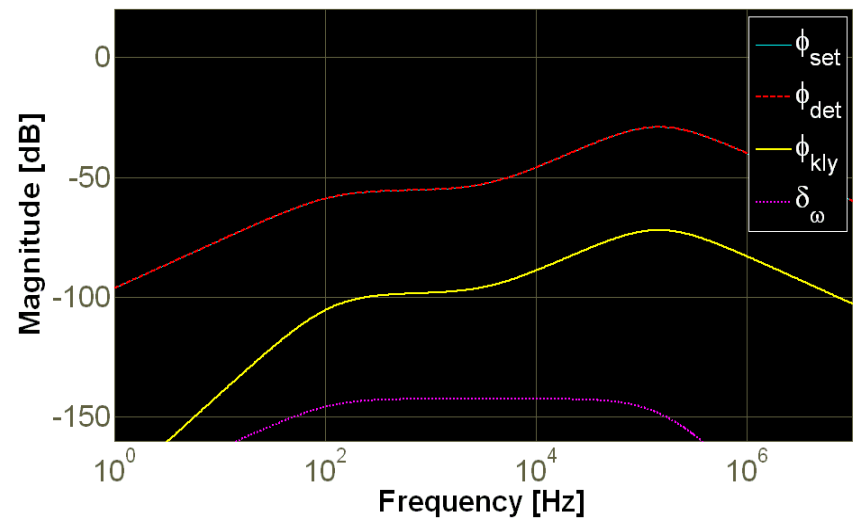
Amplitude Transfer Functions



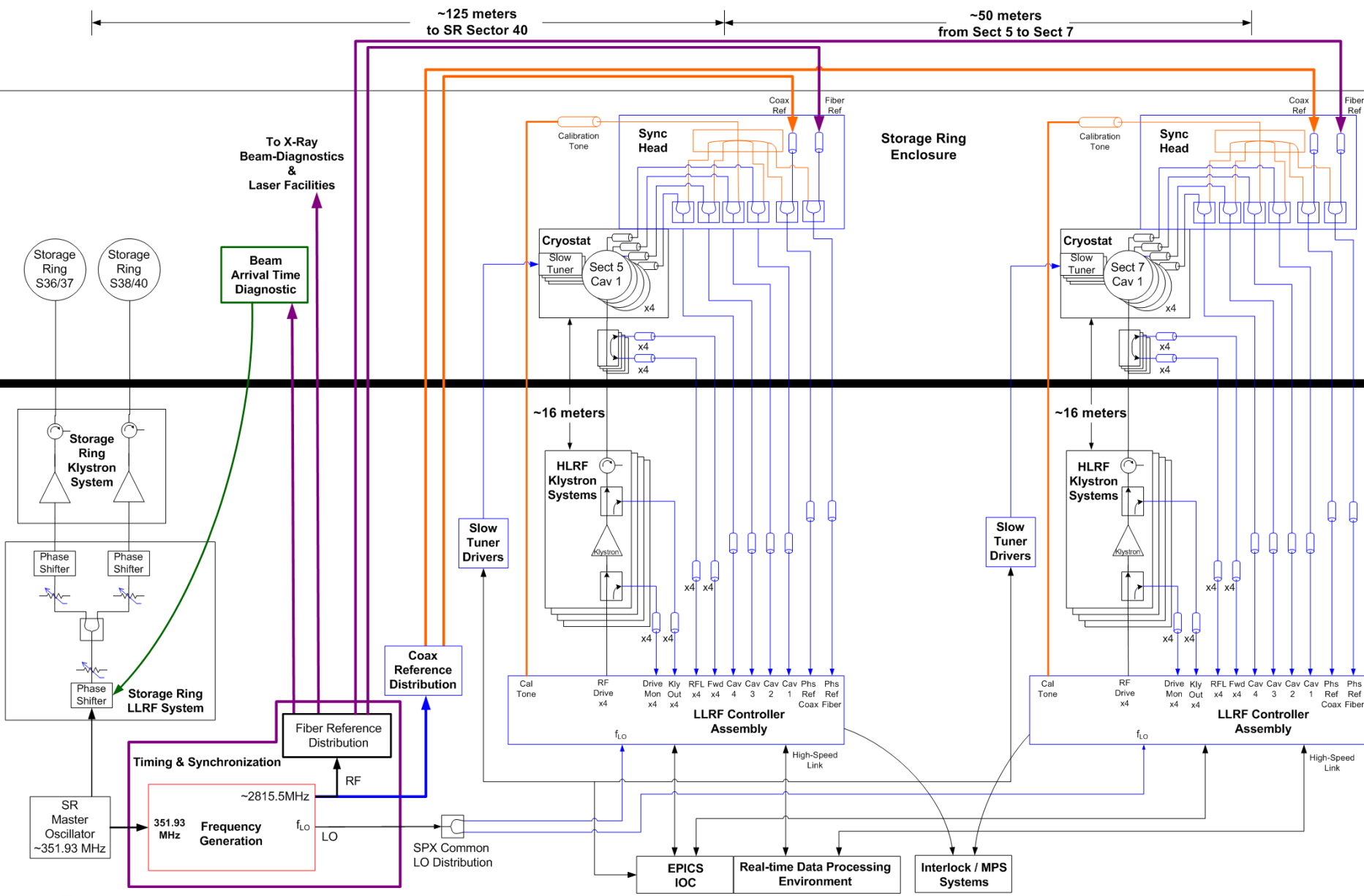
Phase Transfer Functions



Amplitude Transfer Functions

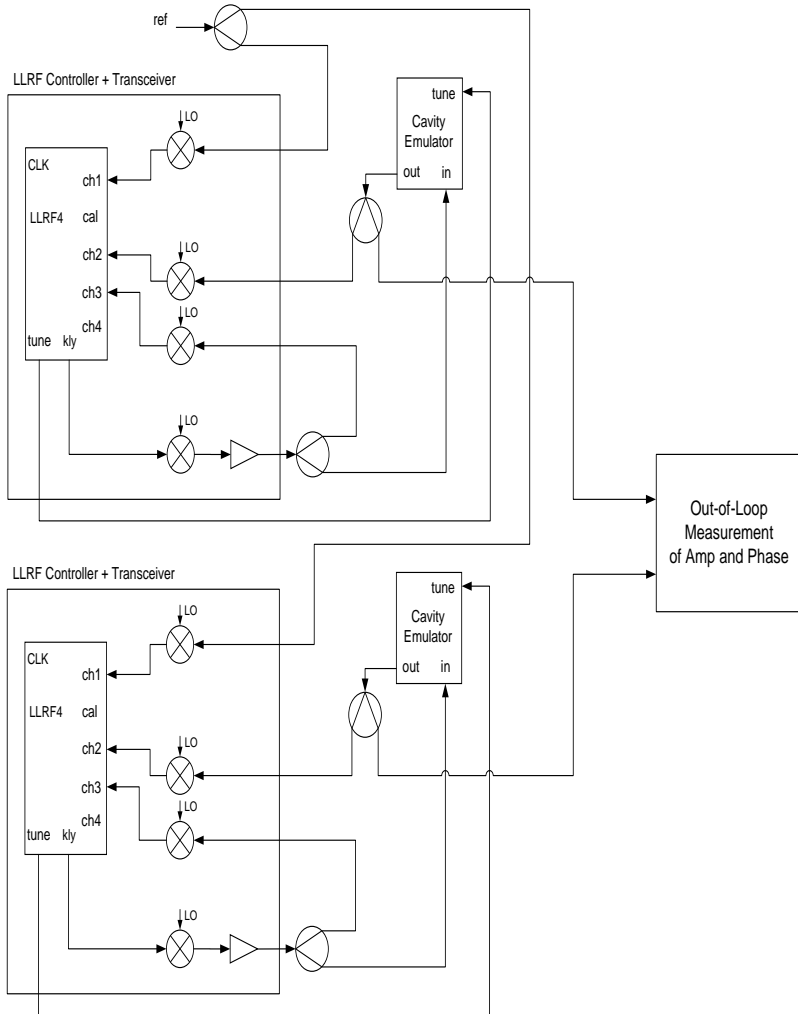


# Production System Concept (2 Sectors, 4 cav/sector)

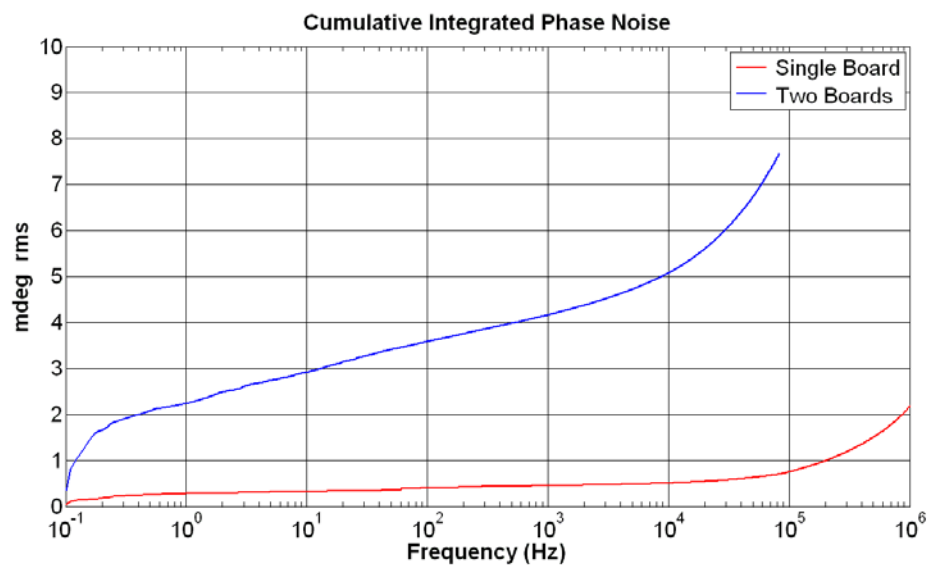
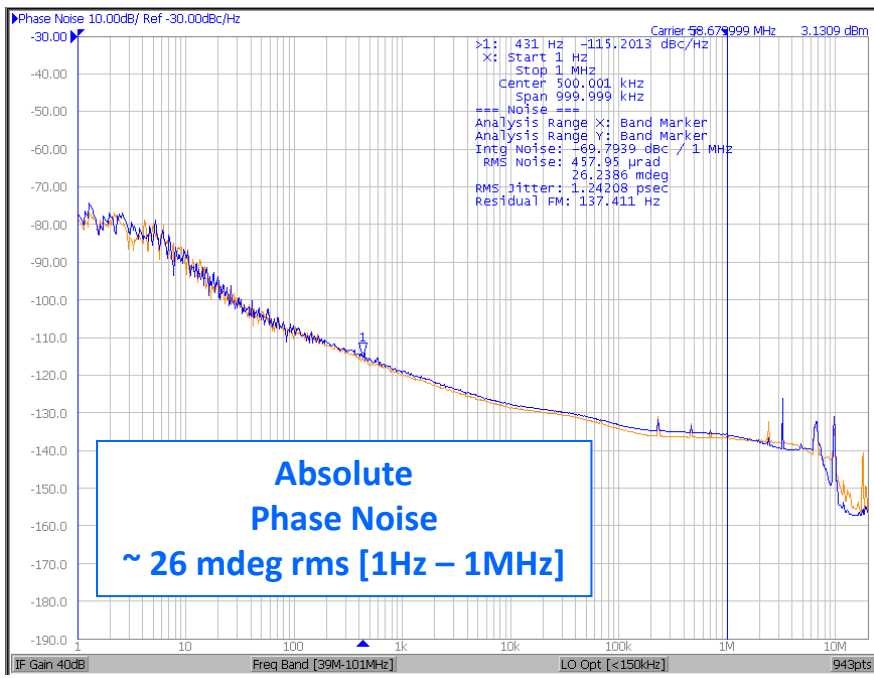
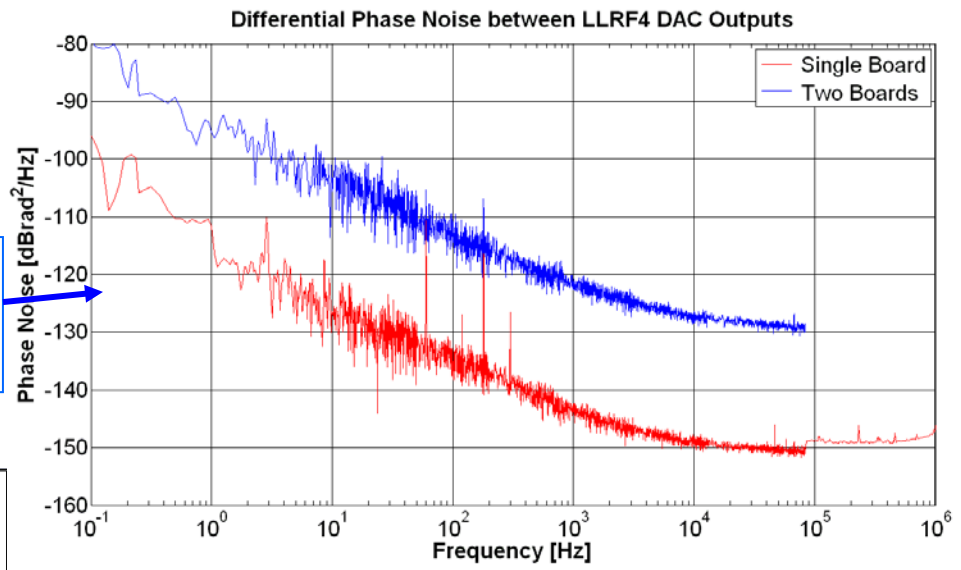
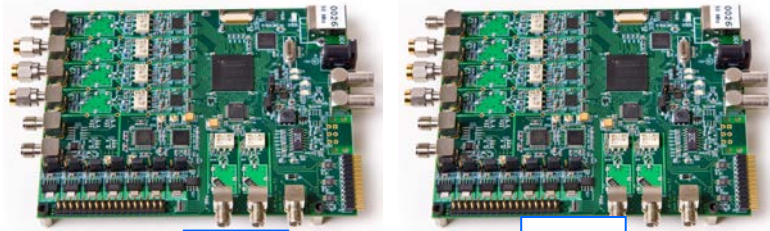




