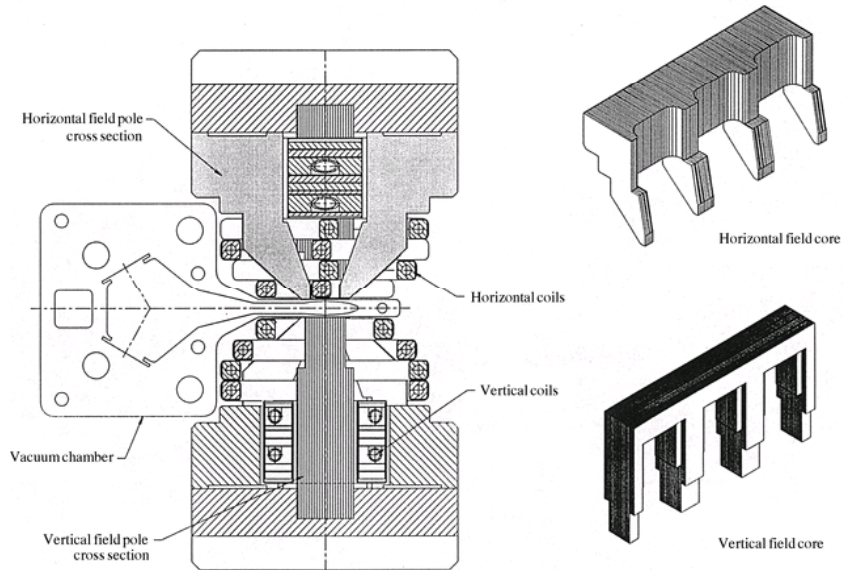


A Review of the IEX Undulator Intermediate Energy X-ray

By Mark Jaski

History



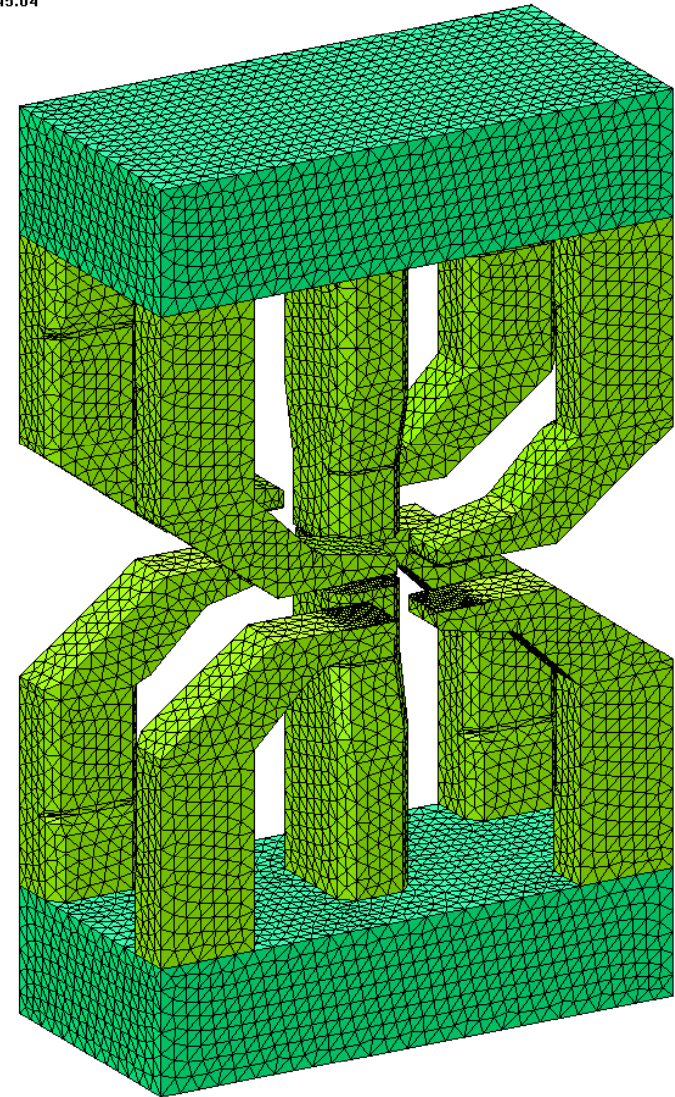
The CPU in Sector 4

- The project started with a request if we could do something similar to the circular polarizing undulator (CPU) that is installed in sector 4.
- Several possible undulator designs were discussed
 - Apple II (all permanent magnet)
 - Electromagnetic/Permanent magnet
 - Electromagnetic
- The device had to be quasiperiodic.

Optimization

24/Feb/2011 14:45:04

- OPERA Optimizer was used to optimize the pole geometry
- Optimization was done on a $\frac{1}{2}$ period model
- The currents were chosen such that the Bx and By coils were limited to 40 and 45 watts respectively. This constraint keeps the coil temperatures down.
- The geometry was modified, dimensions were changed, and the Bx and By effective fields were calculated.
- This process was repeated over and over again until the maximum Bx+By field was obtained.



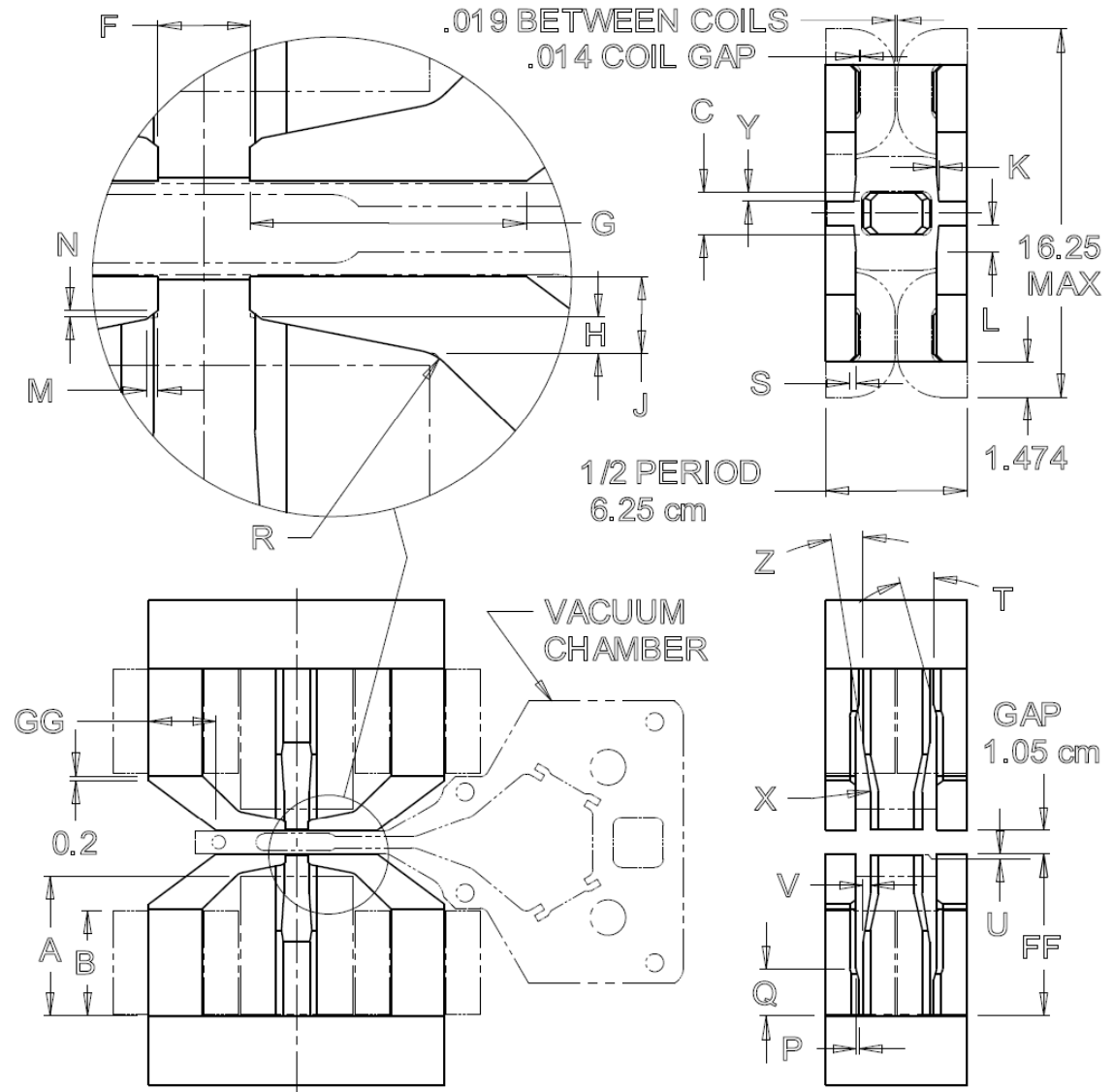
Opera

Optimization Model Dimensions

Table 3: Optimized dimensions.

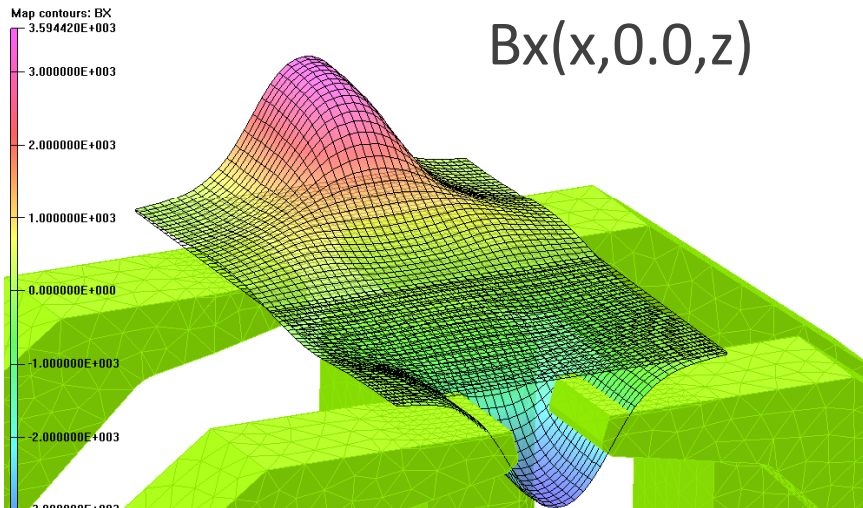
I.D.	Description	Optimal Value	unit
A	By coil height max	6.3	cm
B	Bx coil height max	5.034	cm
C	By pole width	1.823	cm
D*	Conductor size max	0.3264	cm
E*	Conductor size min	0.3231	cm
F	Bx pole gap	1.021	cm
G	Bx pole ball	3.561	cm
H	Bx toenail chamfer	0.404	cm
J	Bx pole toe	0.852	cm
K	Bx tip chamfer z	0.094	cm
L	Bx tip chamfer x	1.176	cm
M	Bx toe tip chamfer x	0.13	cm
N	Bx toe tip chamfer y	0.072	cm
P	Bx cut z	0.131	cm
Q	Bx base height	2.057	cm
R	Bx radius	0.5	cm
S	Bx chamfer	0.276	cm
T	Bx angle	15.5	°
U	By tip offset	0.037	cm
V	By cut z	0.341	cm
W	By base height	5.417	cm
X	By radius	0.5	cm
Y	By chamfer	0.351	cm
Z	By angle	9	°
AA*	Conductor radius	0.081	cm
BB*	Conductor insulation	0.049	cm
CC*	Inner coil fiberglass	0.046	cm
DD*	Outer coil fiberglass	0.036	cm
EE*	Conductor allowance	0.0076	cm
FF	Bx pole height	2.218	cm
GG	Bx pole heel width	2.973	cm

* Not shown in figure 2

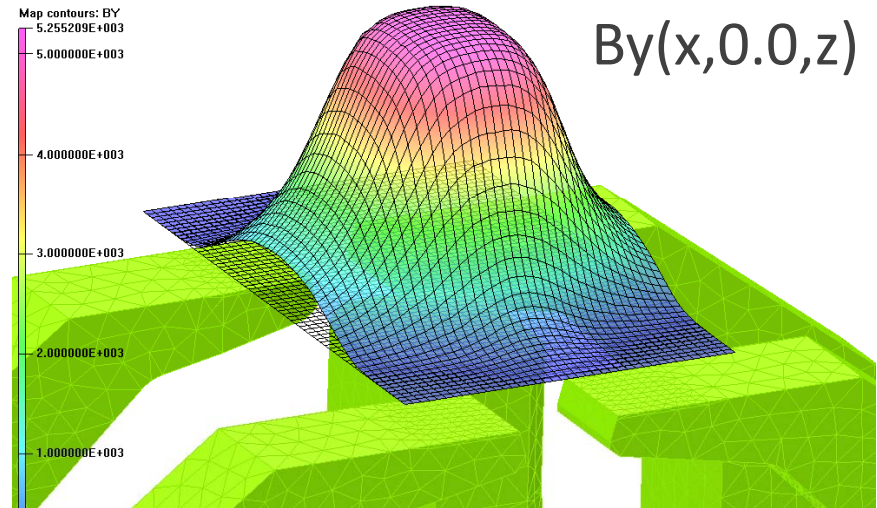


Field Plots

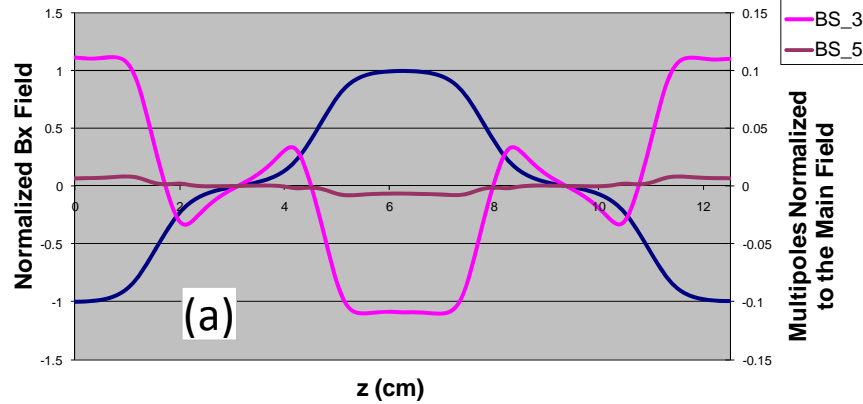
26/Jan/2011 10:39:15



26/Jan/2011 10:40:59

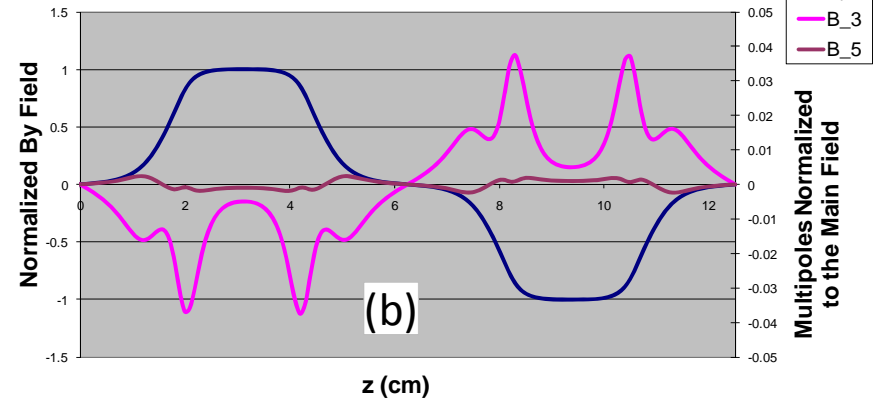


Normalized Bx Multipoles $r = 3\text{mm}$ (B_x peak = 3767 Gauss)



Bx Field

Normalized By Multipoles $r = 3\text{mm}$ (B_y peak = 5456 Gauss)