# Benchtop Demonstrations until Cavities become available



# Trivial Example of Common LO/CLK source Distribution

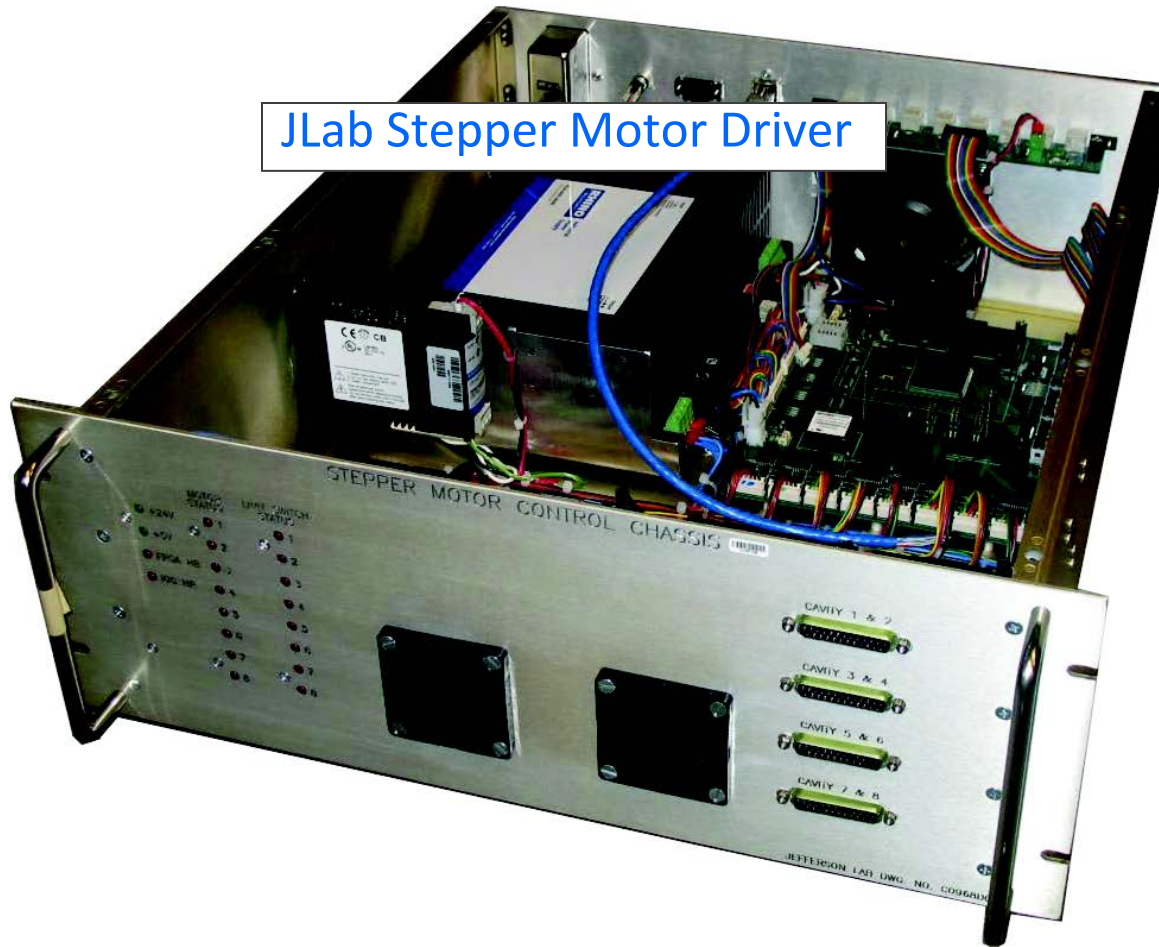


# R&D Period Highlights

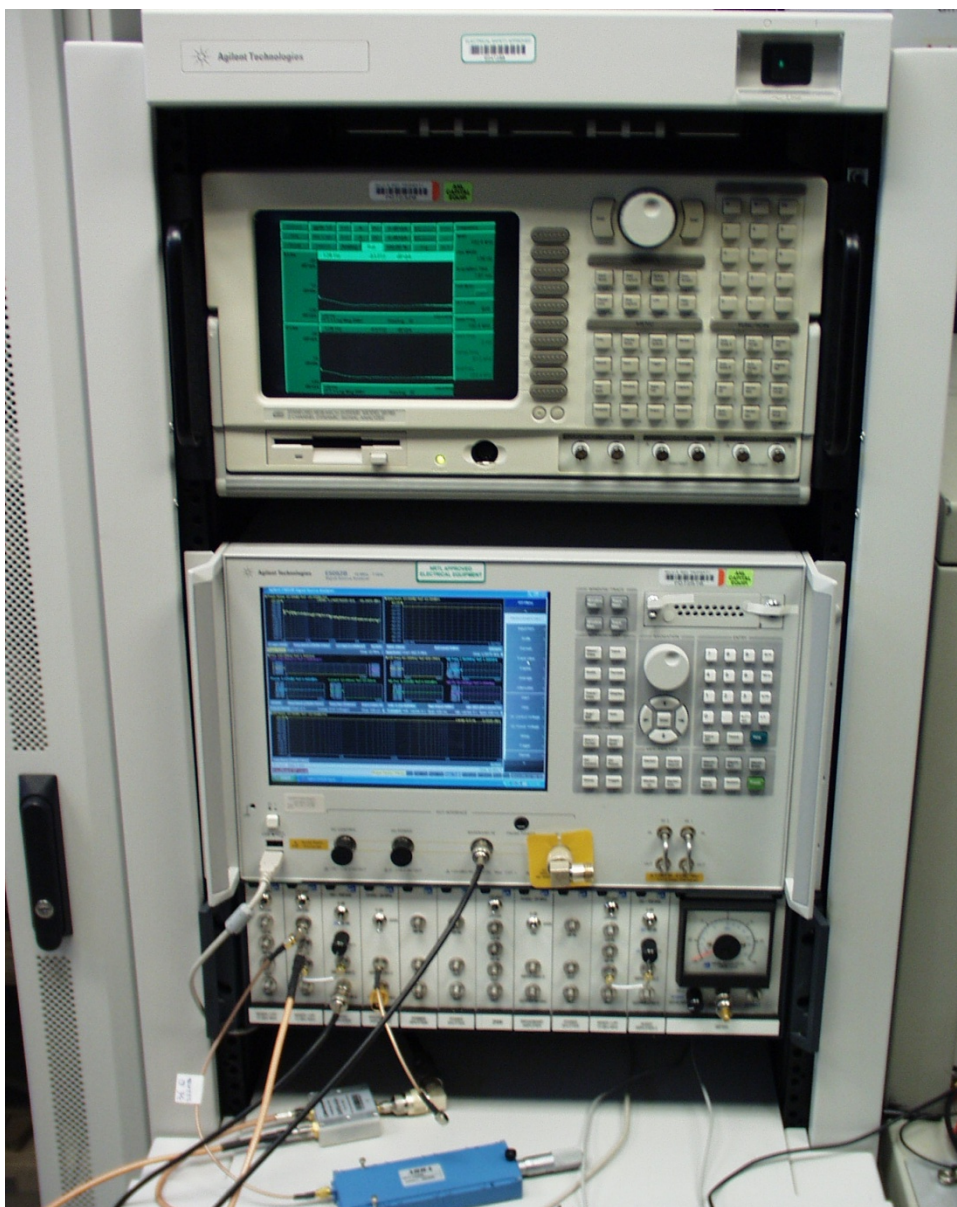
- Ultimate Goal: Demonstrate required rf stability performance on a 2-cavity single cryomodule system
- LBNL Collaboration - Phase I [3/11 – 10/11]
  - Study & report on differential stability between two high-Q cavity emulator systems
  - Delivery of first LLRF4 Chassis and Frequency Generation Chassis
  - ANL prepares to take ownership of LLRF4 based system & prepares tests of LLRF receiver chain
- LBNL Collaboration - Phase II [10/11 – 10/12] (joint with Timing/Synchronization)
  - Completion of LLRF4 based controllers for R&D program
  - Demo of timing/synchronization concepts between RF Cavity and User Laser
- Present LLRF R&D Timeline Overview
  - Receipt of first LLRF4 based system from LBNL [10/11]
  - Receipt of JLab slow tuner stepper motor driver [1/12]
  - Single cavity testing begins at ANL [2/12]
  - 2-cavity cryomodule testing begins at ANL [5/13]
  - 2-cavity in-ring test [begins 9/13]

# Stepper Motor Driver (x2 4-channel driver)

- SPX Cavity will use a scissors jack tuner similar to the JLab 12GeV Upgrade
  - Hence JLab will provide two 4-channel drivers similar to their existing design

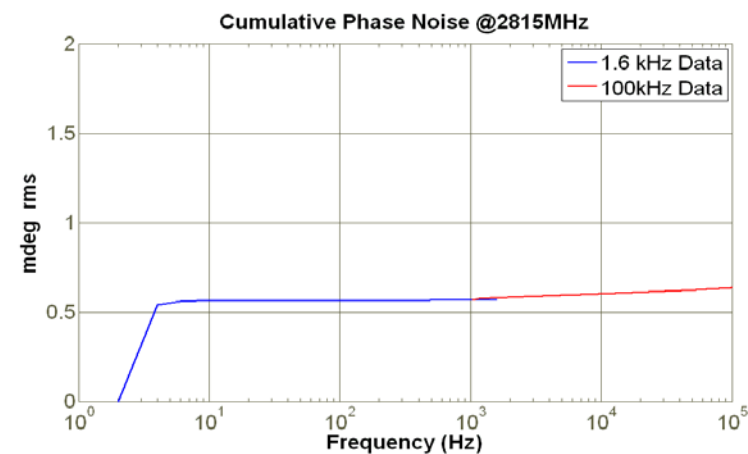
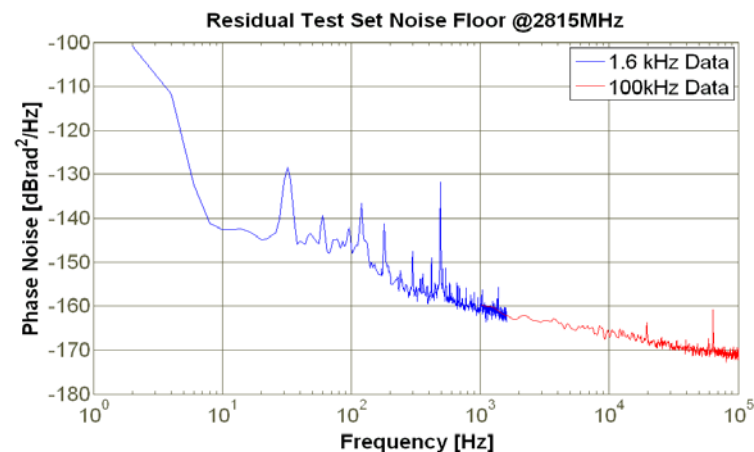


# Challenges and Strategy - Tools



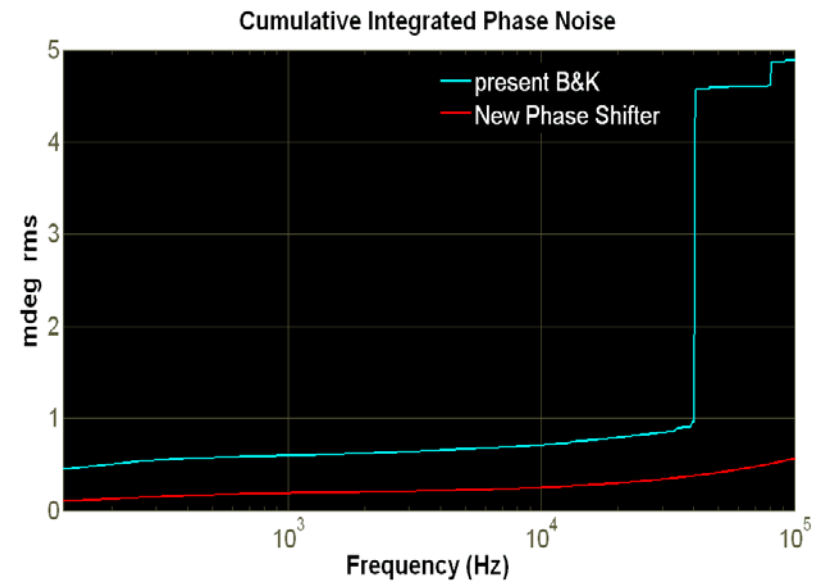
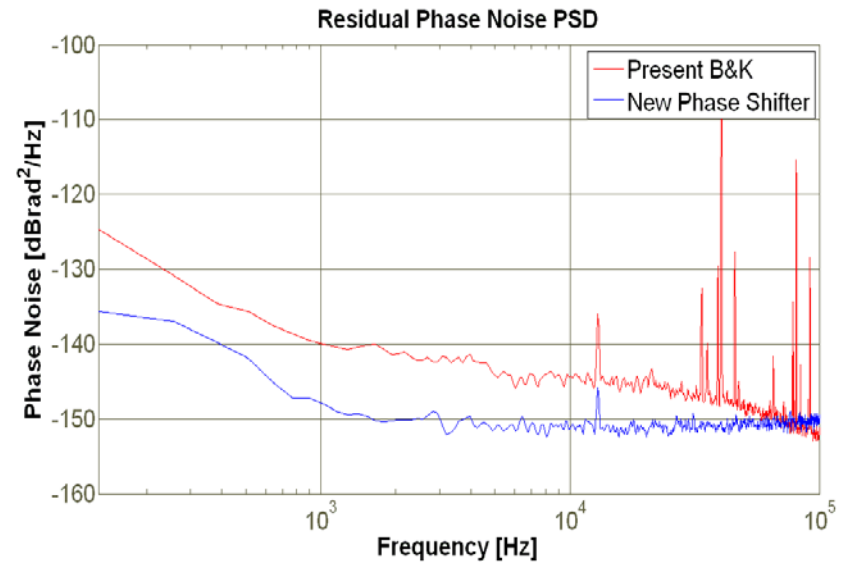
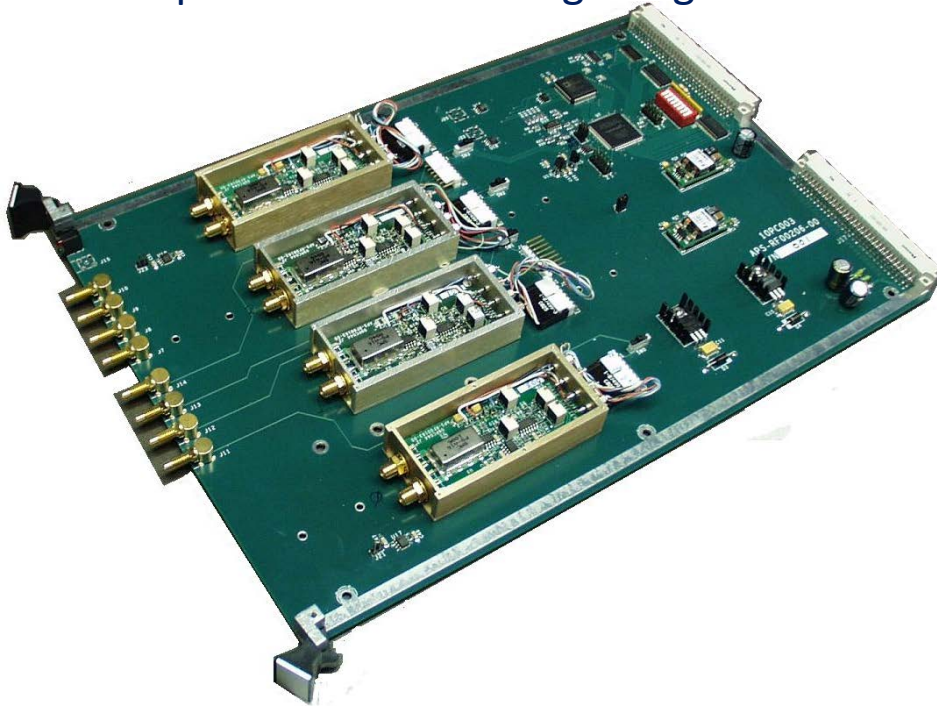
## Phase Noise Measurement Equipment

- Agilent Signal Source Analyzer for absolute phase and amplitude noise
- Wenzel residual noise test set



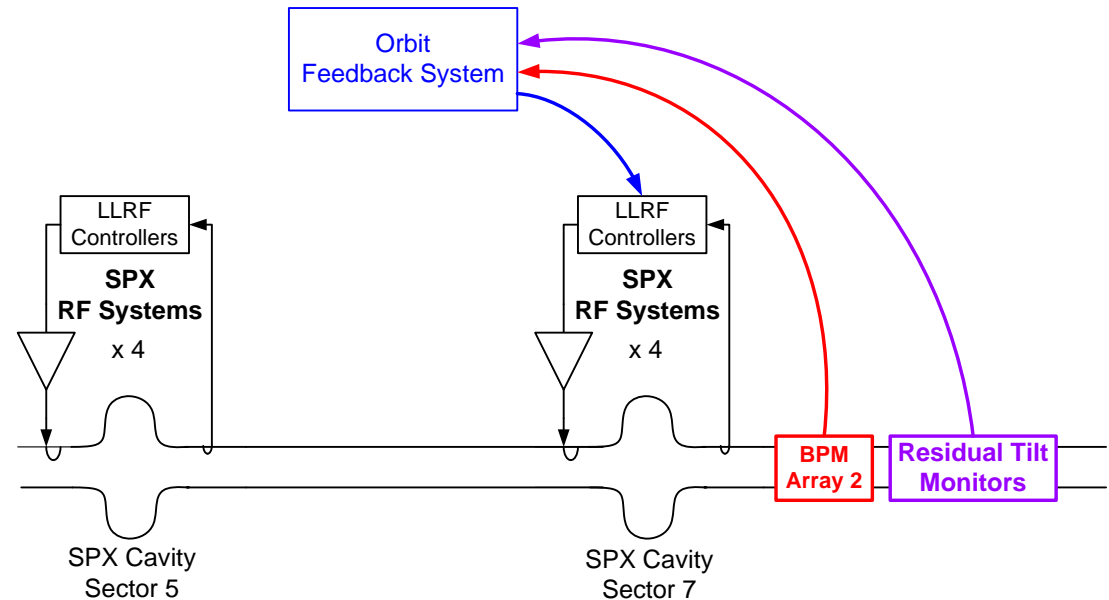
# Phase Shifter candidate for BAT-based feedback to Main Storage Ring 352 MHz RF

- To address common mode phase specs, beam arrival time monitor will feedback to phase of main storage ring 352 MHz rf



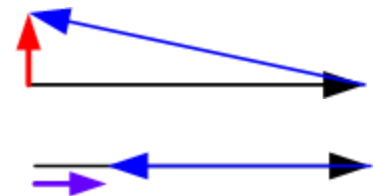
# Conceptual Design Strategy: Differential Specs

- Orbit Feedback System provides long-term stability ...
  - via Beam Position Monitor (BPM) Array 2 sets differential phase < 100(200) Hz
  - via Residual Tilt Monitors sets differential amplitude < 100(200) Hz
- LLRF System on its own > 10 Hz
  - 10 Hz – 100(200) Hz overlap with Orbit Feedback



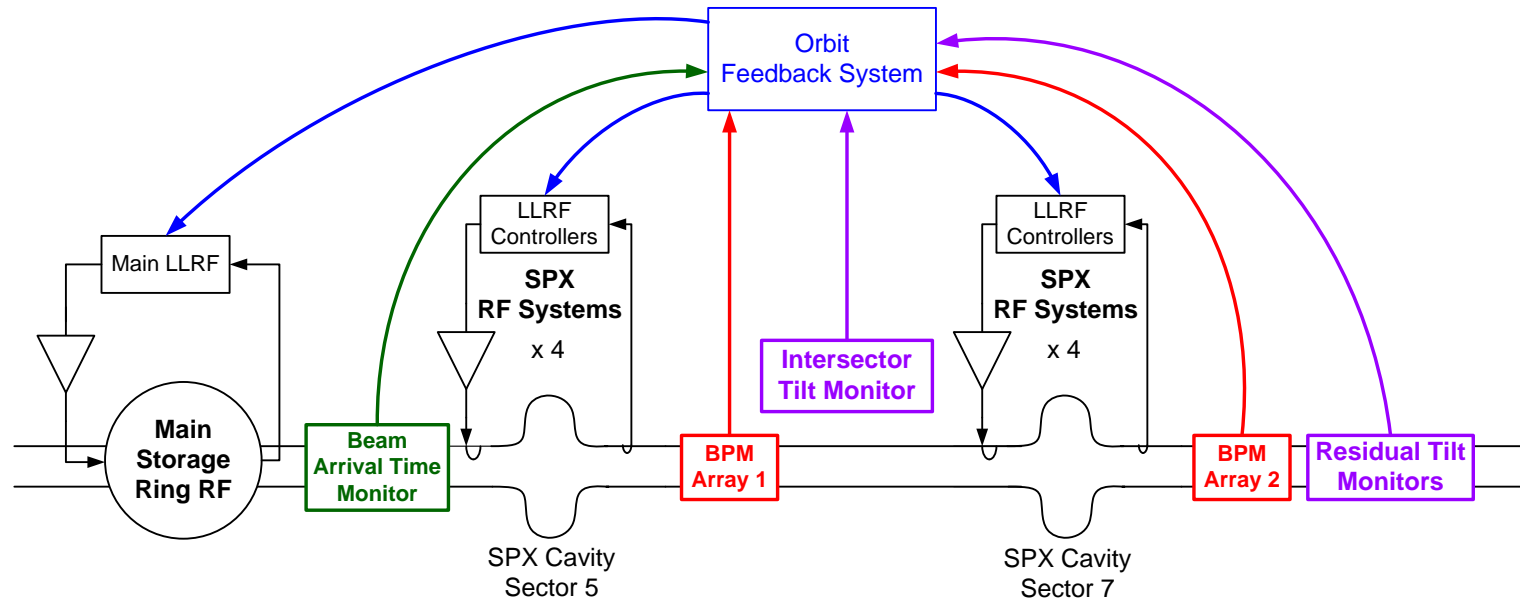
**BPM Array 2:** sets phase of Sector 7

**Residual Tilt Monitors:** sets amplitude of Sector 7



# Conceptual Design Strategy: Common Mode Specs

- Main storage ring rf used to lock beam to master osc. via Beam Arrival Time diagnostic
- SPX follows master oscillator, orbit feedback...
  - via BPM Array 1 sets common mode phase < 100(200) Hz
  - via Intersector Tilt Monitor sets common mode amp < 100(200) Hz
  - **LLRF on its own > 10 Hz**