By Field

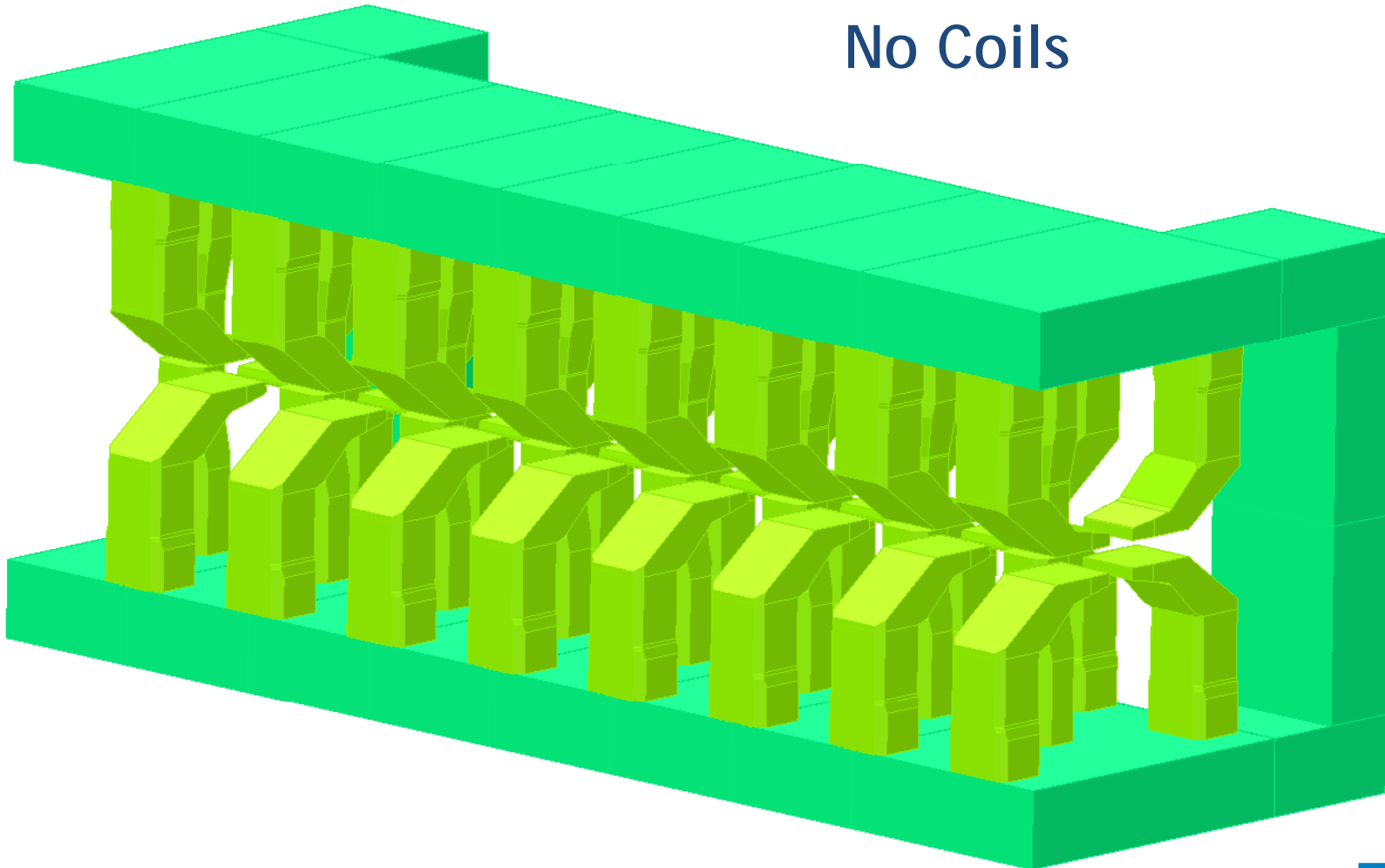
IEX Selected Parameters

General	Period	12.5	cm
	Gap	10.5	mm
	Periods per device (including end poles)	38	Periods
Horizontal Linear Polarization	Minimum Photon Energy	250	eV
	Required vertical effective field	4510	Gauss
	Current density in the copper conductor ²	4.7	A/mm ²
	Current	47.6	A
	Turns per coil ¹	62	turns
	Ampere-turns ^{1, 2}	2951	Ampere-turns
	Watts per coil ^{1, 2}	44.9	Watts
	Total number of coils	152	Each
	Total power ²	6630	Watts
	Maximum temperature of coils	100	°C
Vertical Linear Polarization	Minimum Photon Energy	440	eV
	Required horizontal effective field	3310	Gauss
	Current density in the copper conductor ²	4.9	A/mm ²
	Current	50.3	A
	Turns per coil ¹	46	turns
	Ampere-turns ^{1, 2}	2314	Ampere-turns
	Watts per coil ^{1, 2}	40.2	Watts
	Total number of coils	304	Each
	Total power ²	11,868	Watts
	Maximum temperature of coils	100	°C
Circular Polarization	Minimum Photon Energy	440	eV
	Required horizontal and vertical effective field	2340	Gauss
	Current at vertical effective field	20.7	A
	Current at horizontal effective field	34.2	A
¹ End coils are smaller			
² At the required effective field			

OPERA 4 Period Model For Prototype

24/Jan/2011 12:59:10

No Coils



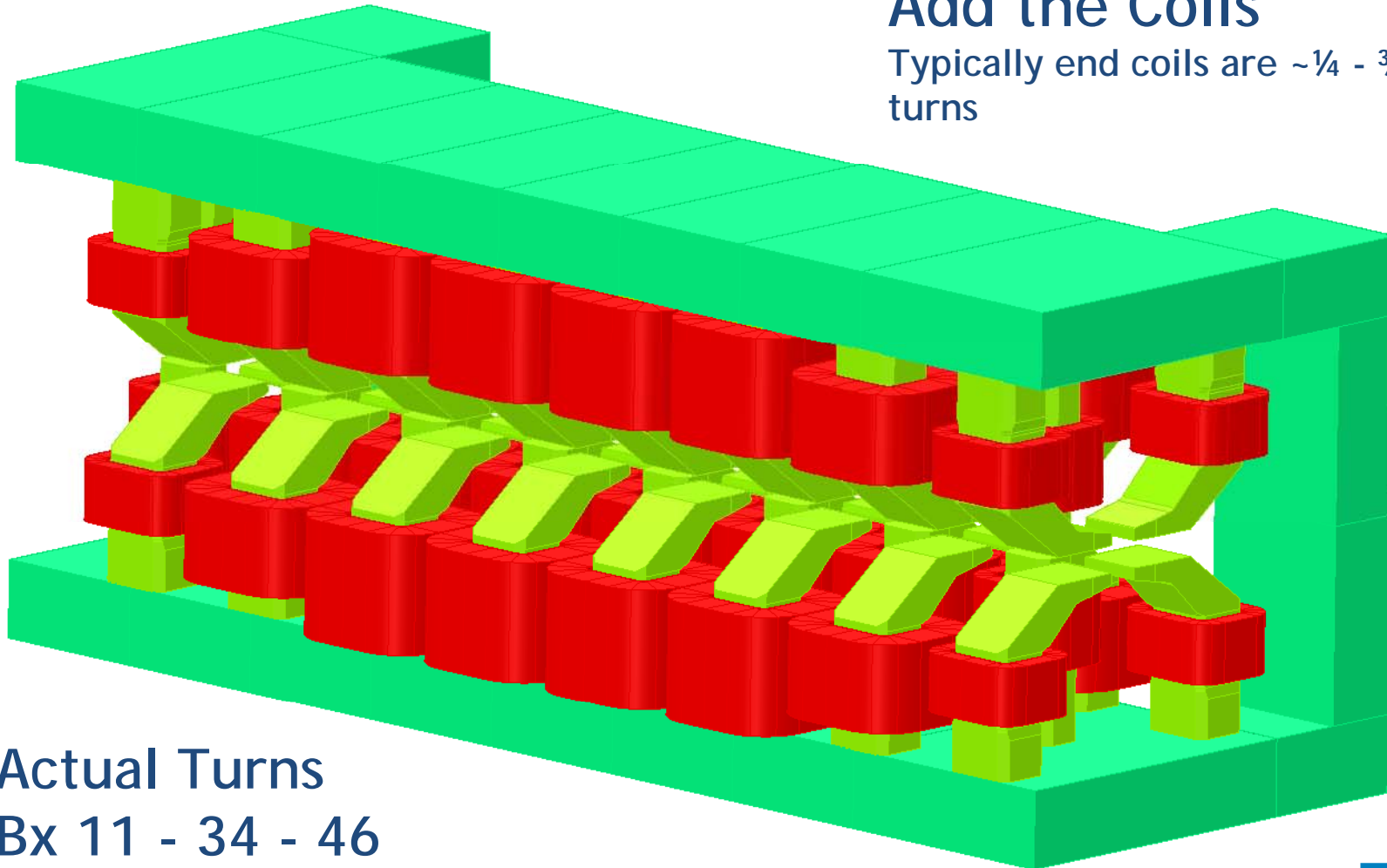
Opera

OPERA 4 Period Model For Prototype

24/Jan/2011 12:58:12

Add the Coils

Typically end coils are $\sim 1/4$ - $3/4$ - 1 turns



Actual Turns

Bx 11 - 34 - 46

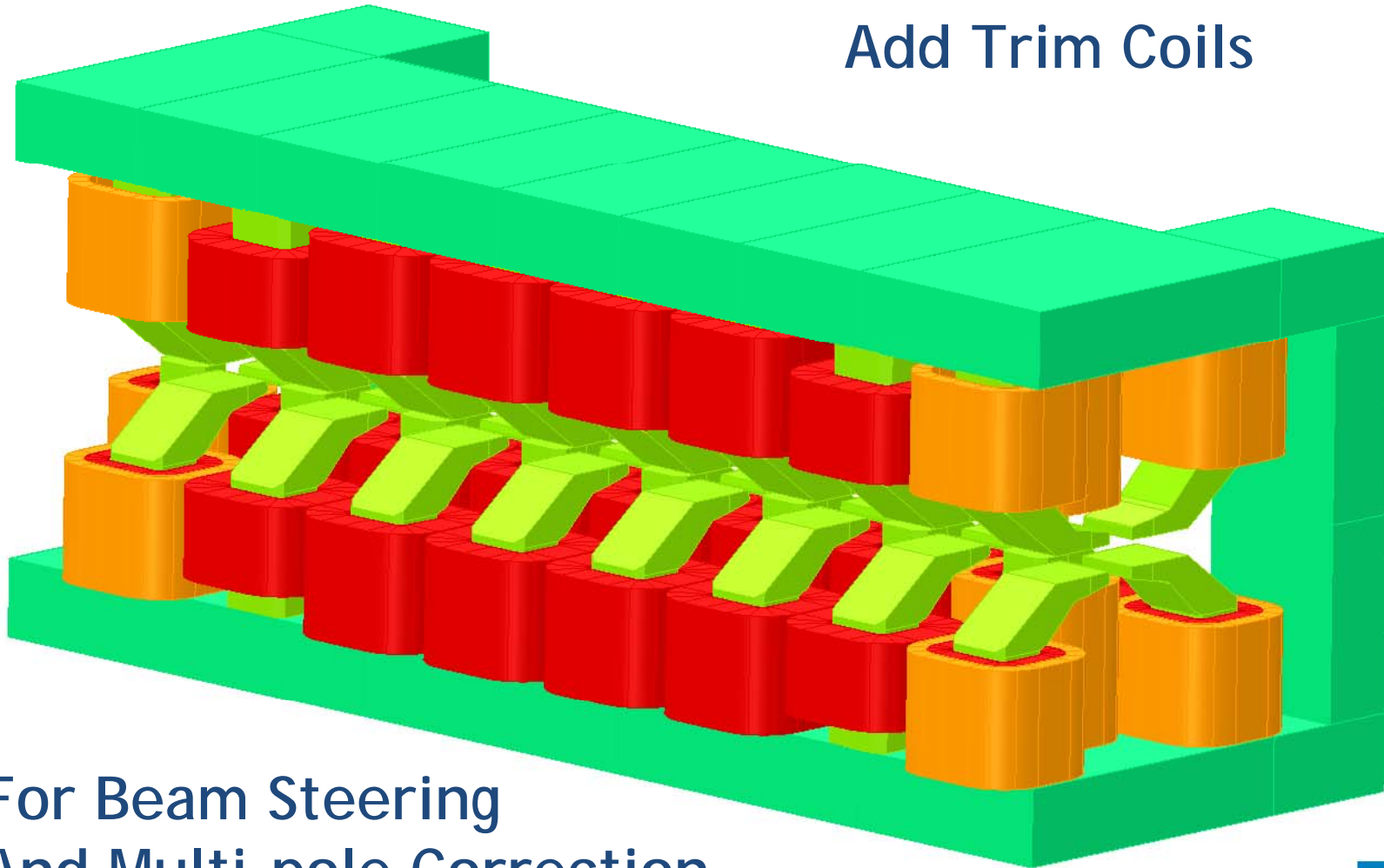
By 15 - 42 - 62

Opera

OPERA 4 Period Model For Prototype

24/Jan/2011 12:57:06

Add Trim Coils



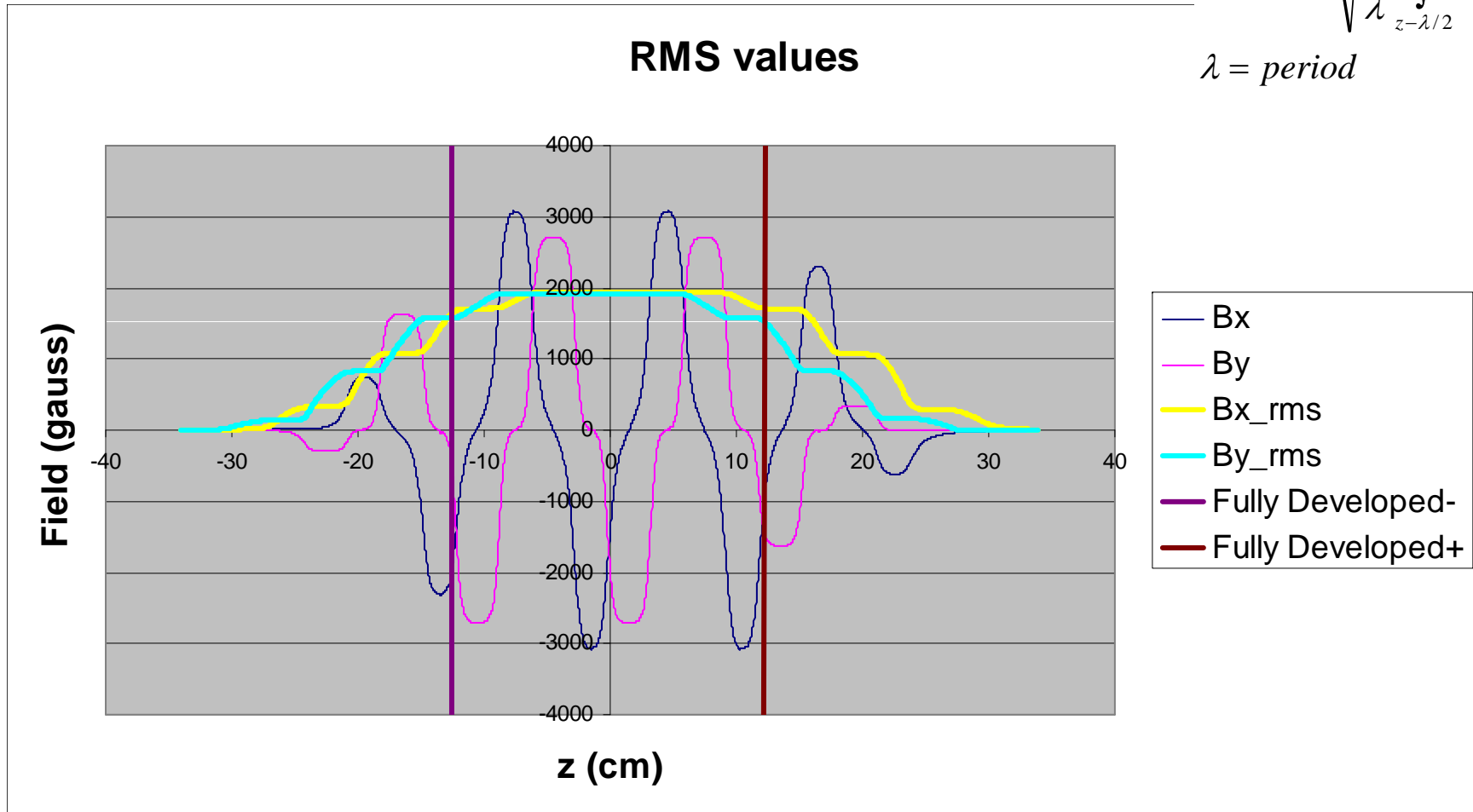
For Beam Steering And Multi-pole Correction

Opera

4 Period Prototype. Why only 4 periods?

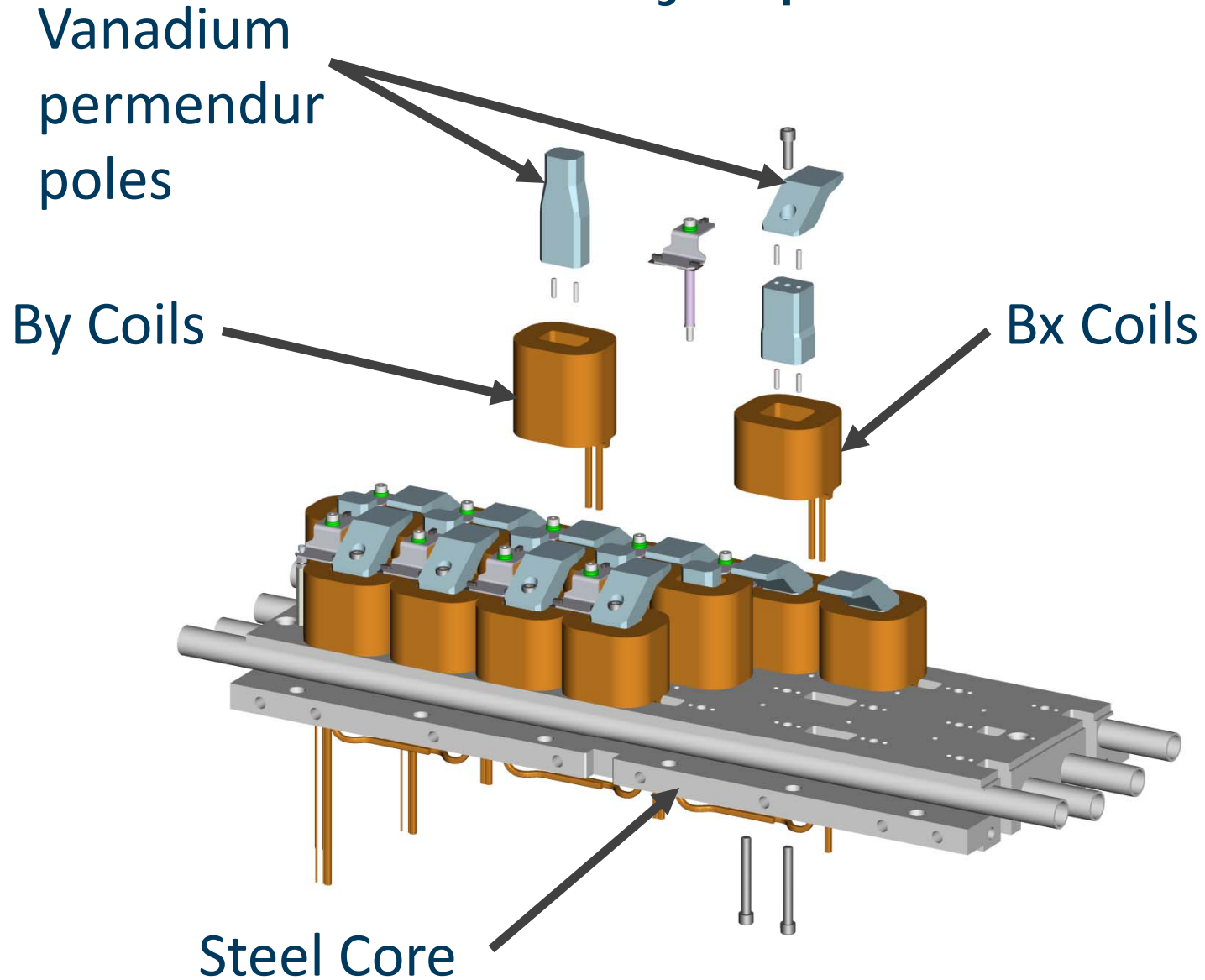
$$B_{rms}(z) = \sqrt{\frac{1}{\lambda} \int_{z-\lambda/2}^{z+\lambda/2} B^2 dz}$$

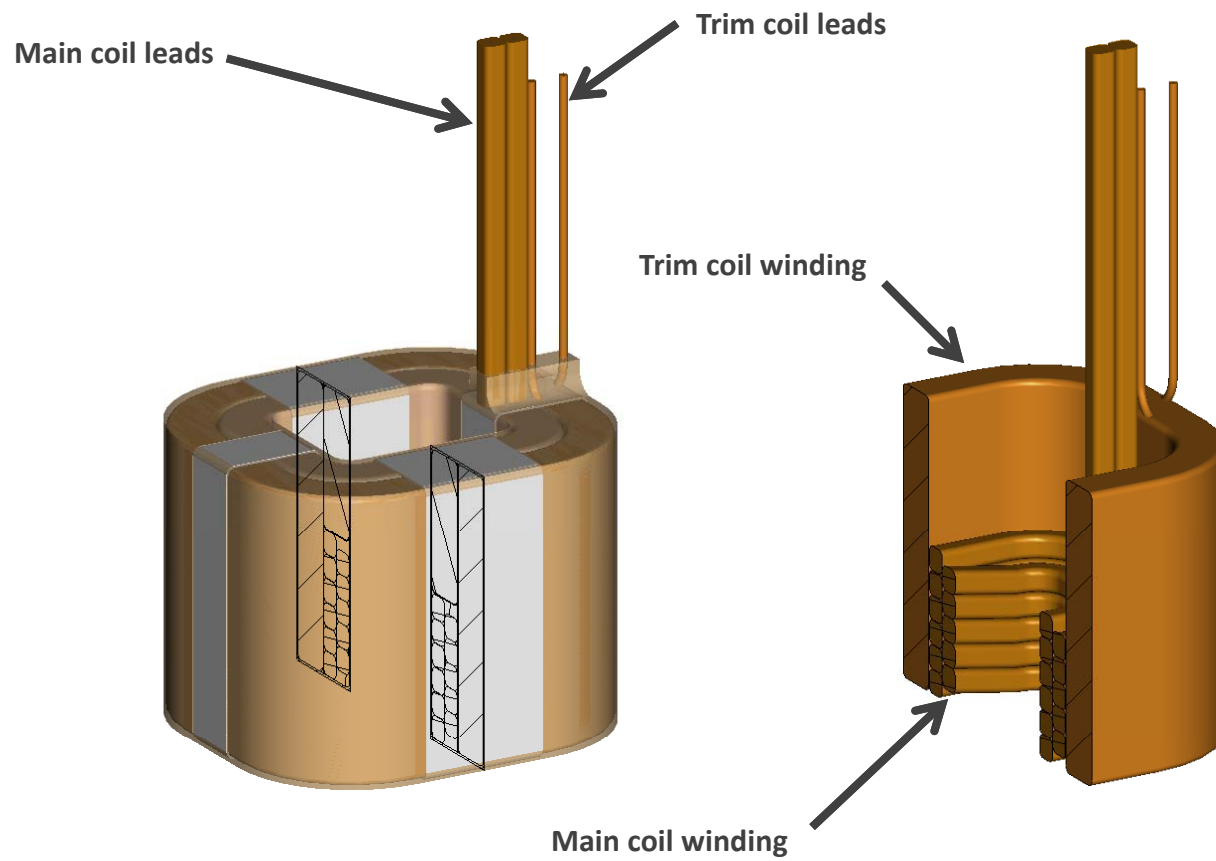
$\lambda = \text{period}$



~2 full Period of fully developed field

General Assembly Exploded View

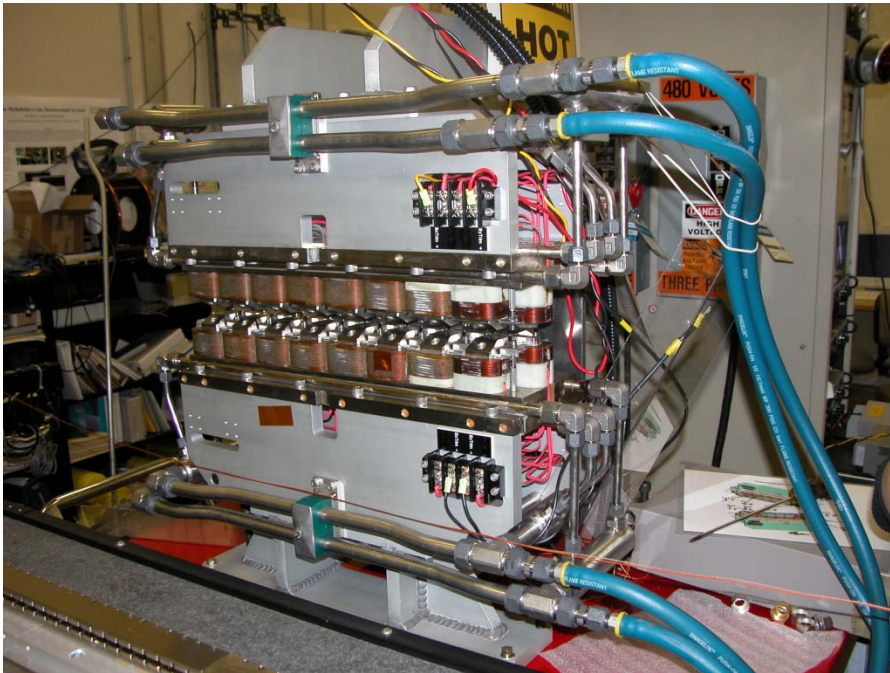




Trim Coils

- Two windings per coil
 - Main coil winding
 - Trim coil winding

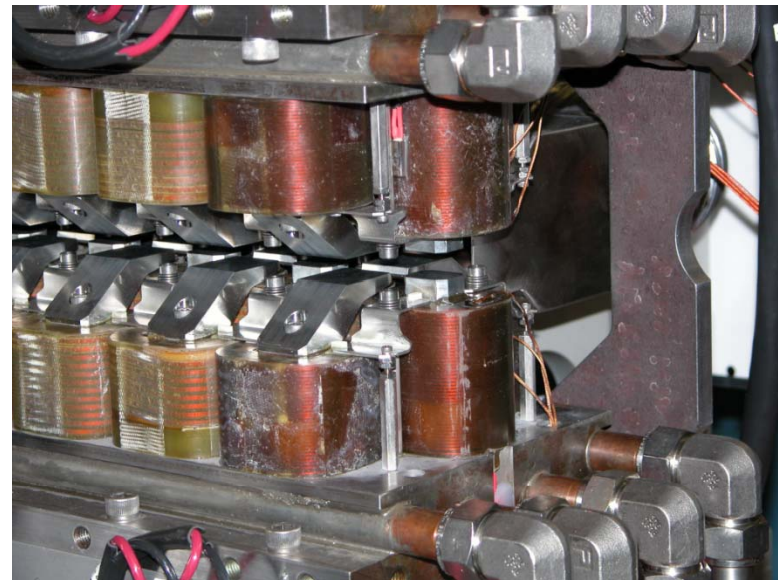
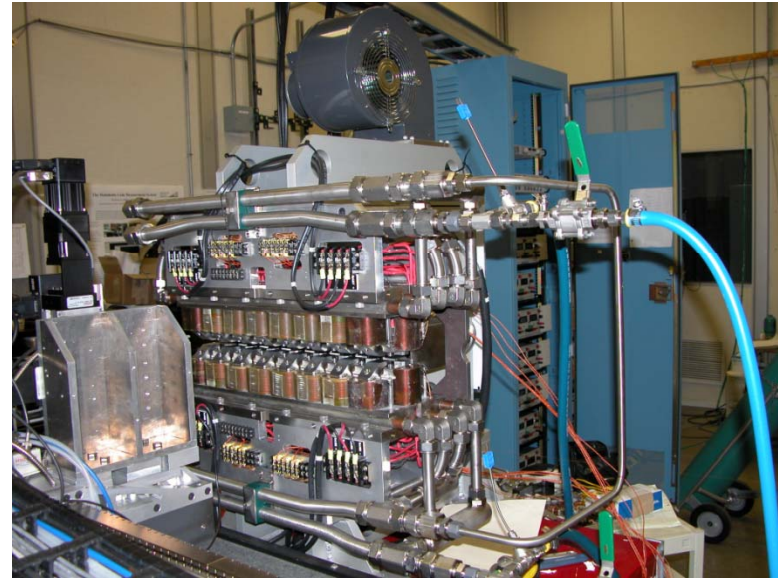
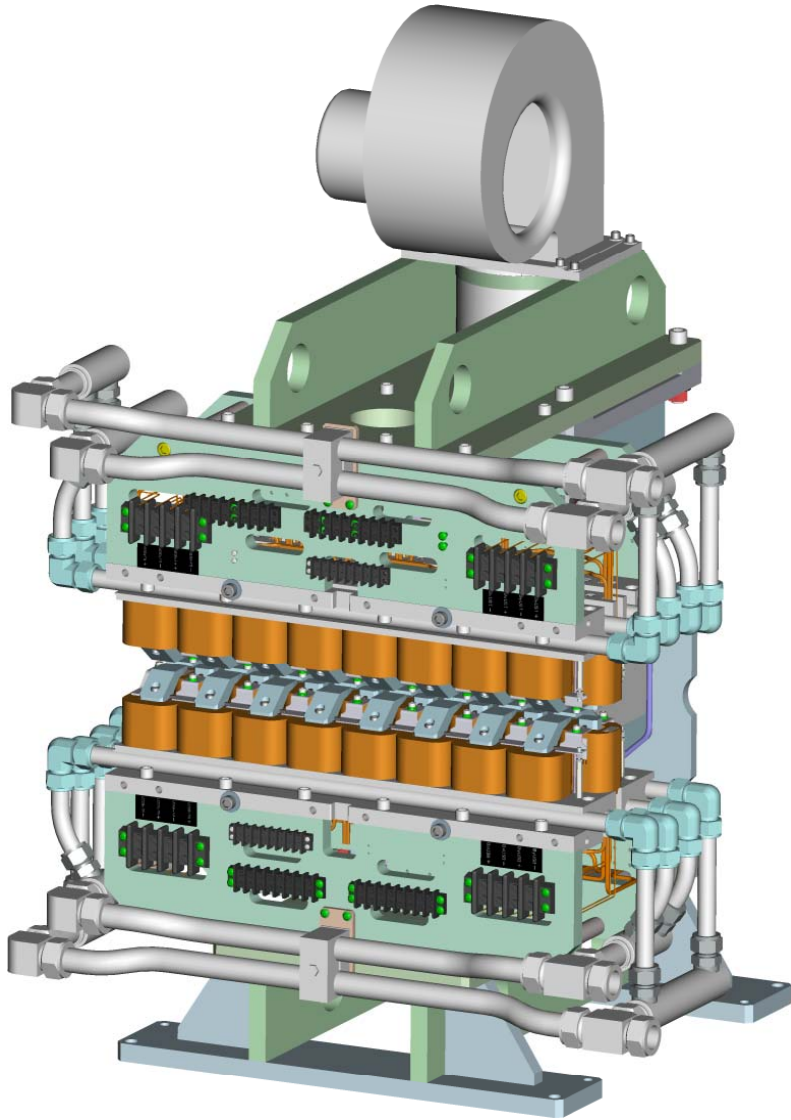
IEX Prototype 1 (4 periods)



Major Changes

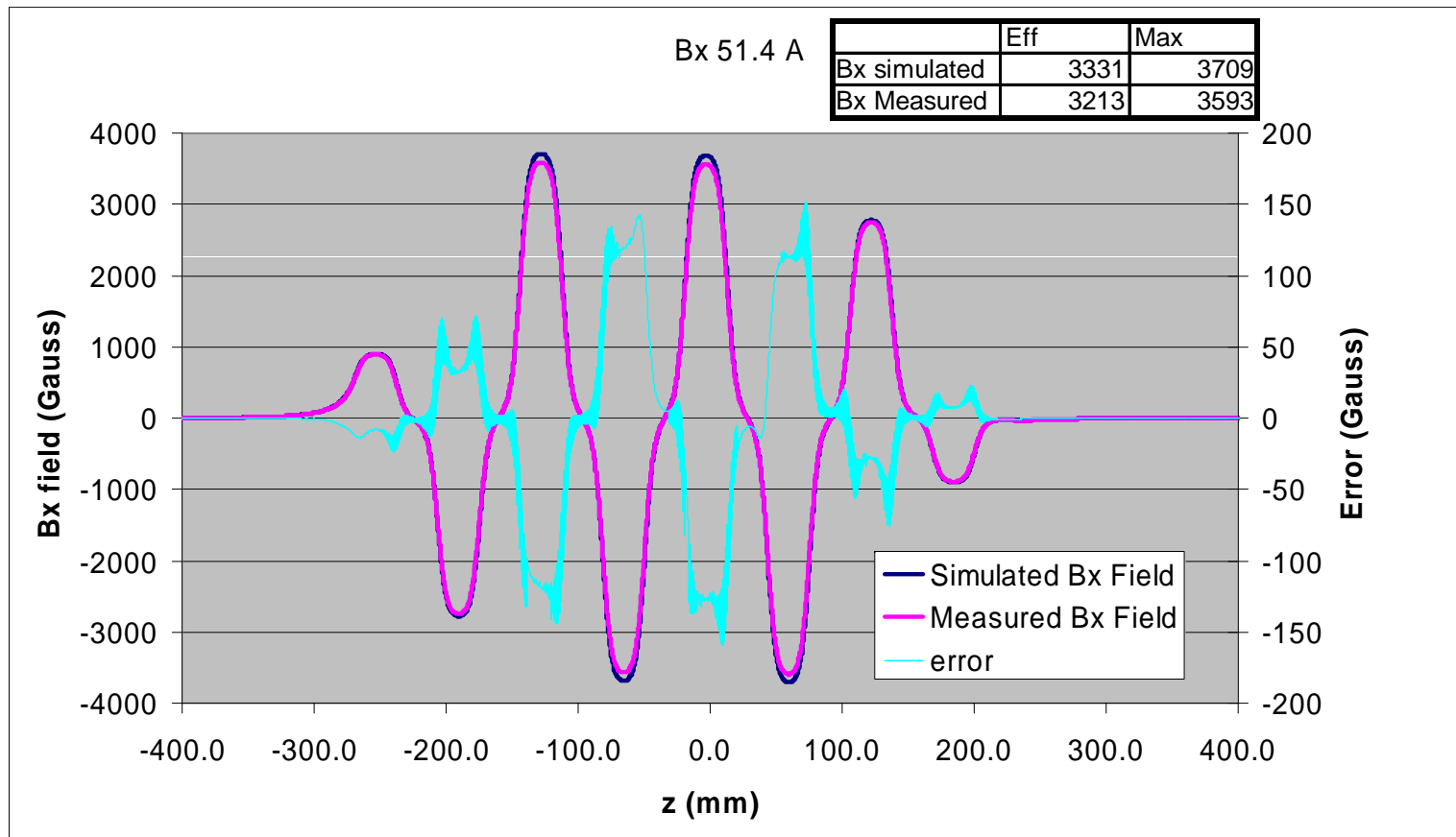
- Magnetic field roll off was too large for storage ring injection. The poles will be made wider.
- Plating reduced the field by $\sim 1\%$. The poles are not plated.
- The gap was changed from 11.0 mm to 10.5 mm to lower the maximum current to lower the temperature rise.
- The period was changed from 12.0 cm to 12.5 cm to make the coils larger and lower the field requirements.