**BPM Array 1:** sets phase of Sector 5

**BPM Array 2:** sets phase of Sector 7

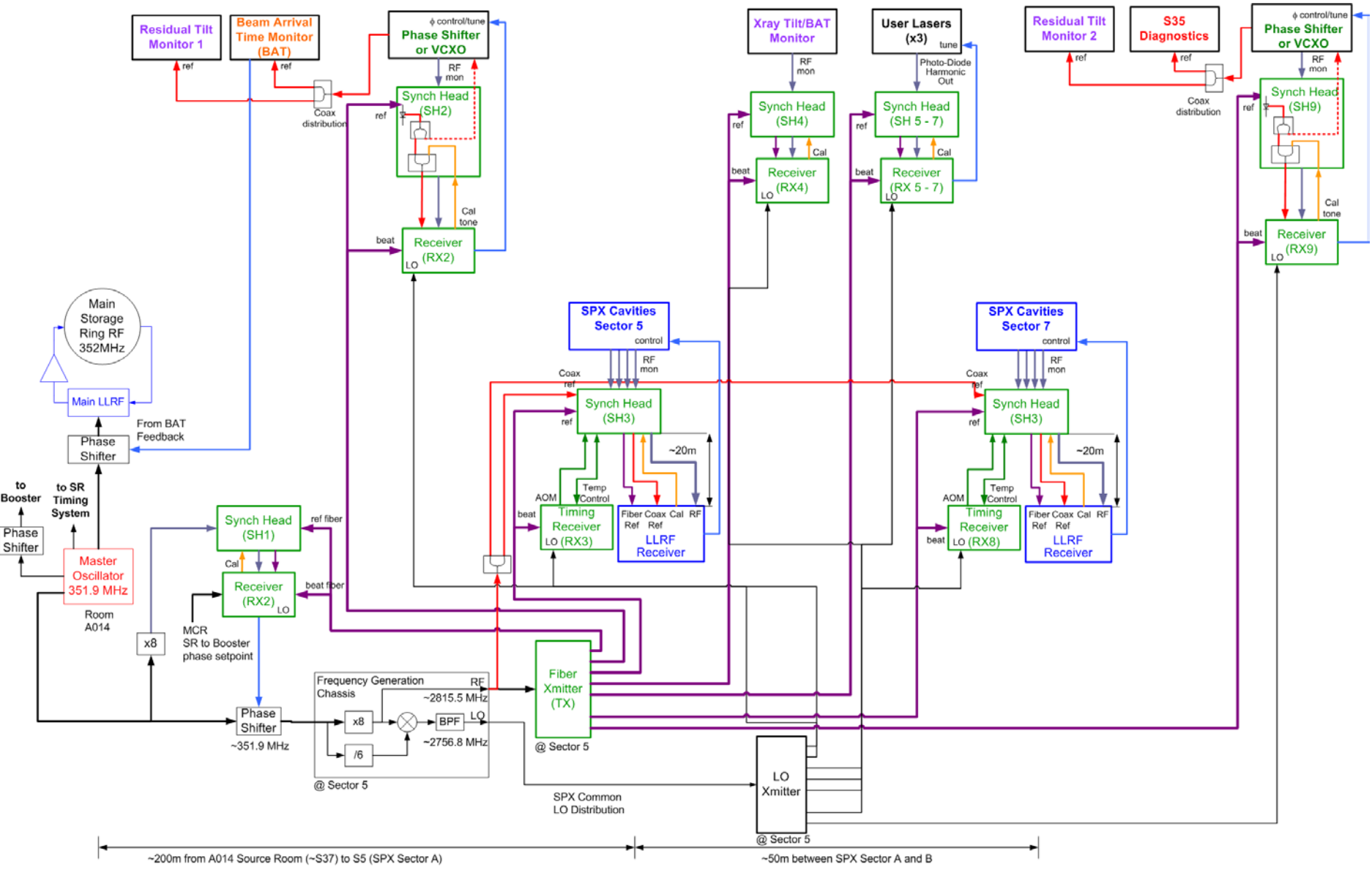
**Intersector Tilt Monitor:** sets amplitude of Sector 5

**Residual Tilt Monitors:** sets amplitude of Sector 7

**Beam Arrival Time Monitor:** sets phase of Main Storage Ring RF

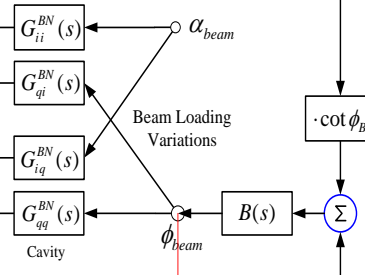
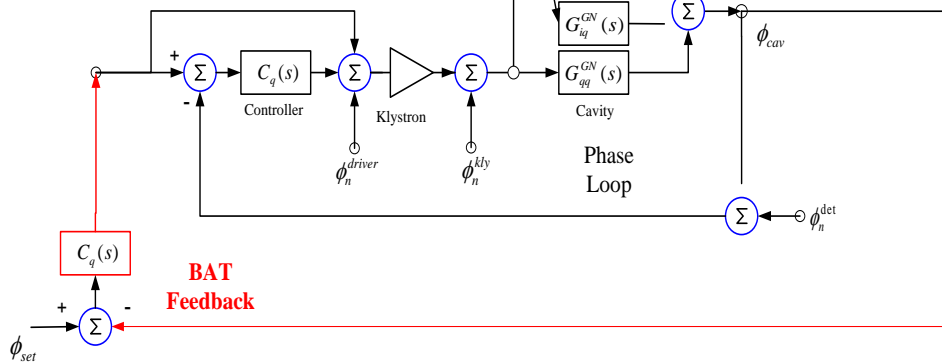
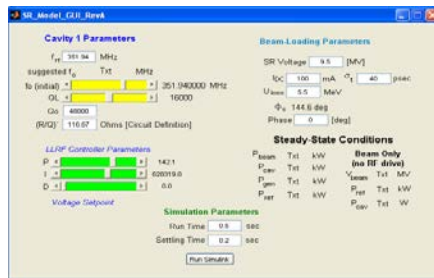
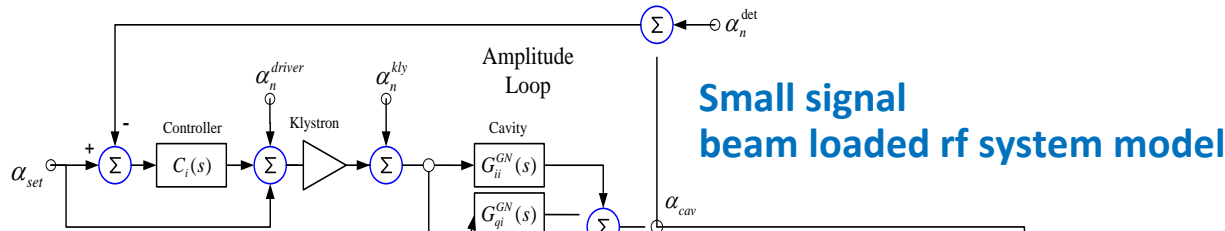




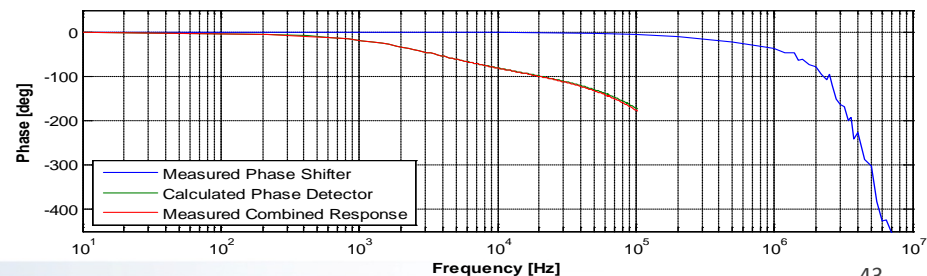
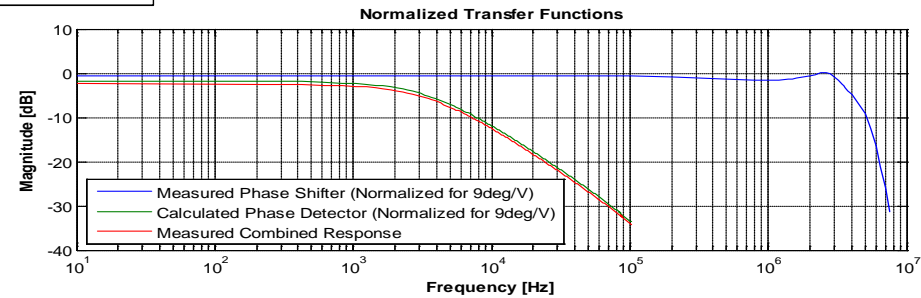


# Challenges and Strategy - Tools

- Developing small signal models for main storage ring rf to aid introduction of BAT feedback loop