IEX Prototype 2



Compare Measured Bx Field To Simulated Bx Field

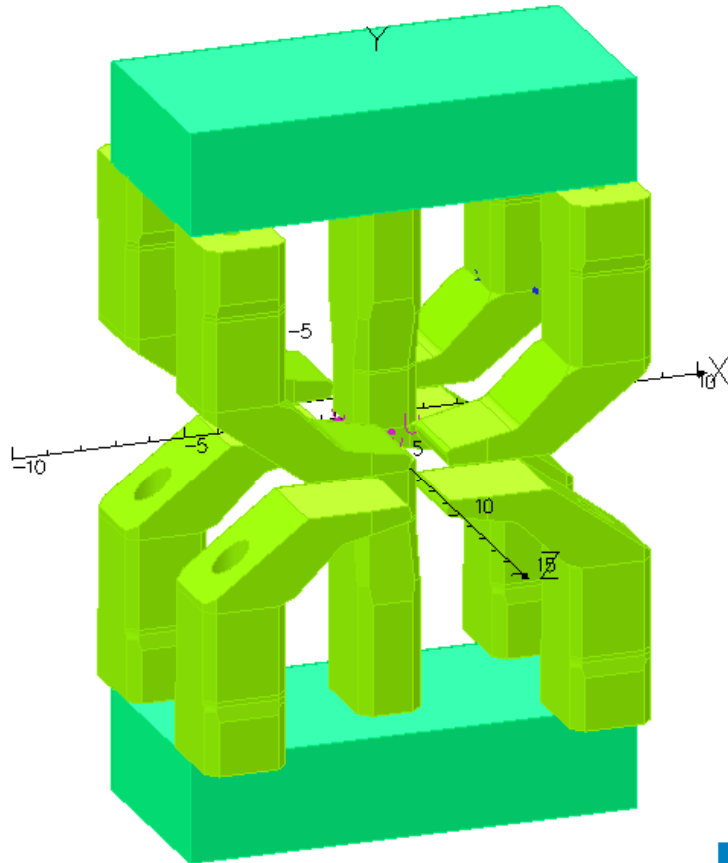
The measured Bx effective field is 3.5% lower than simulated.
The measured Bx Peak field is 3.1% lower than simulated.



Similar results for By

Bolt Holes

11/Nov/2010 09:36:42



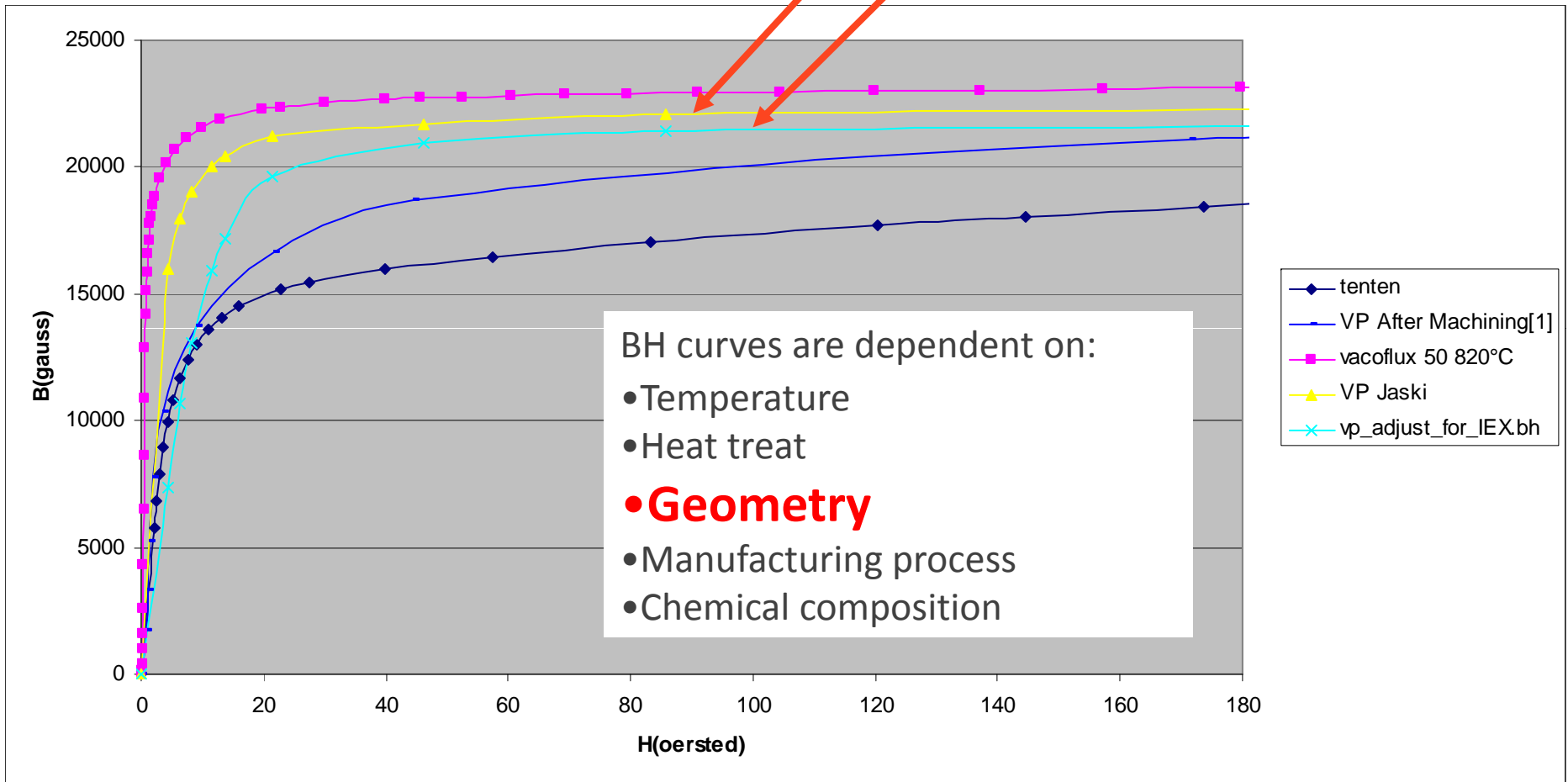
	Without bolt holes	With bolt holes	With bolt holes
	Gauss	Gauss	%
Bx max	3719	3690	-0.8
Bx eff	3360	3338	-0.7
By max	5388	5388	0.0
By eff	4590	4589	0.0

- Bolt holes do cause an 0.8% reduction in the Bx field.
- Bolt holes were not modeled because they add more computation time to the analyses.
- IEXP2 has SS bolts.
- Steel bolts can be used to slightly increase the Bx fields.
- Exchanging steel bolts with SS bolts could be used as a method for tuning.

Opera

Modify the VP BH Curve

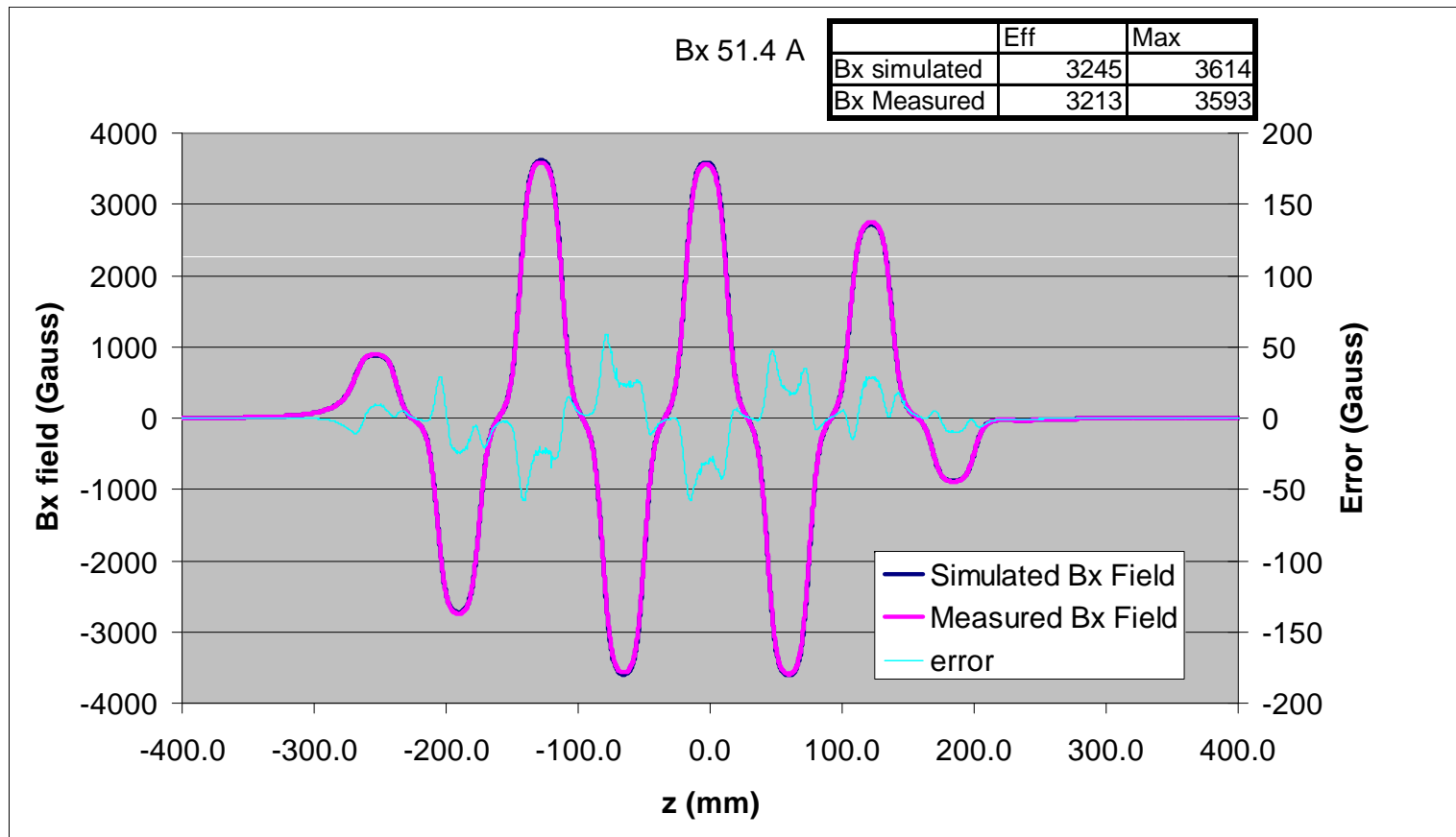
Original BH Curve
Use This BH Curve



[1] "SOME INITIAL RESULTS FROM THE NEW SLAC PERMEAMETER"
J. K. Cobb and R. A. Early

Compare Measured Bx Field To Simulated Bx Field After Adjusted BH Curve

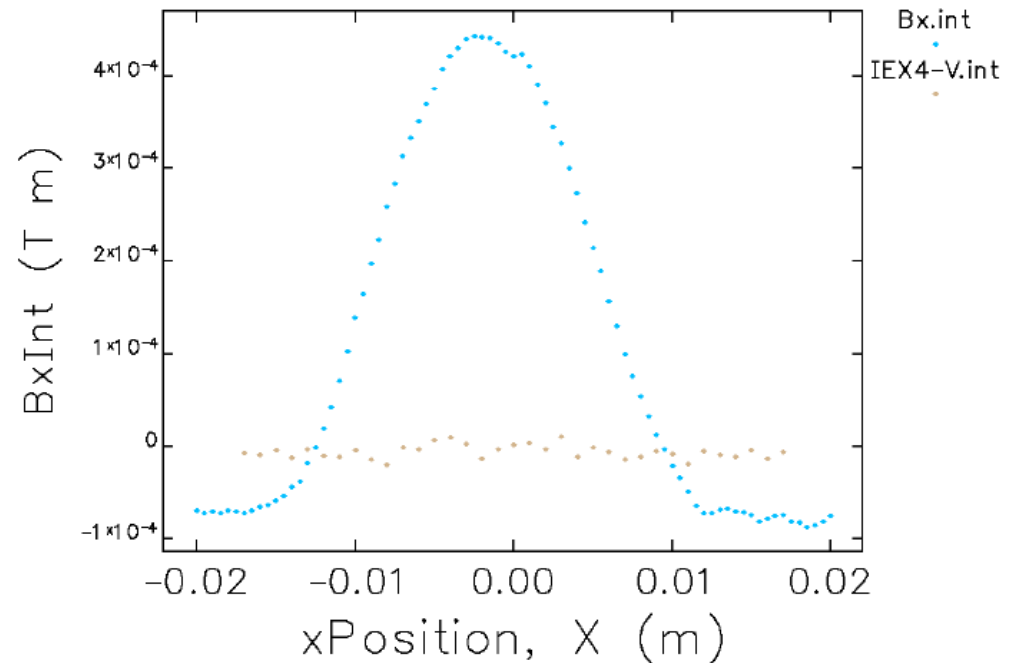
The measured Bx effective field is 1% lower than simulated.
The measured Bx Peak field is 0.6% lower than simulated.