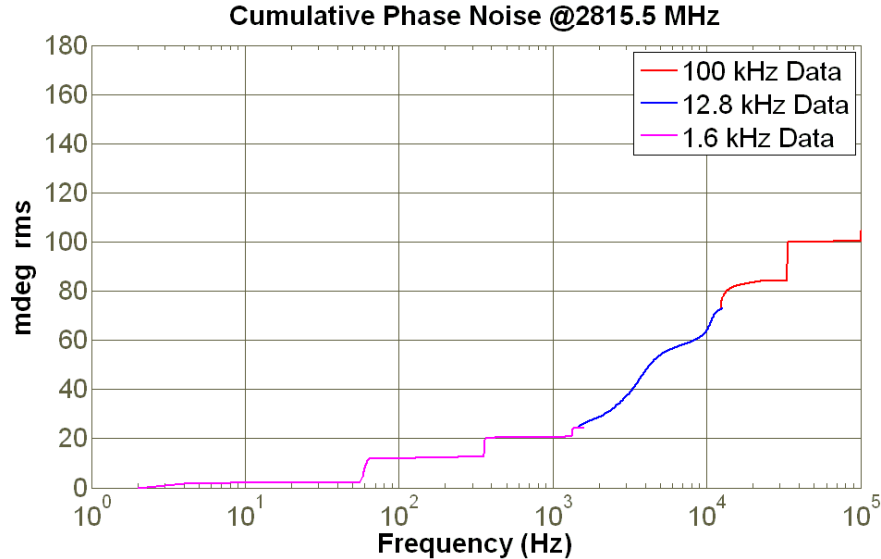
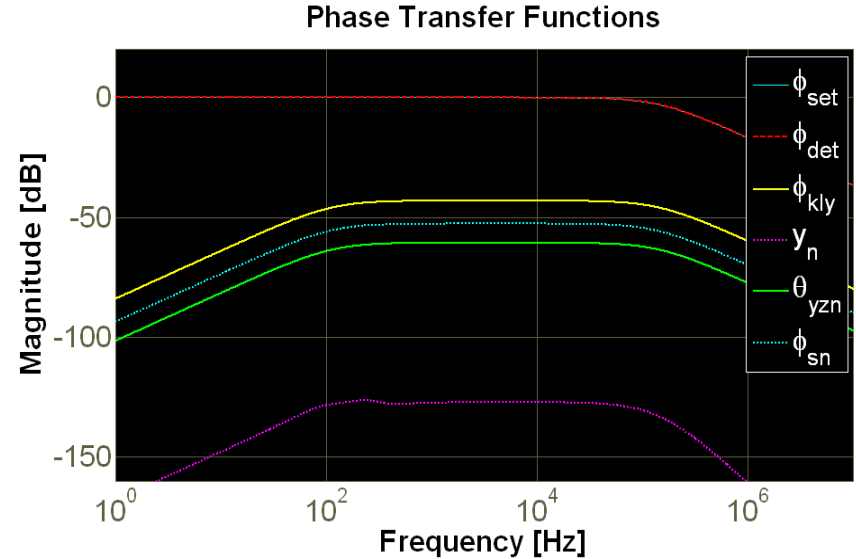
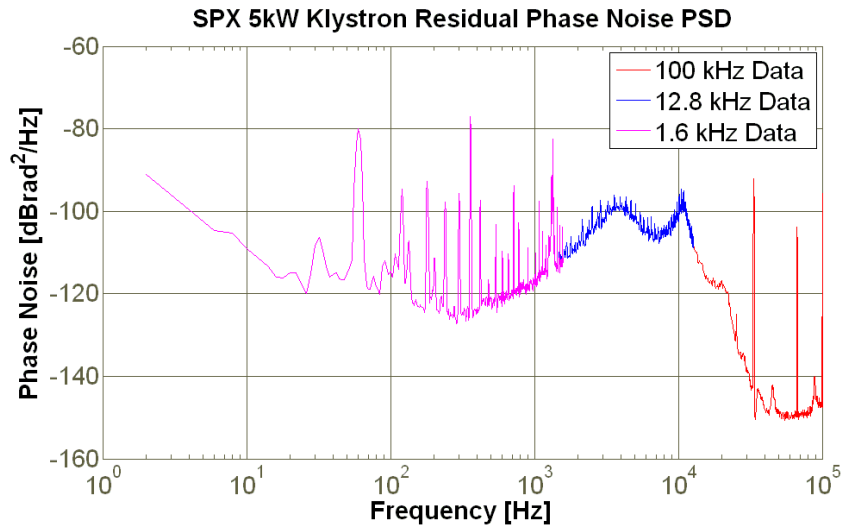
## Measured Phase Shifter & Phase Detector Transfer Functions



# Initial Error Budgeting

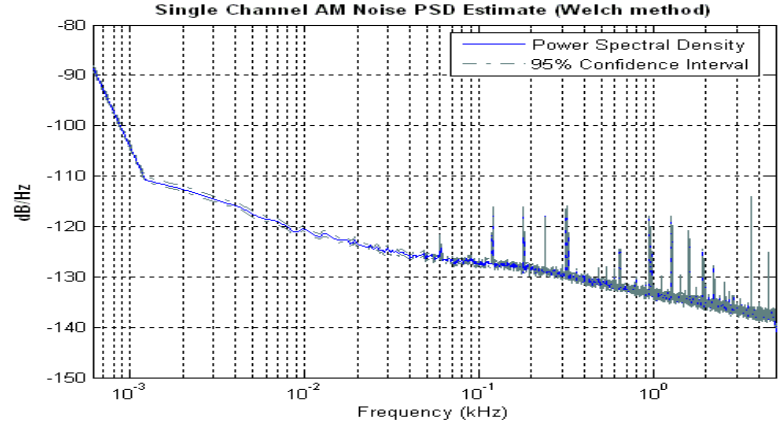
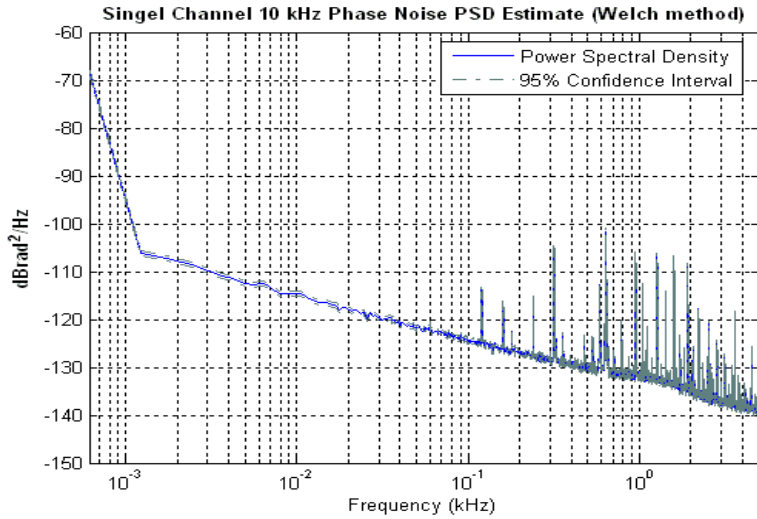
|    | Error/Noise Source <sup>[4]</sup>   | Phase Noise<br>Common Mode<br>[deg rms] <sup>[2]</sup> | Phase Noise<br>Differential Mode<br>[deg rms] <sup>[2] [3]</sup> | Amp Noise<br>Common Mode<br>[% rms] | Amp Noise<br>Differential Mode<br>[% rms] |
|----|---|--|--|-------------------------------------|---|
|    | <b>Total Budget</b>   | <b>4</b>   | <b>0.18</b>  | <b>1</b>                            | <b>1.1</b>                                |
| 2  | Frequency Generation Chassis (SPX)  | 0.1  | N/A  | N/A                                 | N/A                                       |
| 3  | Phase Ref. Distribution   | 0.1  | 0.016  | N/A                                 | N/A                                       |
| 4  | LLRF Receiver Chain   | 0.1  | 0.016  | 0.1                                 | 0.11                                      |
| 5  | Cavity Field Probe Cabling  | 0.1  | 0.016  | 0.1                                 | 0.11                                      |
| 6  | LLRF Transmitter & Control Algorithm<br>(up-conversion process including LO Distribution)   | 0.1  | 0.016  | 0.1                                 | 0.11                                      |
| 7  | <b>Klystron + Driver Amp</b>  | <b>0.1</b>   | <b>0.016</b>   | <b>0.1</b>                          | <b>0.11</b>                               |
| 8  | Microphonics  | 0.1  | 0.016  | 0.1                                 | 0.11                                      |
| 9  | Beam-Loading Offset Noise   | 0.1  | 0.016  | 0.1                                 | 0.11                                      |
| 10 | Beam-Loading Tilt Noise   | 0.1  | 0.016  | 0.1                                 | 0.11                                      |
| 11 | Beam-Loading Synchronous Phase Noise  | 0.1  | 0.016  | 0.1                                 | 0.11                                      |
| 12 | AM-to-PM Cross Modulation   | 0.1  | 0.016  | N/A                                 | N/A                                       |
| 13 | PM-to-AM Cross Modulation   | N/A  | N/A  | 0.1                                 | 0.11                                      |
| 14 | Orbit Feedback Process [outside SPX zone]<br>(differential phase correction)  | N/A  | 0.016  | N/A                                 | N/A                                       |
| 15 | Orbit Feedback Process [inside SPX zone]<br>(common mode phase correction)  | 0.1  | N/A  | N/A                                 | N/A                                       |
| 16 | Storage Ring Beam Jitter <sup>[1]</sup><br>with Beam Arrival Time Feedback Process<br>(including 352MHz MO & RF system noise)                                     | 2.7  | N/A  | N/A                                 | N/A                                       |
| 17 | Residual Tilt Feedback [outside SPX zone]<br>long-term differential amplitude correction  | N/A  | N/A  | N/A                                 | 0.11                                      |
| 18 | Intersector Tilt Feedback Process [inside SPX zone]<br>common mode amplitude set-point  | N/A  | N/A  | 0.1                                 | N/A                                       |
|    |   |  |  |                                     |   |
|    | # of processes competing for differential phase =   | 11   |  |                                     |   |
|    | # of processes competing for common mode phase =  | 13   |  |                                     |   |
|    | # of processes competing for differential amp =   | 10   |  |                                     |   |
|    | # of processes competing for common mode amp =  | 10   |  |                                     |   |
|    | Notes:  |  |  |                                     |   |
|    | [1] existing measurements, but this is expected to be reduced by BAT feedback   |  |  |                                     |   |
|    | [2] no account is taken for these processes being independent, the level to which they are independent contributes to the safety margin                           |  |  |                                     |   |
|    | [3] no account is taken for differential noise processes that are truly independent from cavity to cavity which will contribute an inherent sqrt(8) safety margin |  |  |                                     |   |
|    | [4] resultant contribution from each process = process noise source x transfer function   |  |  |                                     |   |

# Klystron Residual Phase Noise Measurements

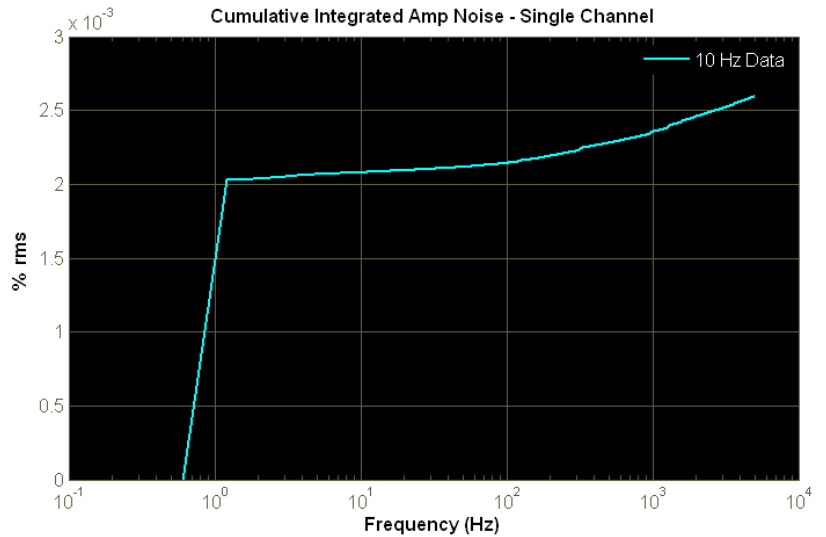
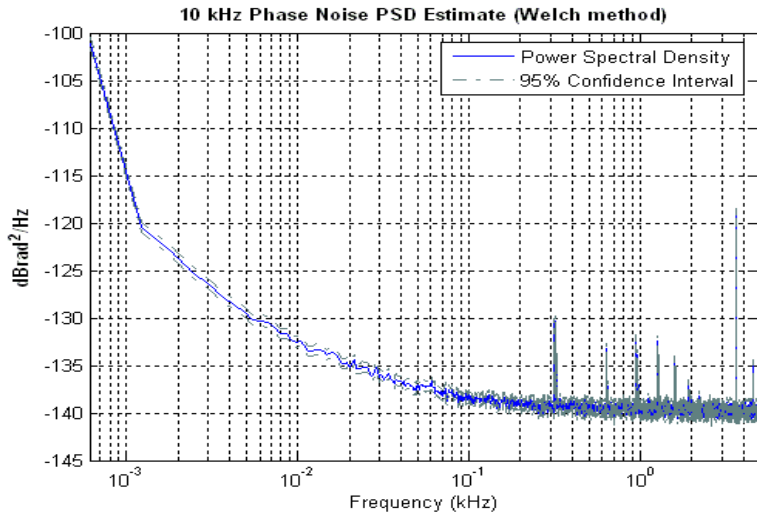


**Klystron residual phase noise = 100mdeg**  
**Expect this to be suppressed by at least 20dB**  
**(factor of 10) to ~10mdeg rms**