Simulated values will drop by ~0.8% if bolt holes are modeled

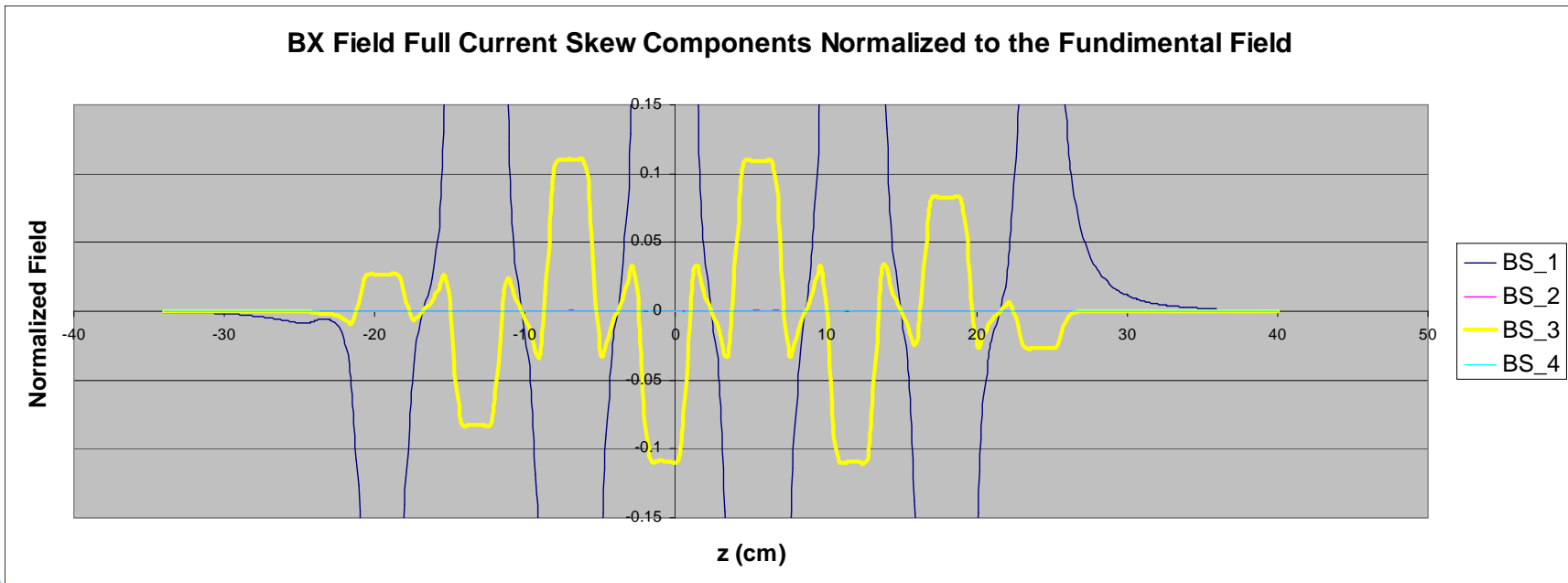
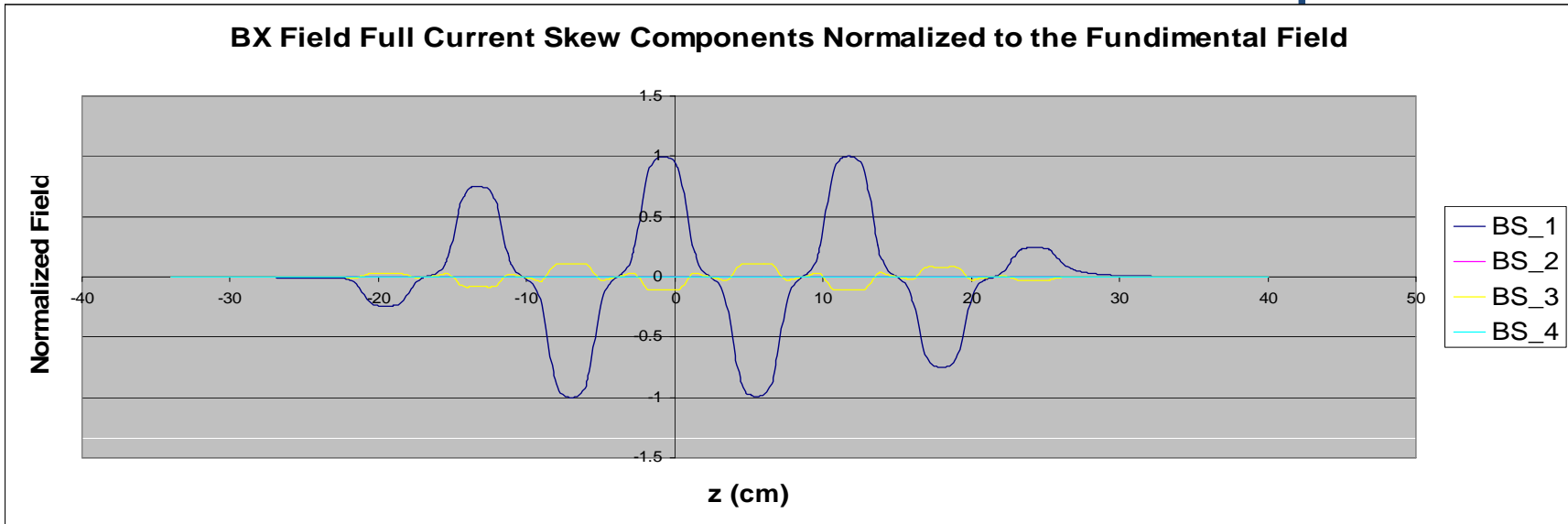
Measurements of IEXP2 Fix the Skew Sextupole

- Aimin X. pointed out a skew sextupole component.
- Yes it can be fixed.
- Not an active fix.



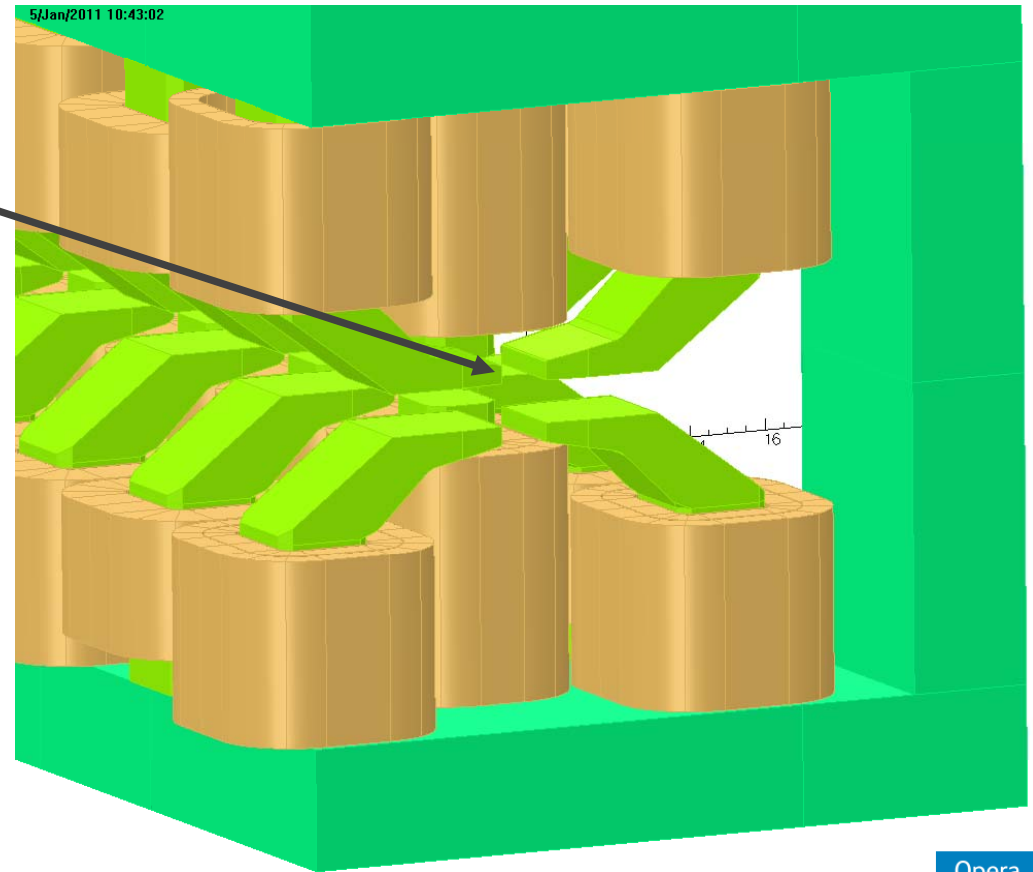
1st integral (y=0) – Very different..
But at same level of By field.
Is this a problem? Can it be fixed?

Measurements of IEXP2 Fix the Skew Sextupole



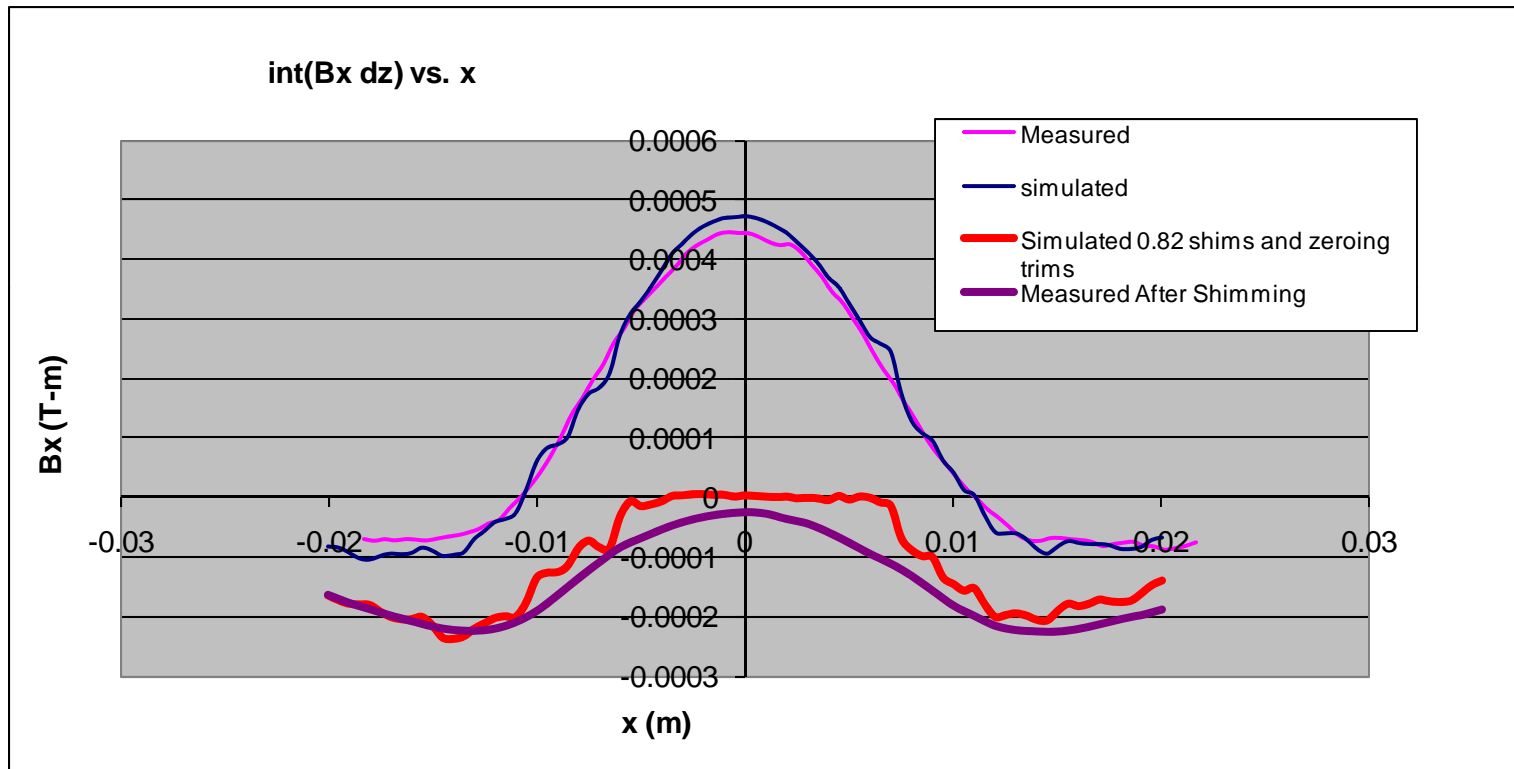
Measurements of IEXP2 Fix the Skew Sextupole

- Grinding these four downstream pole tips reduces the skew sextupole component.
- This was tested and showed this on the prototype.
- The trim coils will be set so the first and second integrals are zero.
- The skew sextupole will be measured and the amount of grinding will be calculated.
- Extra pole tips have been ordered.
- Provisions for easy replacement of these pole tips are provided.



Opera

Measurements of IEXP2 Fix the Skew Sextupole

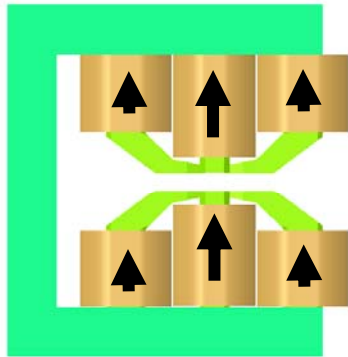


End Coil Multi-pole Field Configurations

7/Jan/2011 07:26:04

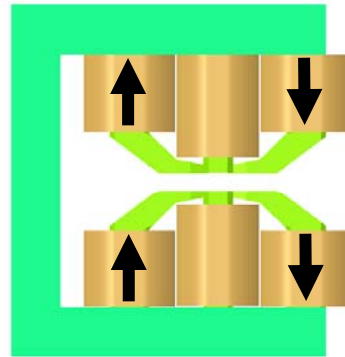
7/Jan/2011 07:26:04

7/Jan/2011 07:26:04



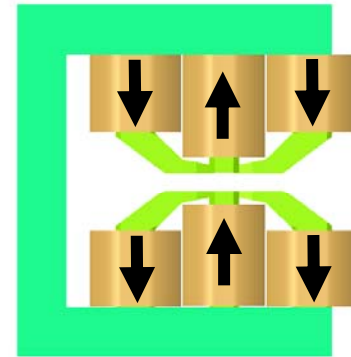
Normal Dipole

Opera



Normal Quadrupole

Opera



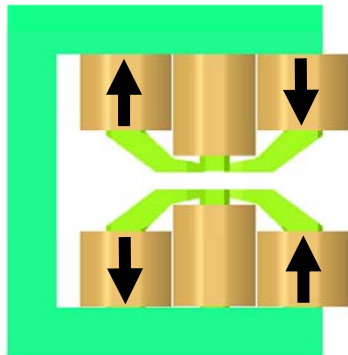
Normal Sextupole

Opera

7/Jan/2011 07:26:04

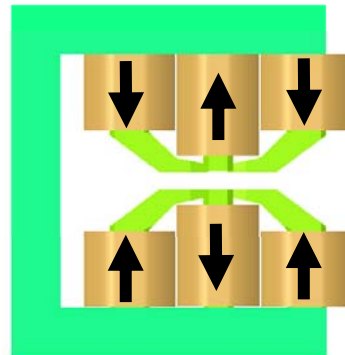
7/Jan/2011 07:26:04

7/Jan/2011 07:26:04



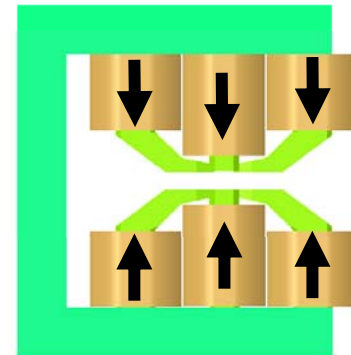
Skew Dipole

Opera



Skew Quadrupole

Opera

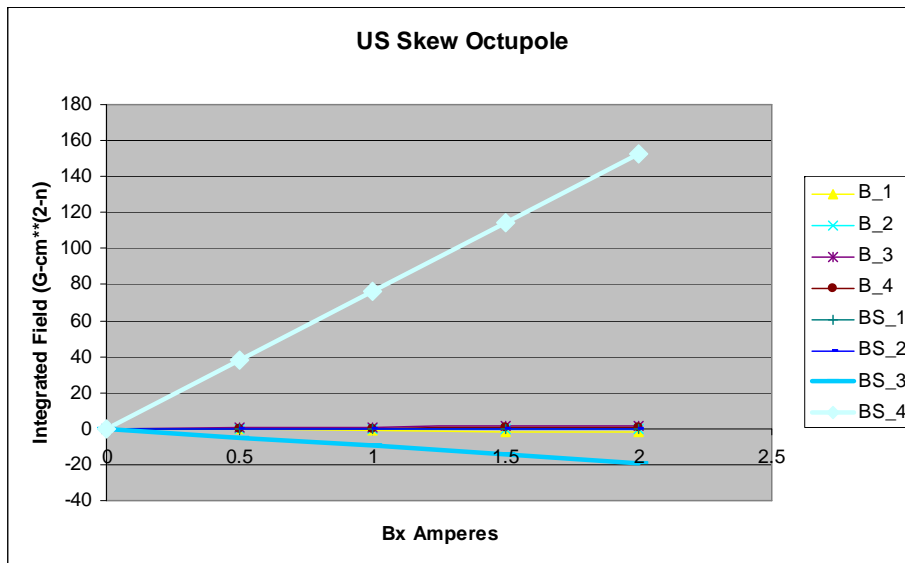
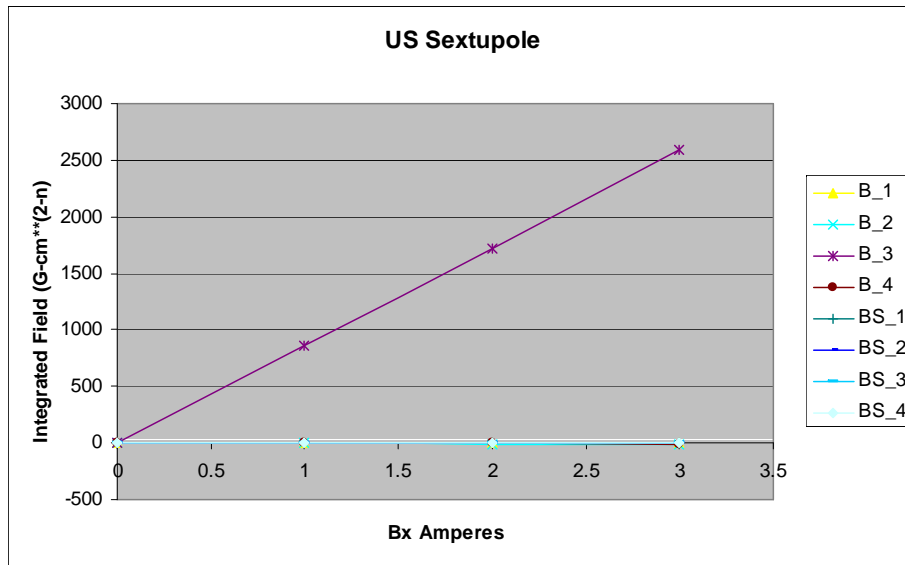


Skew Octupole

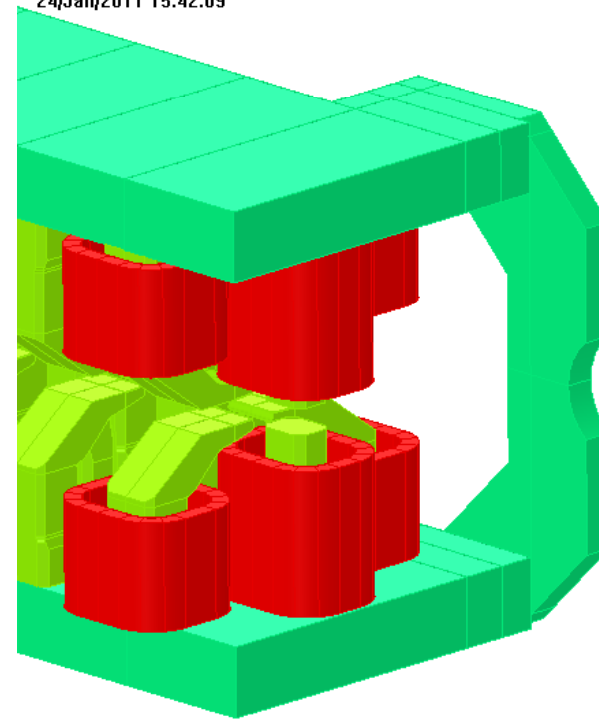
Opera



Preliminary Results

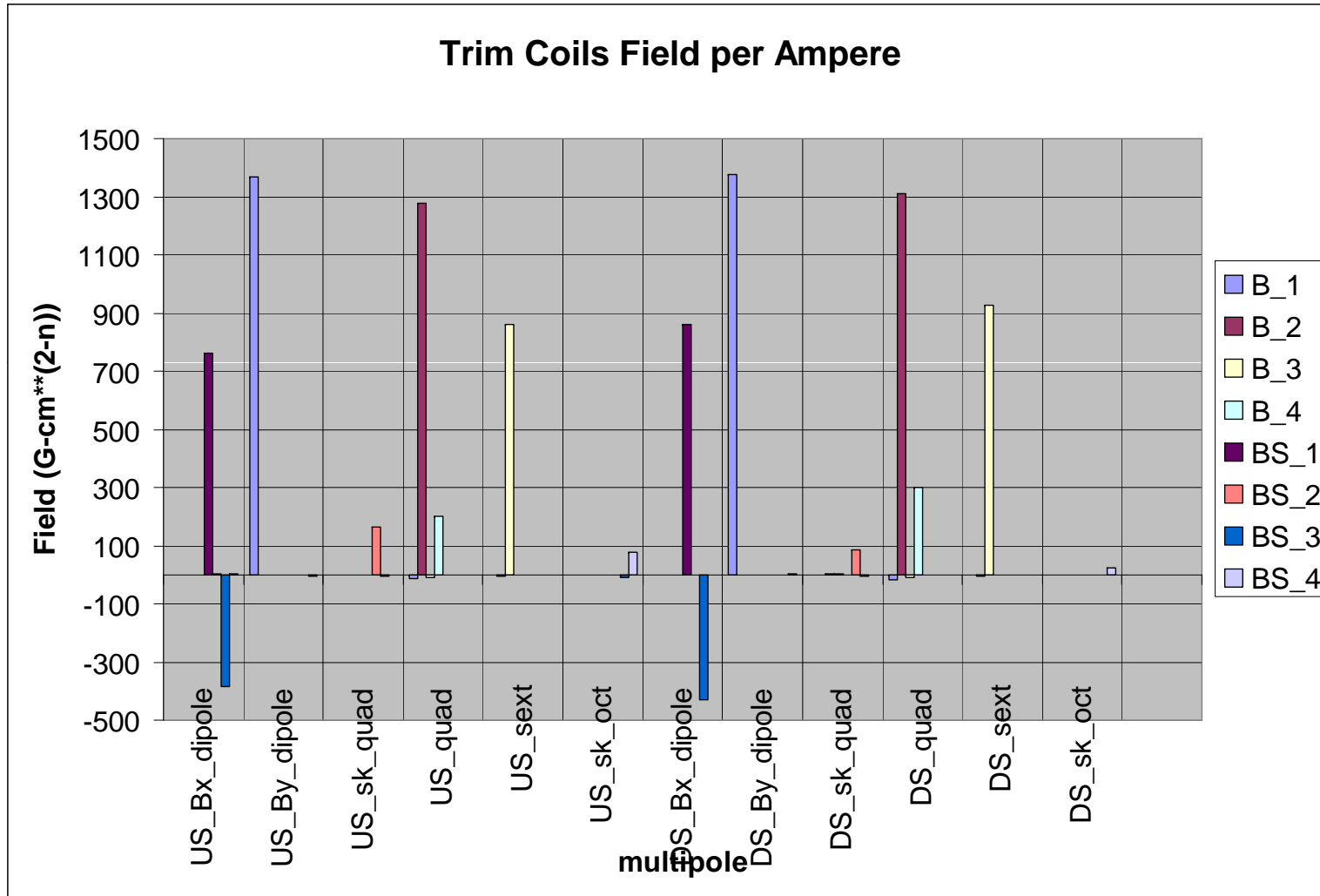


24/Jan/2011 15:42:09



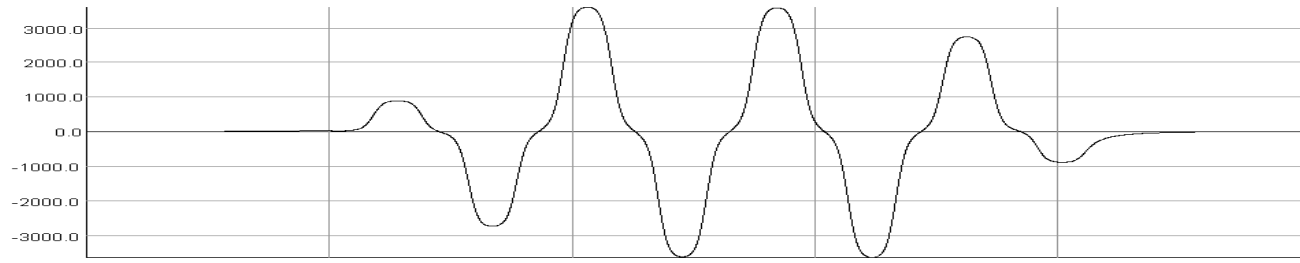
- US sextupole is clean with no other multipoles.
- US skew octupole also has a skew sextupole.
- The flux bridge appears to play a roll in additional multipoles.

Possible Multi-pole Fields With Trim Coils



Bx, 1st integral, and Beam Trajectory No Trim Coils

27/Dec/2010 11:12:45



X coord 0.0 0.0 0.0 0.0 0.0 0.0
 Y coord 0.0 0.0 0.0 0.0 0.0 0.0
 Z coord -40.0 -24.0 -8.0 8.0 24.0 40.0
 Component: BX, from buffer: Line, Integral = -470.68598277877

UNITS
 Length cm
 Magn Flux Density gauss
 Magn Field oersted
 Magn Scalar Pot oersted cm
 Magn Vector Pot gauss cm
 Elec Flux Density C cm⁻²
 Elec Field V cm⁻¹
 Conductivity S cm⁻¹
 Current Density A cm⁻²
 Power W
 Force N
 Energy J
 Mass g

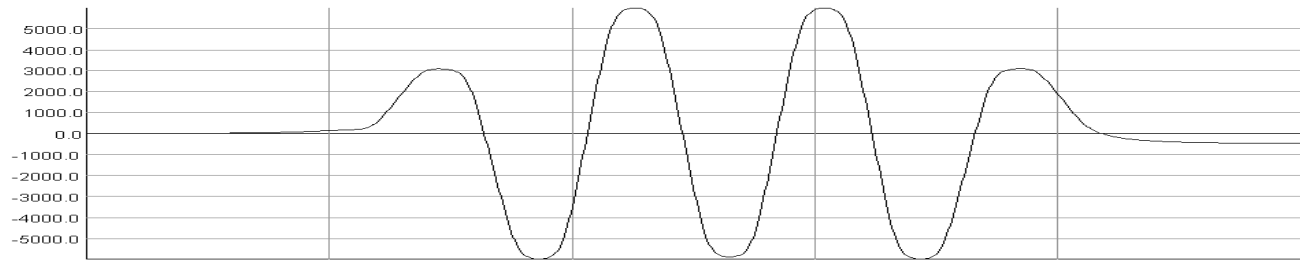
MODEL DATA
 IEX2_4_period_Bx.op3
 TOSCA Magnetostatic
 Nonlinear materials
 Simulation No 2 of 12
 21261353 elements
 4803903 nodes
 36 conductors
 Nodally interpolated fields
 Activated in global coordinates

Field Point Local Coordinates
 Local = Global

FIELD EVALUATIONS
 Line LINE 8001 Cartesian
 (nodal)
 x=0.0 y=0.0 z=-40.0 to 40.0

Opera

27/Dec/2010 10:46:17



X coord 0.0 0.0 0.0 0.0 0.0 0.0
 Y coord 0.0 0.0 0.0 0.0 0.0 0.0
 Z coord -40.0 -24.0 -8.0 8.0 24.0 40.0
 Component: INTEGRAL from table file., Integral = -1554.3173729

UNITS
 Length cm
 Magn Flux Density gauss
 Magn Field oersted
 Magn Scalar Pot oersted cm
 Magn Vector Pot gauss cm
 Elec Flux Density C cm⁻²
 Elec Field V cm⁻¹
 Conductivity S cm⁻¹
 Current Density A cm⁻²
 Power W
 Force N
 Energy J
 Mass g

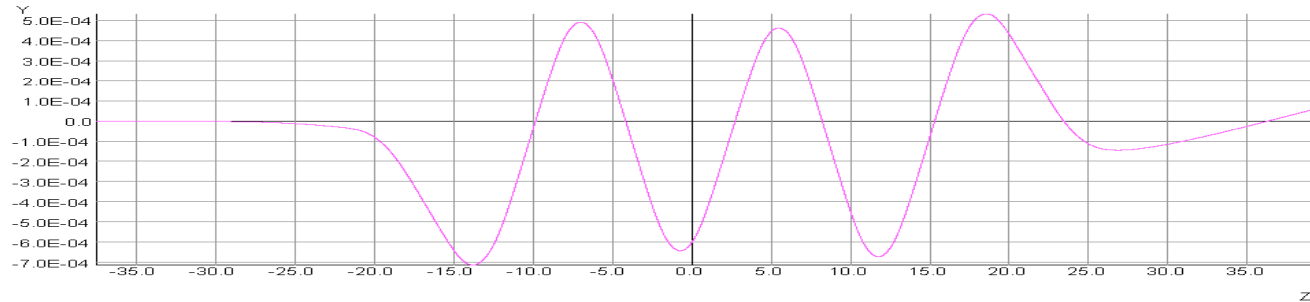
MODEL DATA
 IEX2_4_period_Bx.op3
 TOSCA Magnetostatic
 Nonlinear materials
 Simulation No 2 of 12
 21261353 elements
 4803903 nodes
 36 conductors
 Nodally interpolated fields
 Activated in global coordinates

Field Point Local Coordinates
 Local = Global

FIELD EVALUATIONS
 Line LINE 8001 Cartesian
 (nodal)
 x=0.0 y=0.0 z=-40.0 to 40.0

Opera

27/Dec/2010 11:13:18



UNITS
 Length cm
 Magn Flux Density gauss
 Magn Field oersted
 Magn Scalar Pot oersted cm
 Magn Vector Pot gauss cm
 Elec Flux Density C cm⁻²
 Elec Field V cm⁻¹
 Conductivity S cm⁻¹
 Current Density A cm⁻²
 Power W
 Force N
 Energy J
 Mass g

MODEL DATA
 IEX2_4_period_Bx.op3
 TOSCA Magnetostatic
 Nonlinear materials
 Simulation No 2 of 12
 21261353 elements
 4803903 nodes
 36 conductors
 Nodally interpolated fields
 Activated in global coordinates

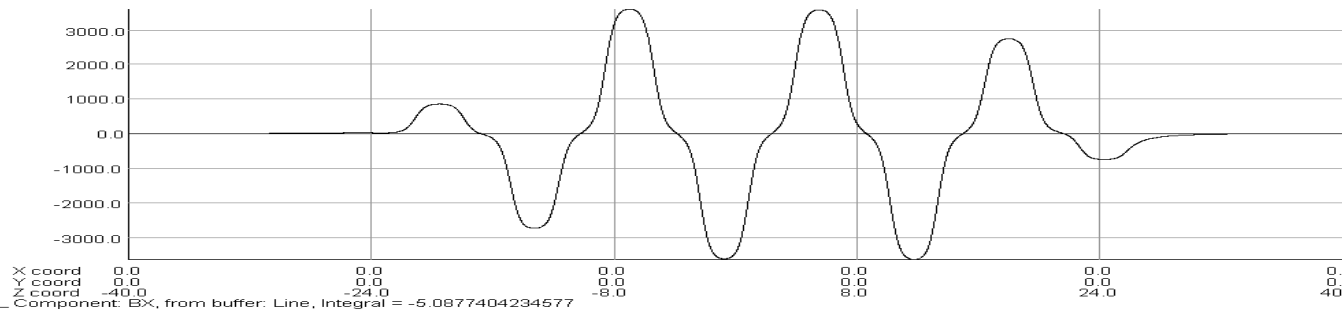
Field Point Local Coordinates
 Local = Global

FIELD EVALUATIONS
 Line LINE 8001 Cartesian
 (nodal)
 x=0.0 y=0.0 z=-40.0 to 40.0

Opera

Bx, 1st integral, and Beam Trajectory With Trim Coils

27/Dec/2010 10:26:42



UNITS
Length cm
Magn Flux Density gauss
Magn Field oersted
Magn Scalar Pot oersted cm
Magn Vector Pot gauss cm
Elec Flux Density C cm⁻²
Elec Field V cm⁻¹
Conductivity S cm⁻¹
Current Density A cm⁻²
Power W
Force N
Energy J
Mass g

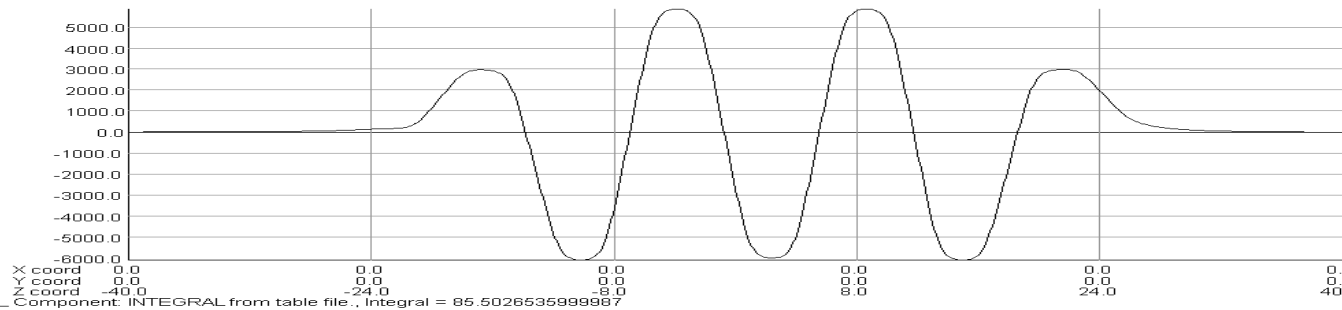
MODEL DATA
IEX2_4_period_Bx.op3
TOSCA Magnetostatic
Nonlinear materials
Simulation No 11 of 12
21261353 elements
4803903 nodes
36 conductors
Nodally interpolated fields
Activated in global coordinates

Field Point Local Coordinates
Local = Global

FIELD EVALUATIONS
Line LINE 8001 Cartesian
(nodal)
x=0.0 y=0.0 z=-40.0 to 40.0

Opera

27/Dec/2010 10:27:33



UNITS
Length cm
Magn Flux Density gauss
Magn Field oersted
Magn Scalar Pot oersted cm
Magn Vector Pot gauss cm
Elec Flux Density C cm⁻²
Elec Field V cm⁻¹
Conductivity S cm⁻¹
Current Density A cm⁻²
Power W
Force N
Energy J
Mass g