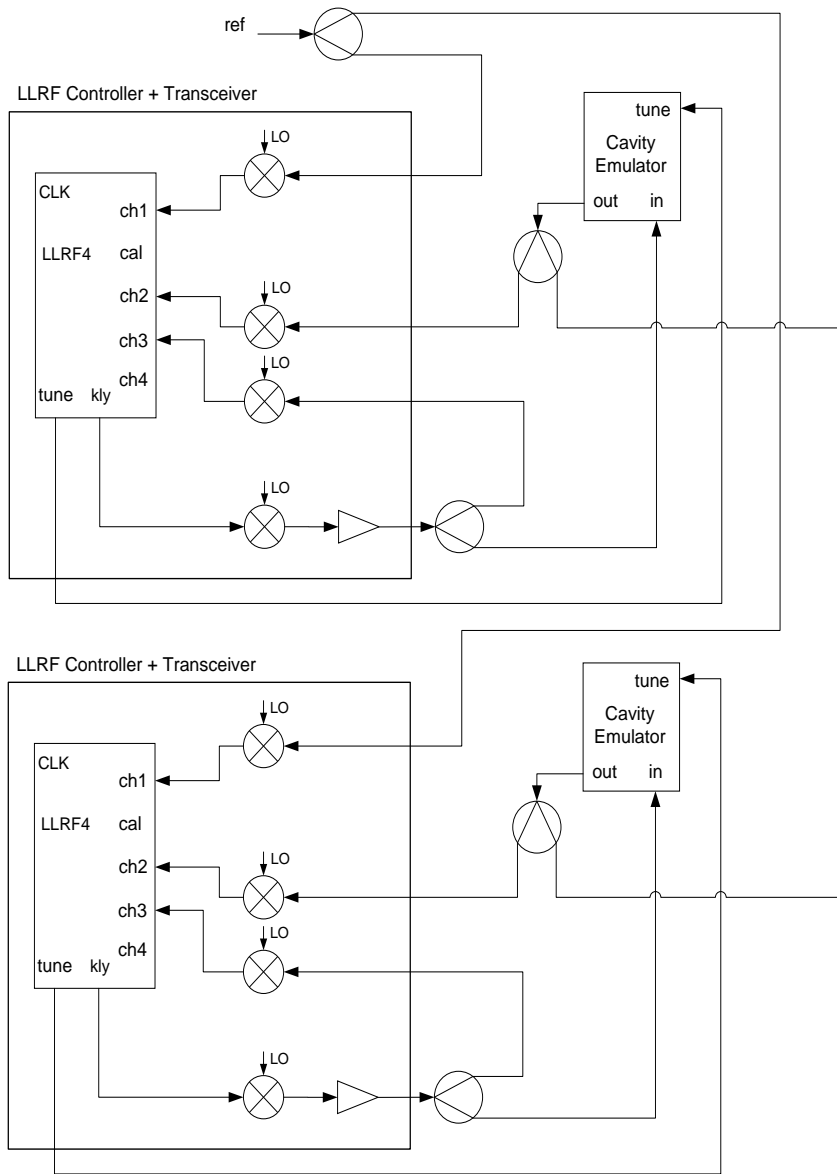
# LLRF4 Noise



Assume -135dB/Hz over 1e6 bandwidth =  
~0.02% rms



# LLRF R&D Plan - LBNL Collaboration



LLRF control of 2 high-Q cavity system emulators

- Analog cavity emulators allow for LLRF development independent of cavity production schedule
- Study & report on differential stability
- Build up of LLRF4 based controllers to support 2-cavity R&D program

Out-of-Loop  
Measurement  
of Amp and Phase

$$f_{IF} = \frac{2815.5}{48} \cong 58.7 \text{ MHz}$$

$$f_{LO} = \frac{47}{48} \cdot 2815.5 \cong 2756.8 \text{ MHz}$$

$$f_{ADC} = \frac{f_{LO}}{36} \cong 76.6 \text{ MSPS}$$

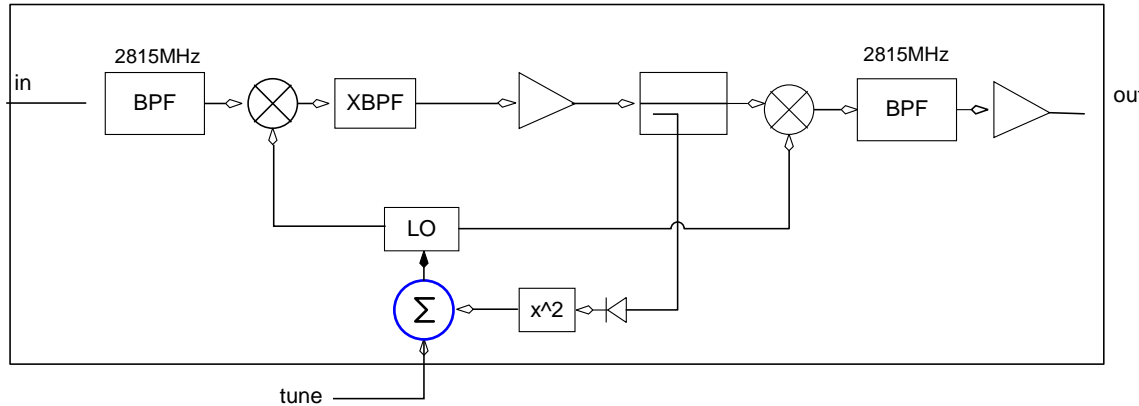
$$f_{DAC} = 2f_{ADC} \cong 153.2 \text{ MSPS}$$

$$\frac{f_{alias}}{f_{ADC}} = \frac{11}{47}$$

$$\frac{f_{bunch}}{f_{ADC}} = \frac{4}{47}$$

# LLRF R&D Plan - BenchTop Demonstrations

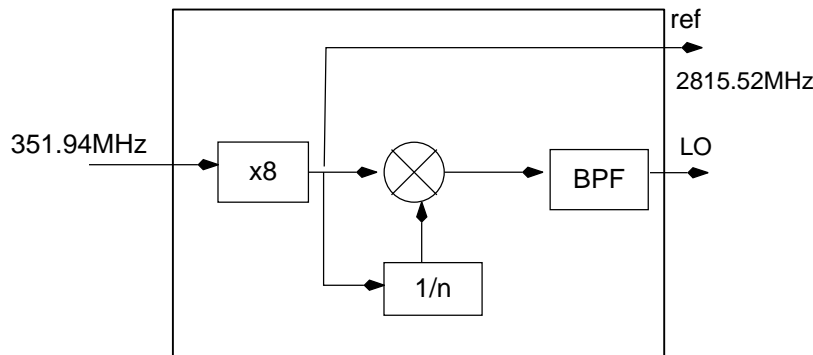
Cavity Emulator



## Cavity Emulators

- Allow for LLRF development independent of initial cavity production schedule
- Add VCO-based LO to simulate Lorentz detuning & tuning control

Reference and LO



$$f_{IF} = \frac{2815.5}{48} \cong 58.7 \text{ MHz}$$

$$f_{LO} = \frac{47}{48} \cdot 2815.5 \cong 2756.8 \text{ MHz}$$

$$\frac{f_{alias}}{f_{ADC}} = \frac{11}{47}$$

$$f_{ADC} = \frac{f_{LO}}{36} \cong 76.6 \text{ MSPS}$$

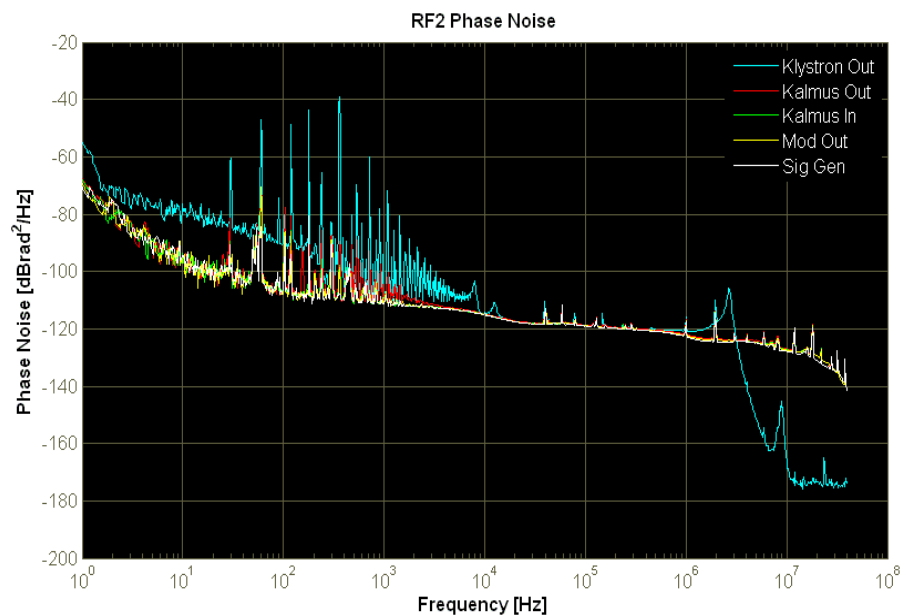
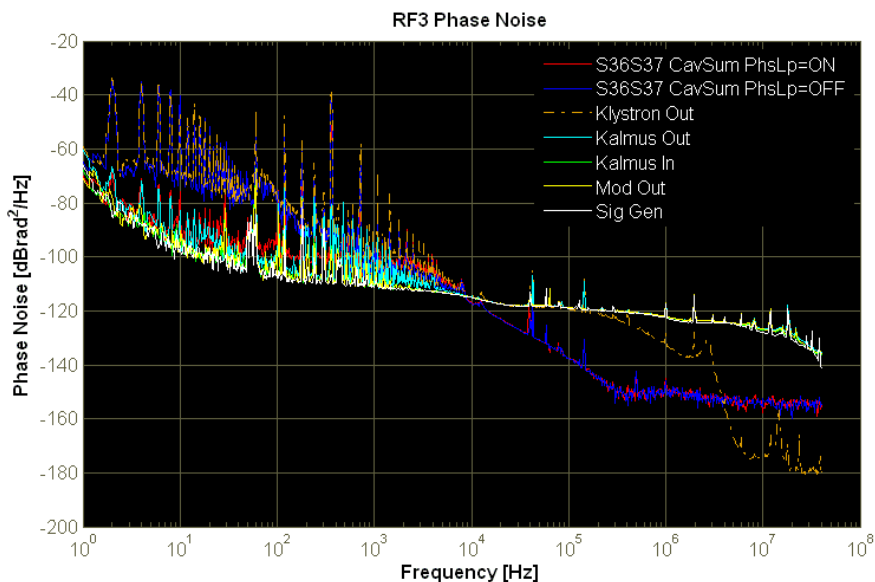
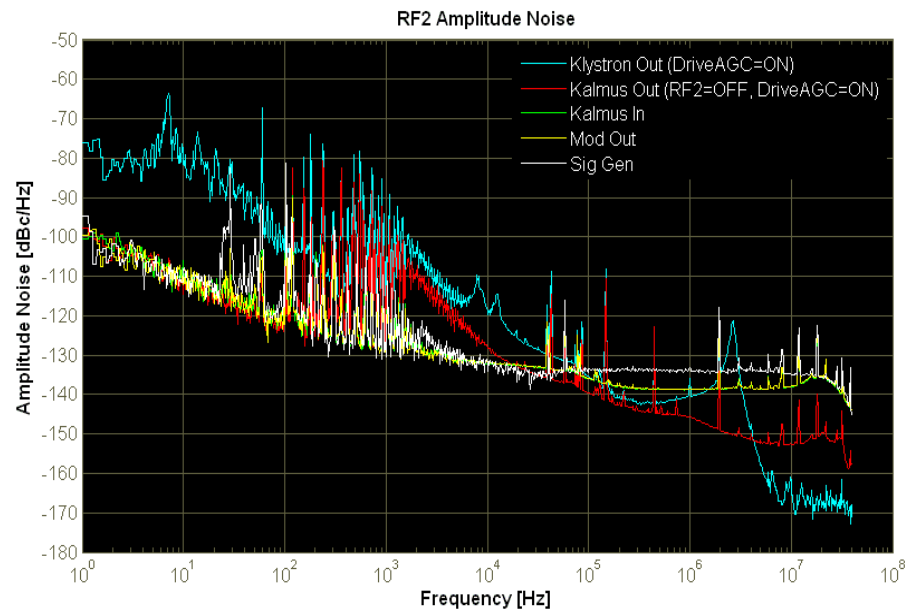
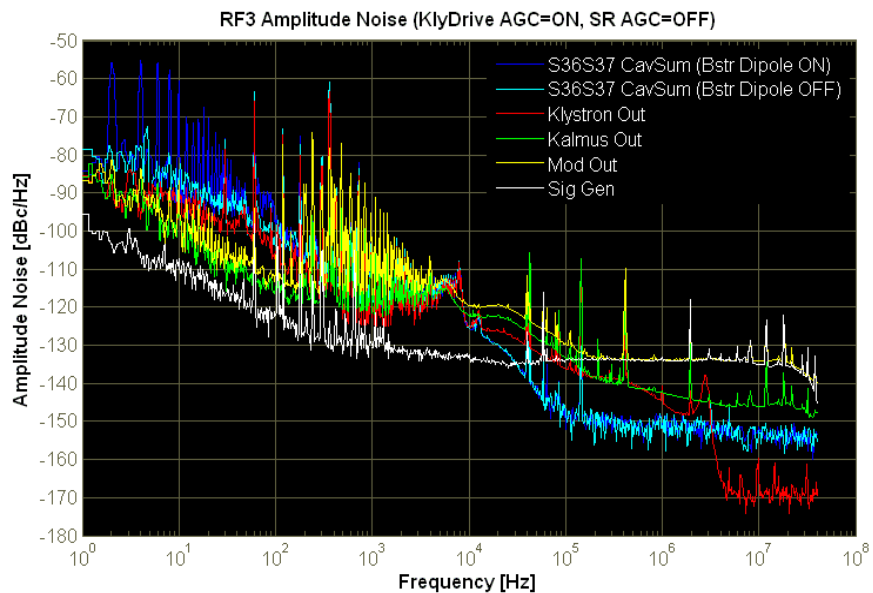
$$\frac{f_{bunch}}{f_{ADC}} = \frac{4}{47}$$