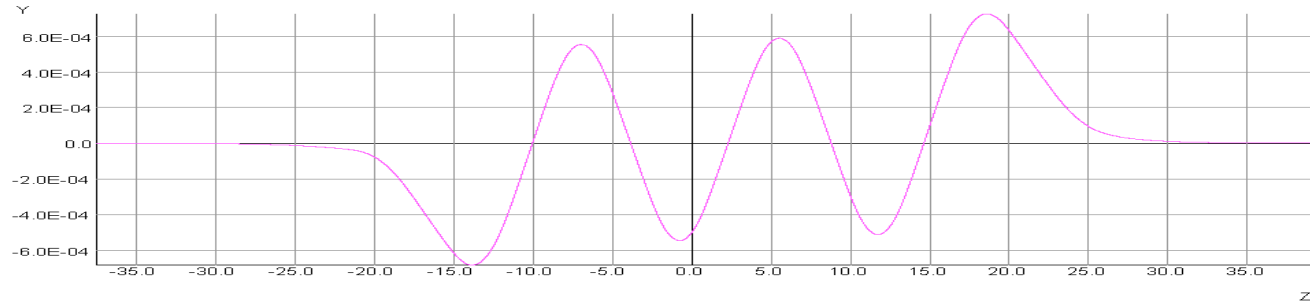
MODEL DATA
IEX2_4_period_Bx.op3
TOSCA Magnetostatic
Nonlinear materials
Simulation No 11 of 12
21261353 elements
4803903 nodes
36 conductors
Nodally interpolated fields
Activated in global coordinates

Field Point Local Coordinates
Local = Global

FIELD EVALUATIONS
Line LINE 8001 Cartesian
(nodal)
x=0.0 y=0.0 z=-40.0 to 40.0

Opera

27/Dec/2010 10:28:33



UNITS
Length cm
Magn Flux Density gauss
Magn Field oersted
Magn Scalar Pot oersted cm
Magn Vector Pot gauss cm
Elec Flux Density C cm⁻²
Elec Field V cm⁻¹
Conductivity S cm⁻¹
Current Density A cm⁻²
Power W
Force N
Energy J
Mass g

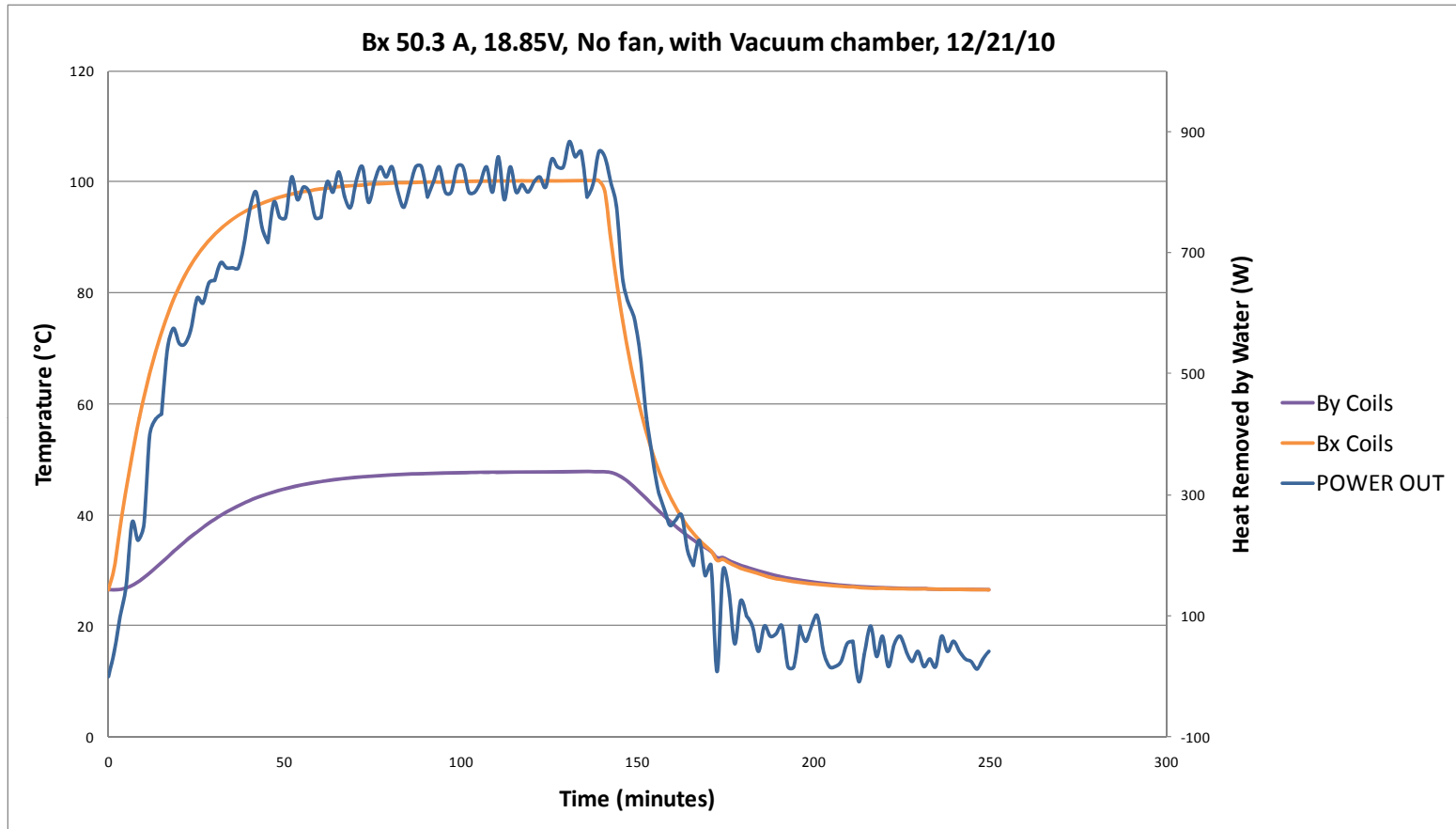
MODEL DATA
IEX2_4_period_Bx.op3
TOSCA Magnetostatic
Nonlinear materials
Simulation No 11 of 12
21261353 elements
4803903 nodes
36 conductors
Nodally interpolated fields
Activated in global coordinates

Field Point Local Coordinates
Local = Global

FIELD EVALUATIONS
Line LINE 8001 Cartesian
(nodal)
x=0.0 y=0.0 z=-40.0 to 40.0

Opera

Thermal Test (with help from Jeff C.)

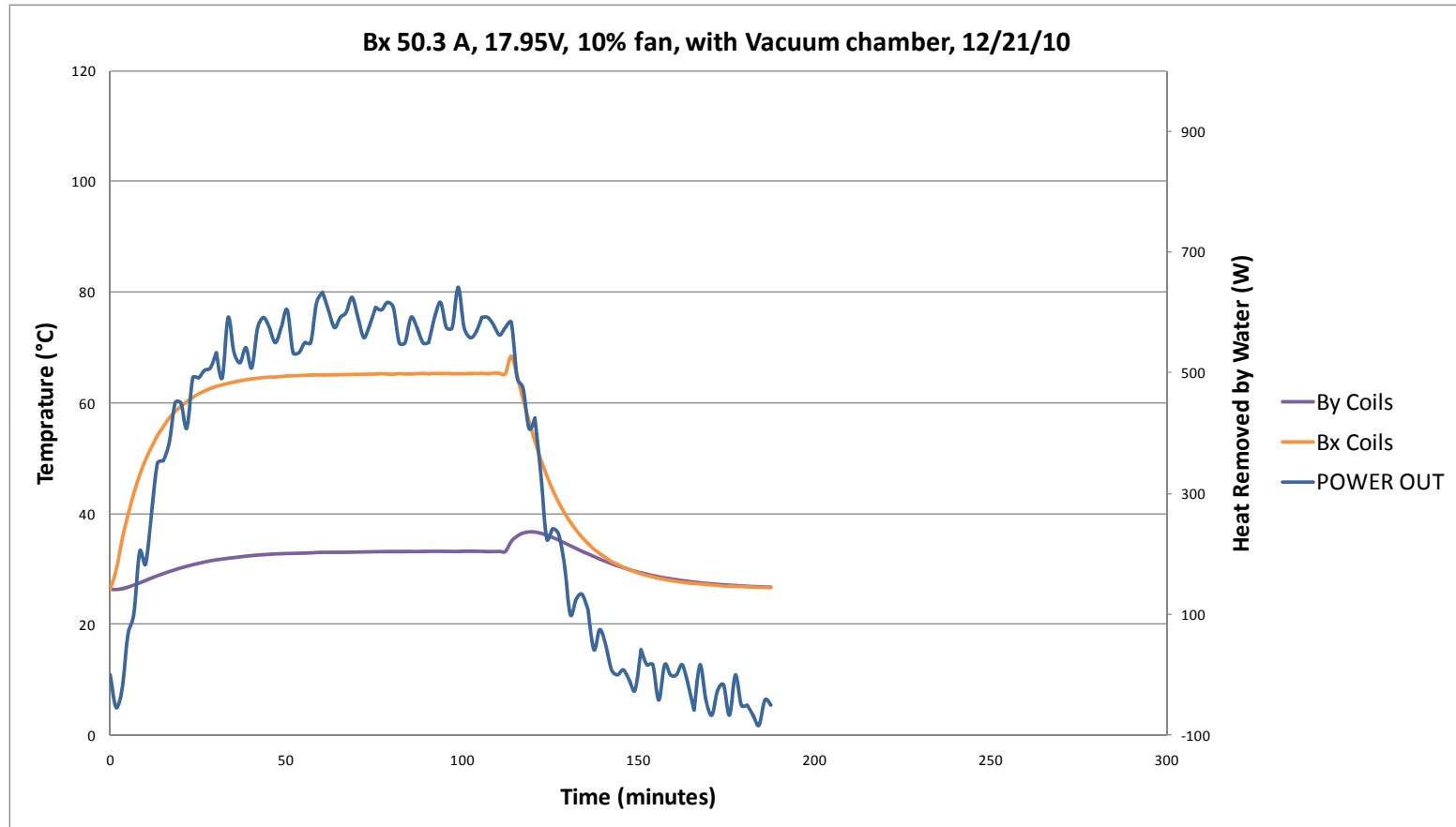


With Vacuum Chamber

Bx 50.3 Amps
18.85 V
No fan
949 Watts total in
until 137 minute mark
then power off

827 W removed by water
87% removed by water

Thermal Test (with help from Jeff C.)



With Vacuum Chamber

Bx 50.3 Amps
17.95 V
10% fan
903 Watts total in
until 111 minute mark
then power off and fan off

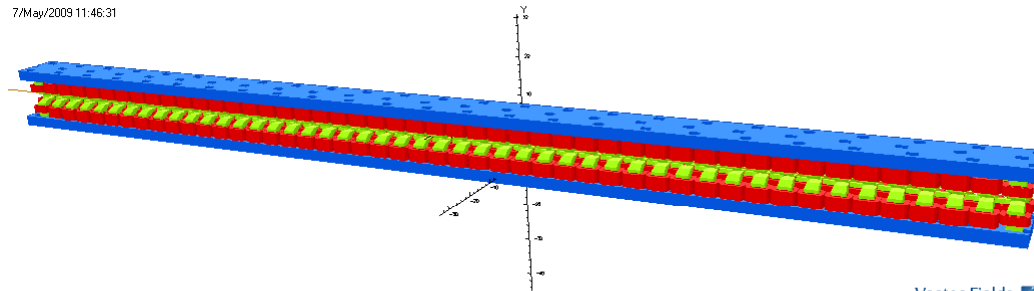
578 W removed by water
64% removed by water

Tunnel Heating

- Without the fan turned on ~1500 W of heat will leak into the tunnel at full current.
- With the fan turned on ~3500 W of heat will leak into the tunnel at full current.
- Sometimes the device is on full current. Sometimes the device is off. Sometimes the device operates somewhere in-between.
- The heat into the tunnel is not constant. This make the tunnel temperature difficult to control.
- Reversing the fan and sucking the heat from the device into the tunnel air handling system eases controlling the tunnel temperature
 - Suggested by Marvin K.
- This minimizes the heat leaking into the tunnel.
- A smoke test with a reversed fan showed adequate good air flow.
- A thermal test showed similar coil cooling.

Quasi-periodicity with an Electromagnet Device

7/May/2009 11:46:31

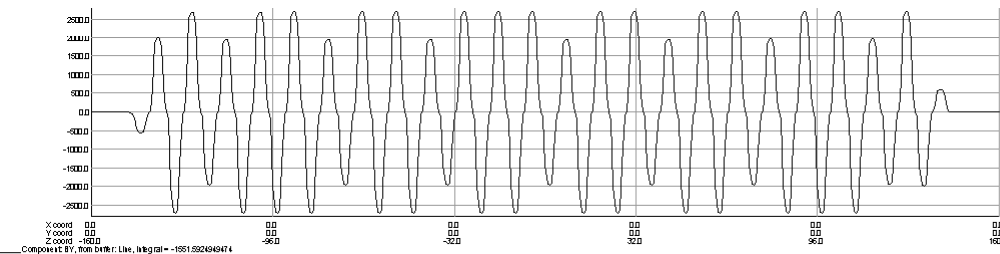


Vector Fields
software for electromagnetic design

Energy	J
Mass	g
PROBLEM DATA	
24_period_QP_circ_3_5_12_13_18_19_2	
TOSCA Magnetostatic	
Nonlinear materials	
Simulation No 7 of 8	
19466875 elements	
6720933 nodes	
150 conductors	
Nodally interpolated fields	
Activated in global coordinates	
Field Point Local Coordinates	
Local = Global	
FIELD EVALUATIONS	
Line	LINE 401 Cartesian
(nodal)	
x=0.0, y=0.0, z=-160.0 to 160.0	

24 Period Model Shown

7/May/2009 11:41:42

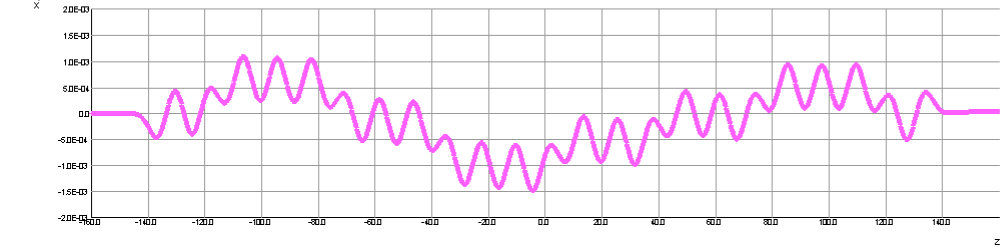


Vector Fields
software for electromagnetic design

Energy	J
Mass	g
PROBLEM DATA	
24_period_QP_circ_3_5_12_13_18_19_2	
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FIELD EVALUATIONS	
Line	LINE 401 Cartesian
(nodal)	
x=0.0, y=0.0, z=-160.0 to 160.0	

Quasiperiodic By Field

7/May/2009 11:58:59

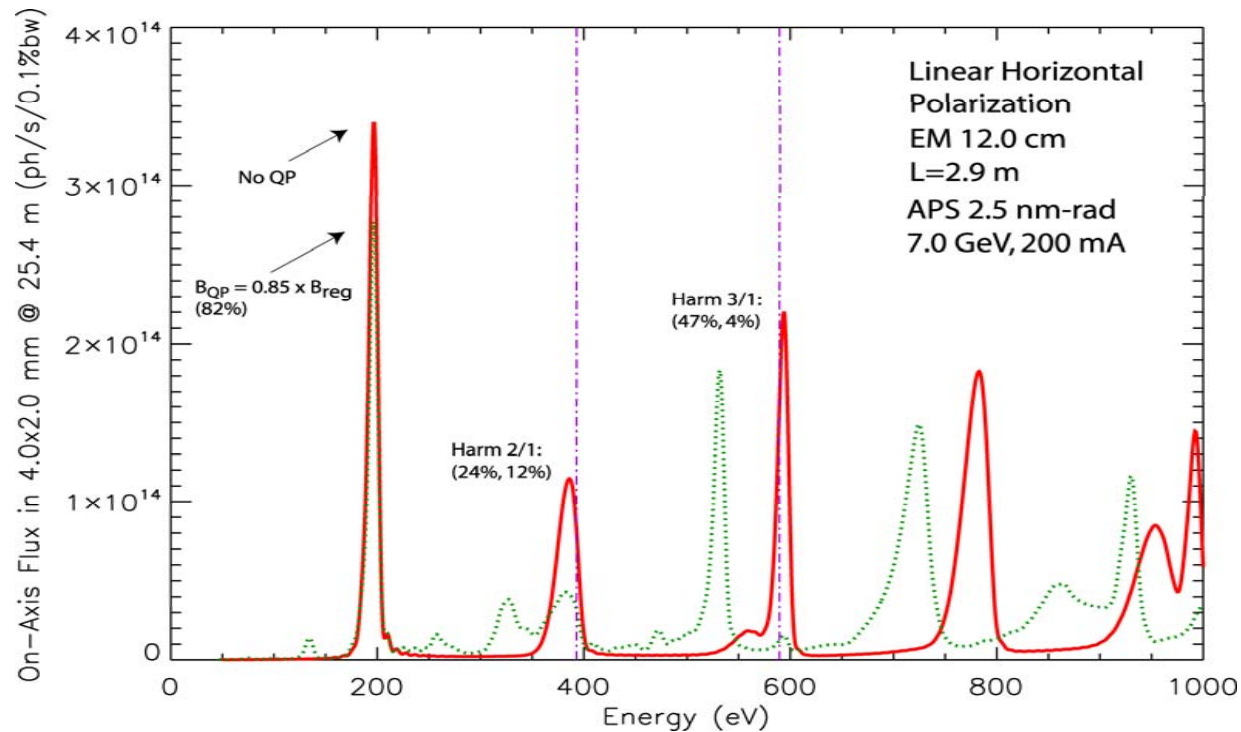


Vector Fields
software for electromagnetic design

Energy	J
Mass	g
PROBLEM DATA	
24_period_QP_circ_3_5_12_13_18_19_2	
TOSCA Magnetostatic	
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Simulation No 7 of 8	
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x=0.0, y=0.0, z=-160.0 to 160.0	

Quasiperiodic Electron Trajectory

Quasi-periodicity Suppresses the Higher Harmonics



Flux with and without quasi-periodicity turned to a 15% field-strength reduction at the QP poles for the EM. The 3rd harmonic is reduced by over 90% while the first harmonic is reduced by ~18%.