$$f_{DAC} = 2f_{ADC} \cong 153.2 \text{ MSPS}$$

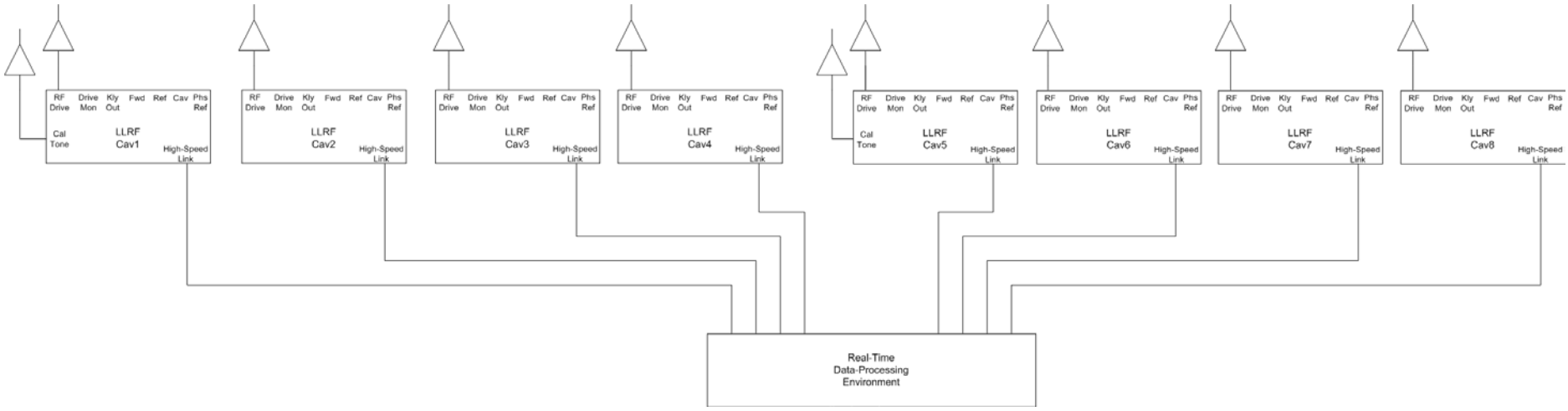
## Frequency Plan has considered the following:

- Direct synthesis, clock generation input frequencies, ADC & DAC clock needs, SNR degradation concerns for 2-point processing, separating harmonics due to non-linearities, clock jitter vs. sensible S-band filters in choice of IF frequency, bunch spacing considerations

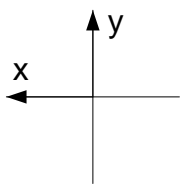
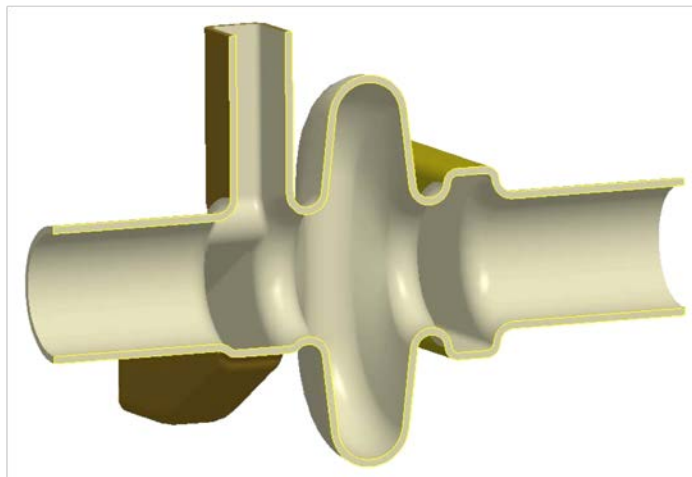
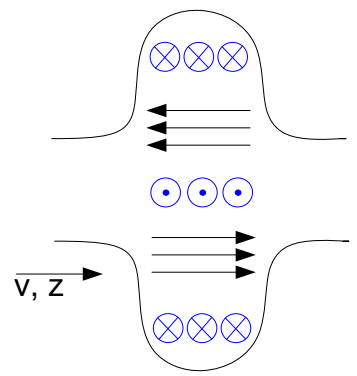
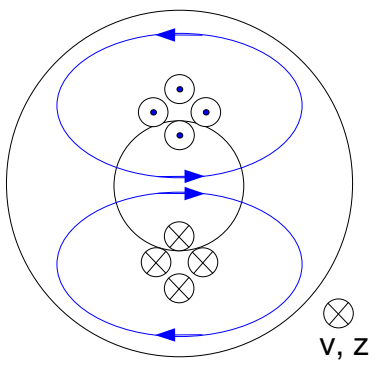




| Signal                         | Condition               | Integrated Jitter / Phase Noise<br>[1 Hz - 100 kHz] Bandwidth |                                     |
|--------------------------------|-------------------------|---|-------------------------------------|
|                                |                         | Jitter<br>(psec RMS)  | Phase Noise<br>@352MHz<br>(deg RMS) |
| 352 MHz Source                 | N/A                     | 0.280   | 0.036                               |
| S36+S37 Cav Sum <sup>(3)</sup> | Both Phase Loops OPEN   | 19.219  | 2.435                               |
|                                | Both Phase Loops CLOSED | 2.726   | 0.345                               |
| S38+S40 Cav Sum <sup>(4)</sup> | Both Phase Loops OPEN   | 16.047  | 2.033                               |
|                                | Both Phase Loops CLOSED | 0.952   | 0.121                               |



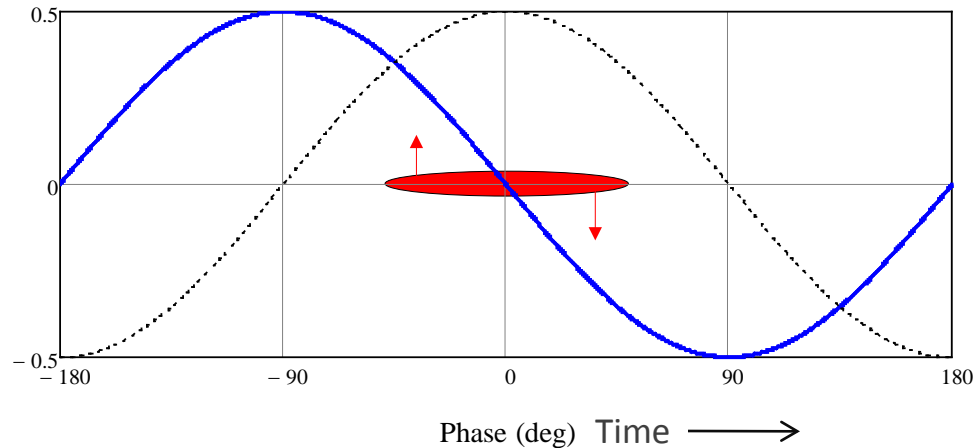
# Beam Loading



$V_Z(y) = V_m \cdot y$  Longitudinal voltage

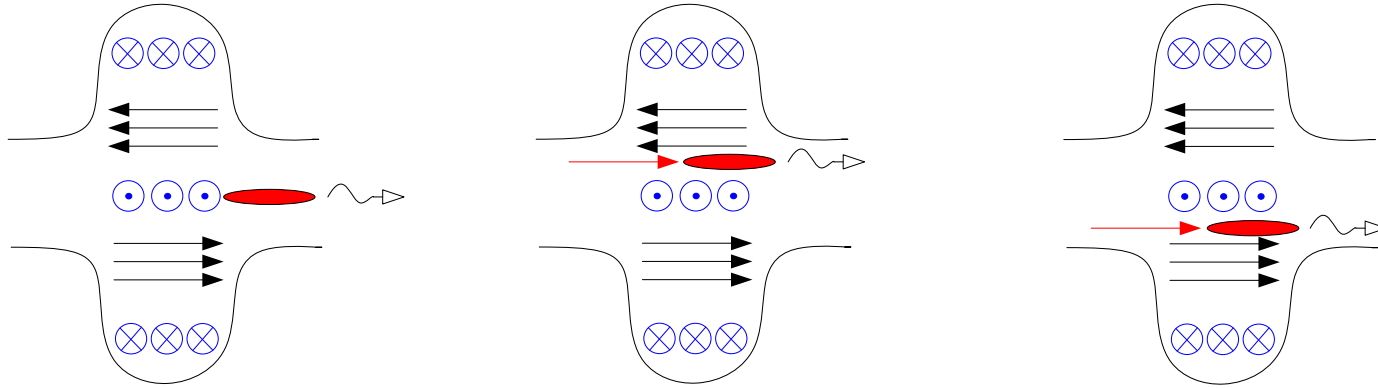
$V_t = j \frac{V_m}{K_o}$  Vertical deflecting voltage

— Magnetic Field  
— Electric Field



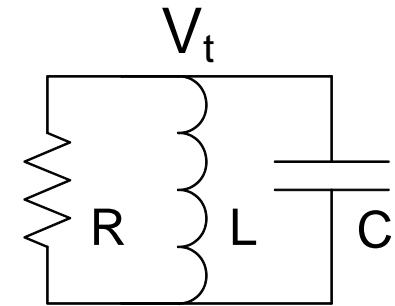
— Cavity Transverse Voltage  
- - - Cavity Longitudinal Voltage /  $\kappa_o$  ( $y > 0$ )

# Beam Loading



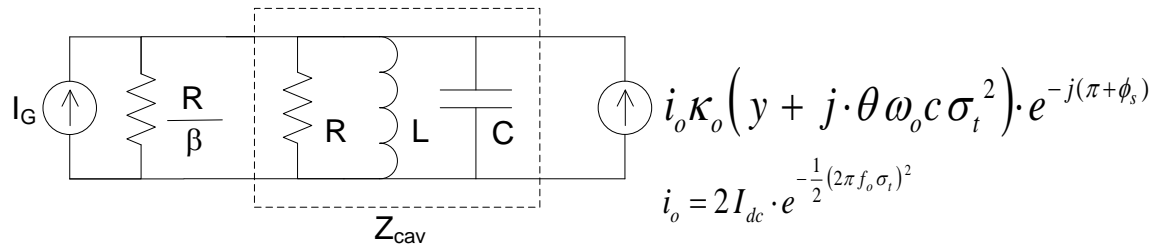
Dipole loss factor:  $k_{\perp} \equiv \frac{U_{loss}}{q^2} = \frac{|V_Z(y)|^2}{4U} = \frac{\omega_r}{2} \left( \frac{R}{Q} \right)' (\kappa_o y)^2$

Circuit definition R/Q:  $\left( \frac{R}{Q} \right)' = \frac{V_t^2}{2\omega_r U} = 17.8 \Omega$

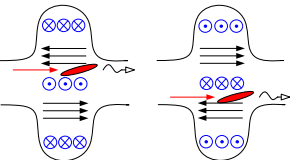


$$U_{loss} = q^2 k_{\perp} = \frac{1}{2} C V_t^2 \quad \Rightarrow V_t^2 = \left( \frac{q \cdot \kappa_o y}{C} \right)^2 \quad \Rightarrow q_{eq} = |q \cdot \kappa_o y|$$

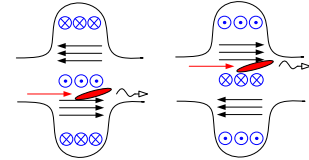
# Deflecting Cavity Beam Loading



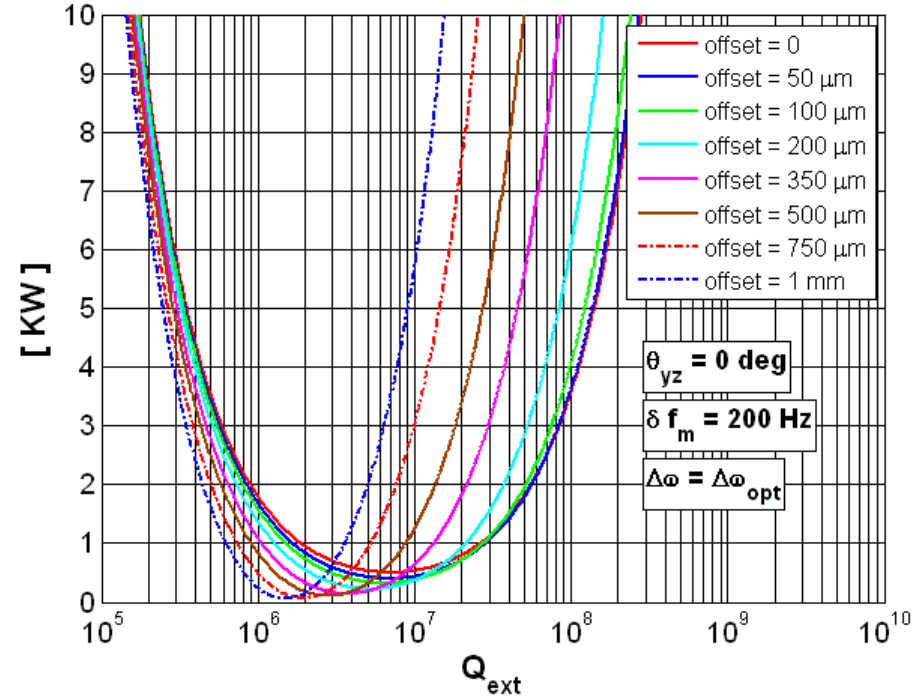
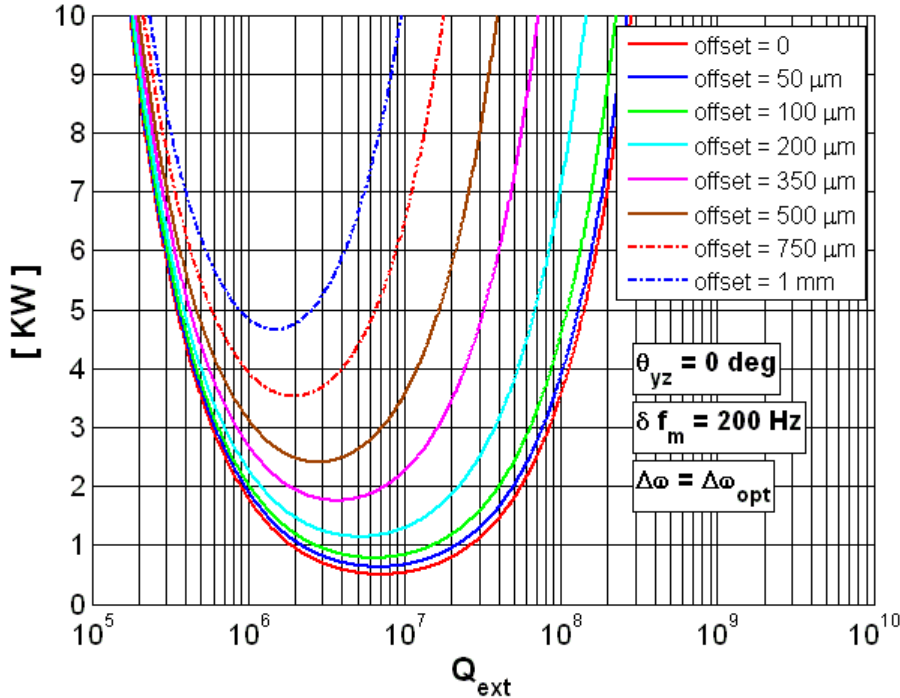
$$P_s^+ = \frac{V_t^2}{8\beta(R/Q)'Q_o} \cdot \left[ \left( \beta + 1 + \frac{P_B}{P_{cav}} \right)^2 + \left( 2Q_o \frac{(\Delta f + \delta f_m)}{f_r} + \frac{P_B}{P_{cav}} \tan \phi_s \right)^2 \right]$$



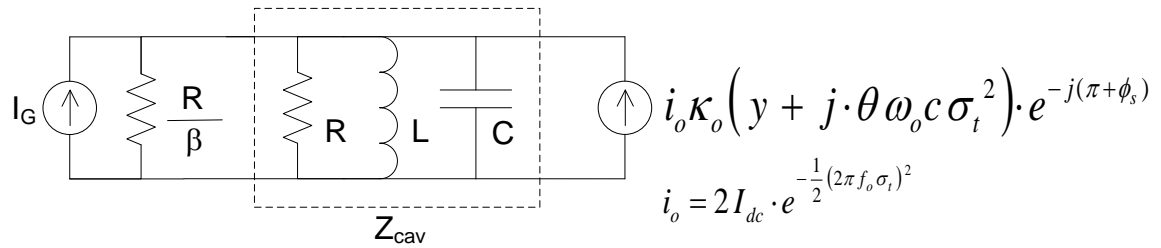
$V_t \cdot y > 0$



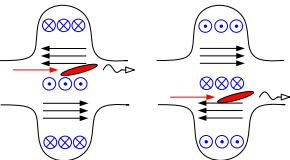
$V_t \cdot y < 0$



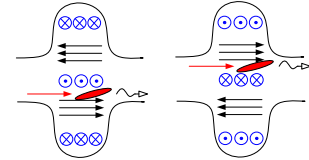
# Deflecting Cavity Beam Loading



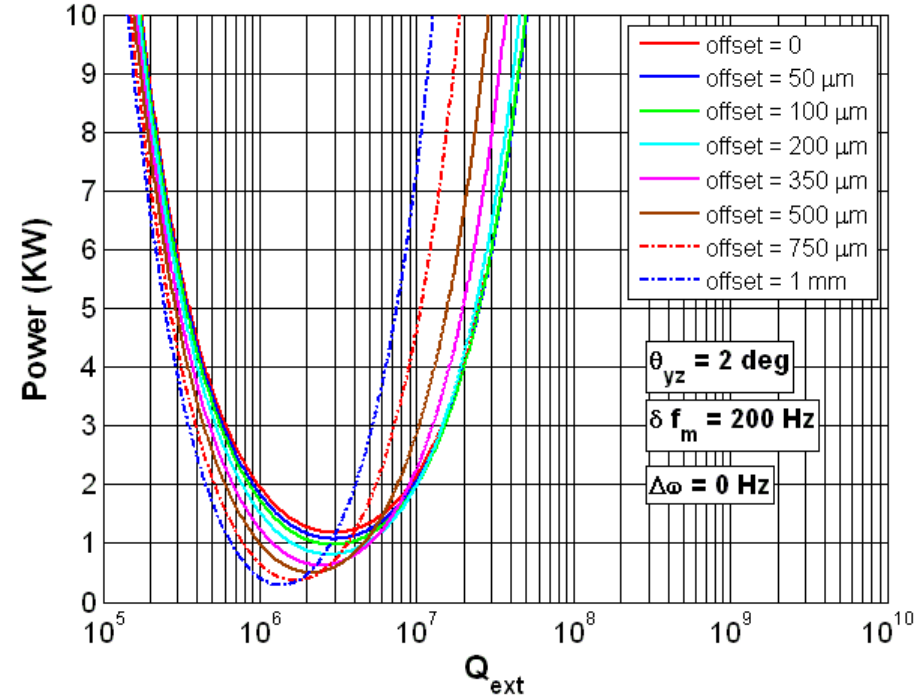
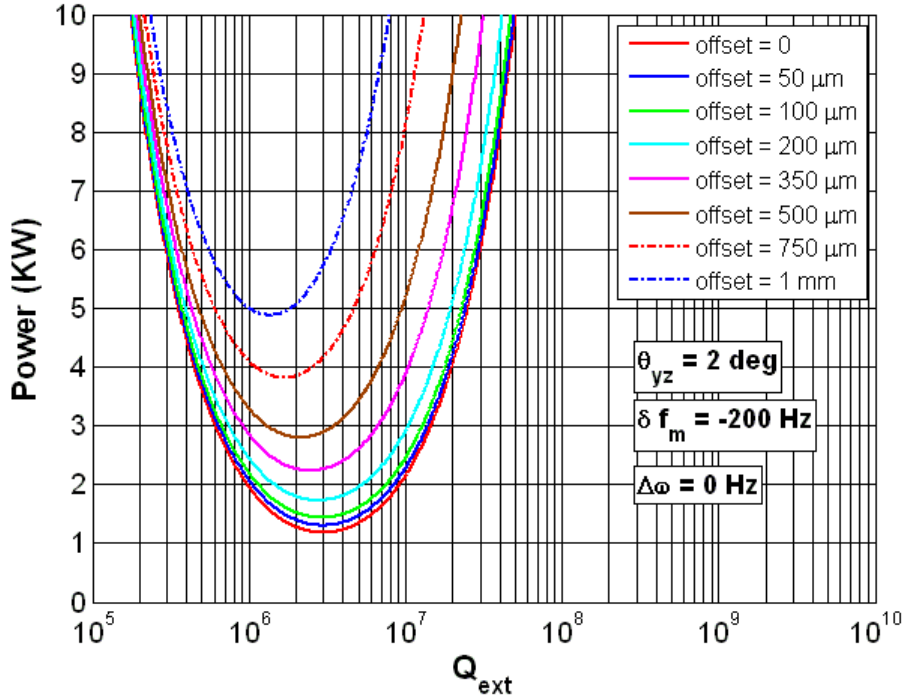
$$P_s^+ = \frac{V_t^2}{8\beta(R/Q)'Q_o} \cdot \left[ \left( \beta + 1 + \frac{P_B}{P_{cav}} \right)^2 + \left( 2Q_o \frac{(\Delta f + \delta f_m)}{f_r} + \frac{P_B}{P_{cav}} \tan \phi_s \right)^2 \right]$$



$V_t \cdot y > 0$



$V_t \cdot y < 0$



# LLRF Timeline