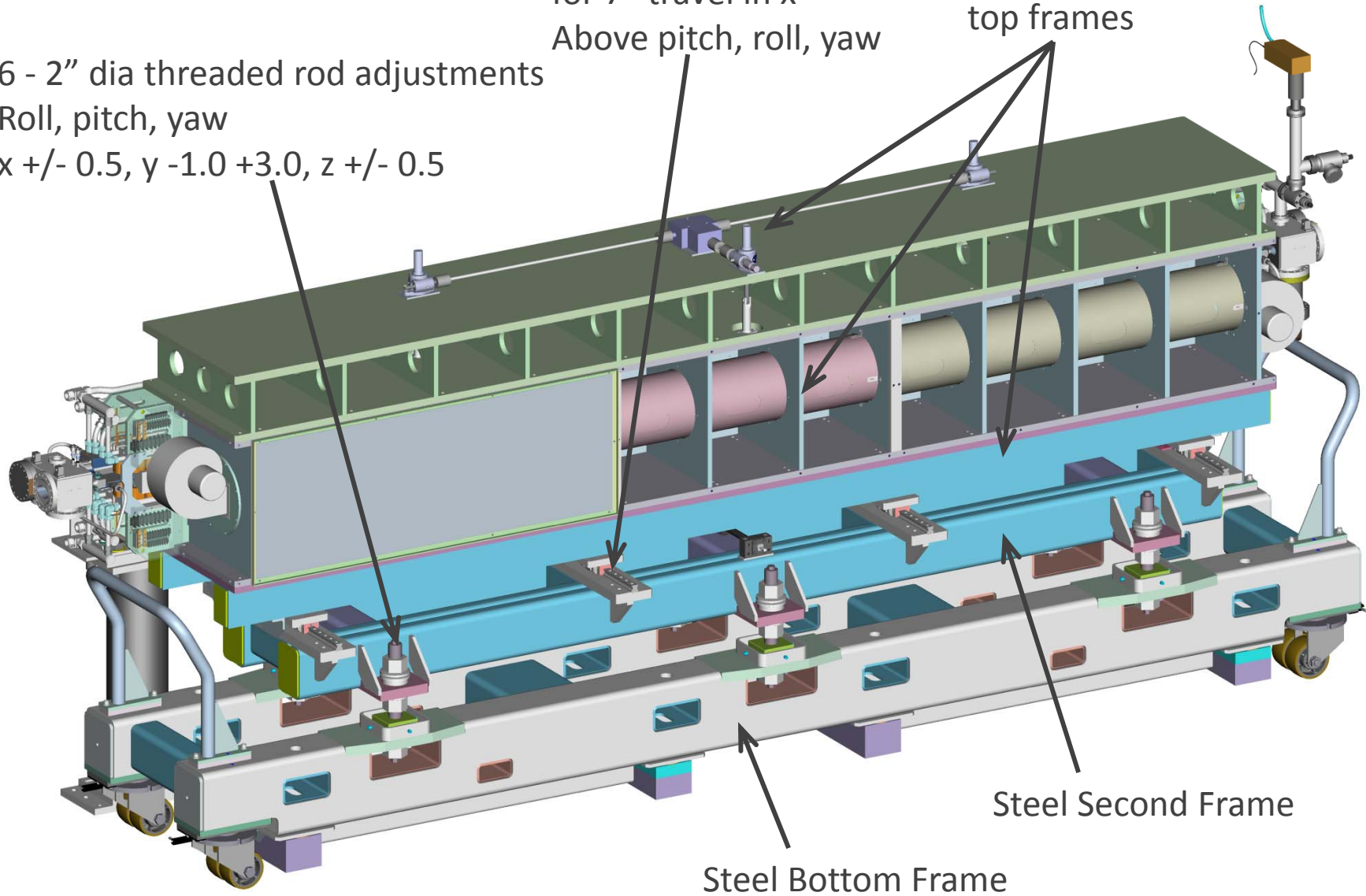
R. Dejus et al., Spectral Performance Of Circular Polarizing Quasi-periodic Undulators For Soft X-rays At The Advanced Photon Source, PAC09

IEX Layout

6 - 2" dia threaded rod adjustments
Roll, pitch, yaw
x +/- 0.5, y -1.0 +3.0, z +/- 0.5

Linear Roller bearings
for 7" travel in x
Above pitch, roll, yaw

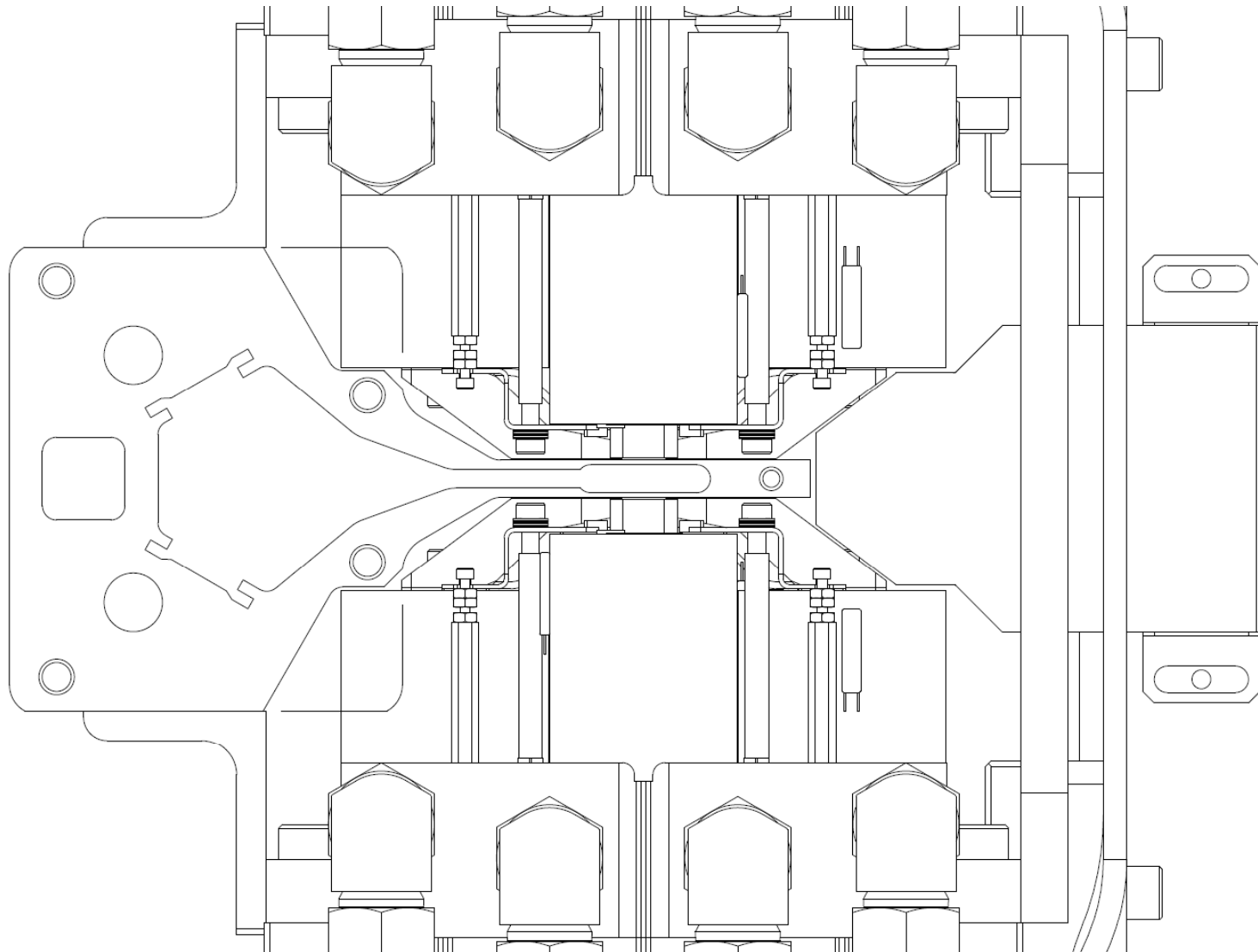
Welded aluminum
top frames



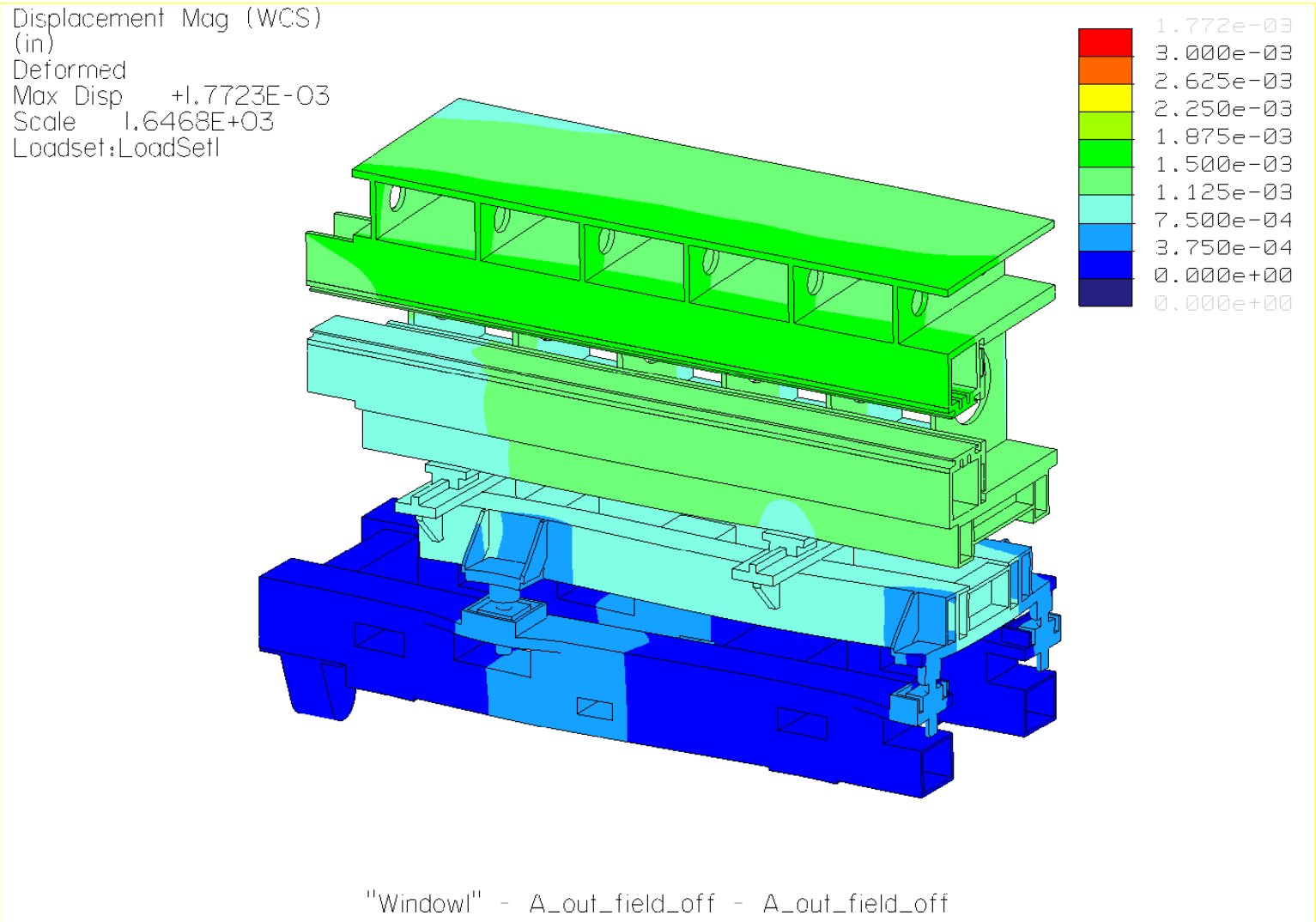
Steel Second Frame

Steel Bottom Frame

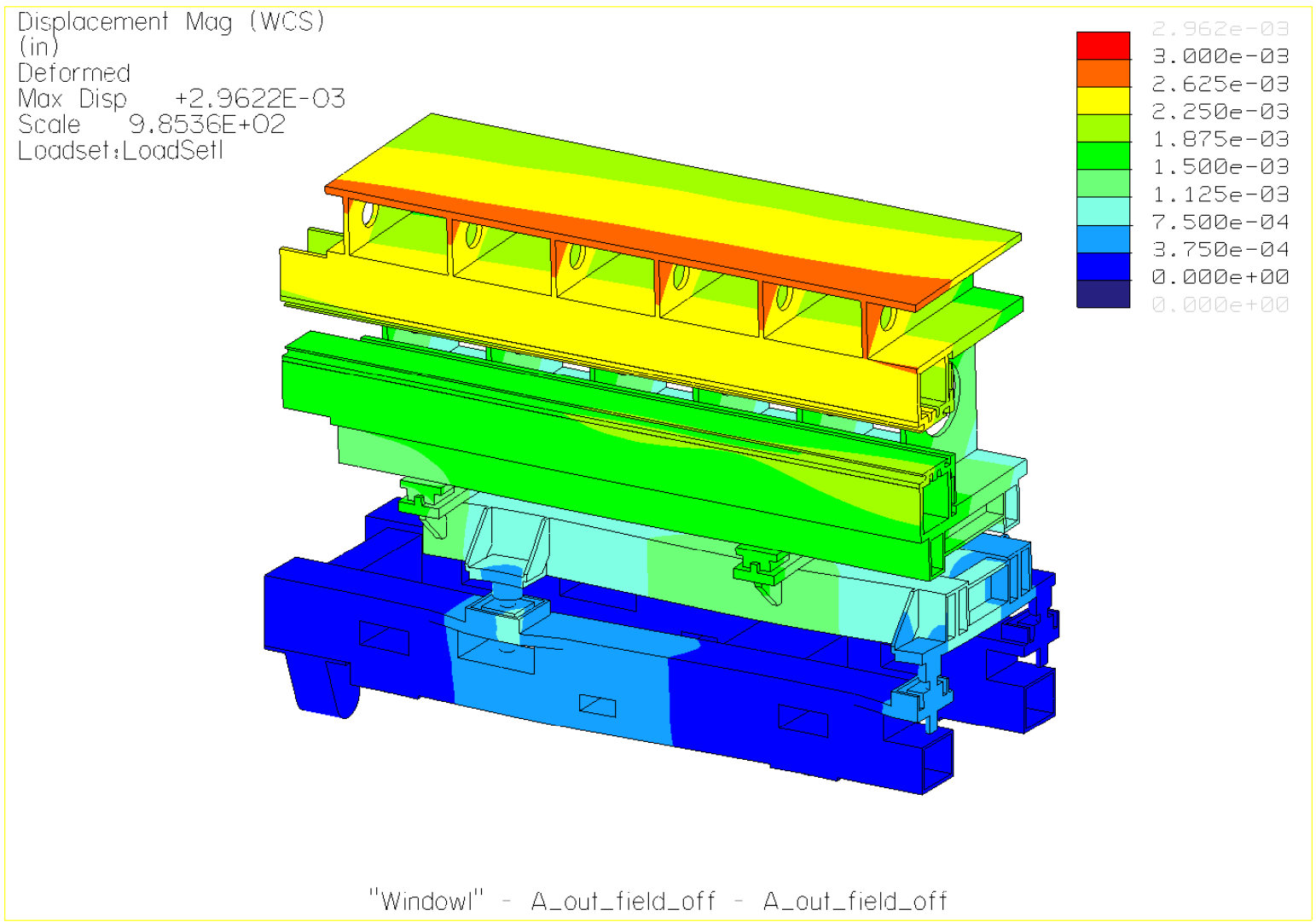
Modified Vacuum Chamber



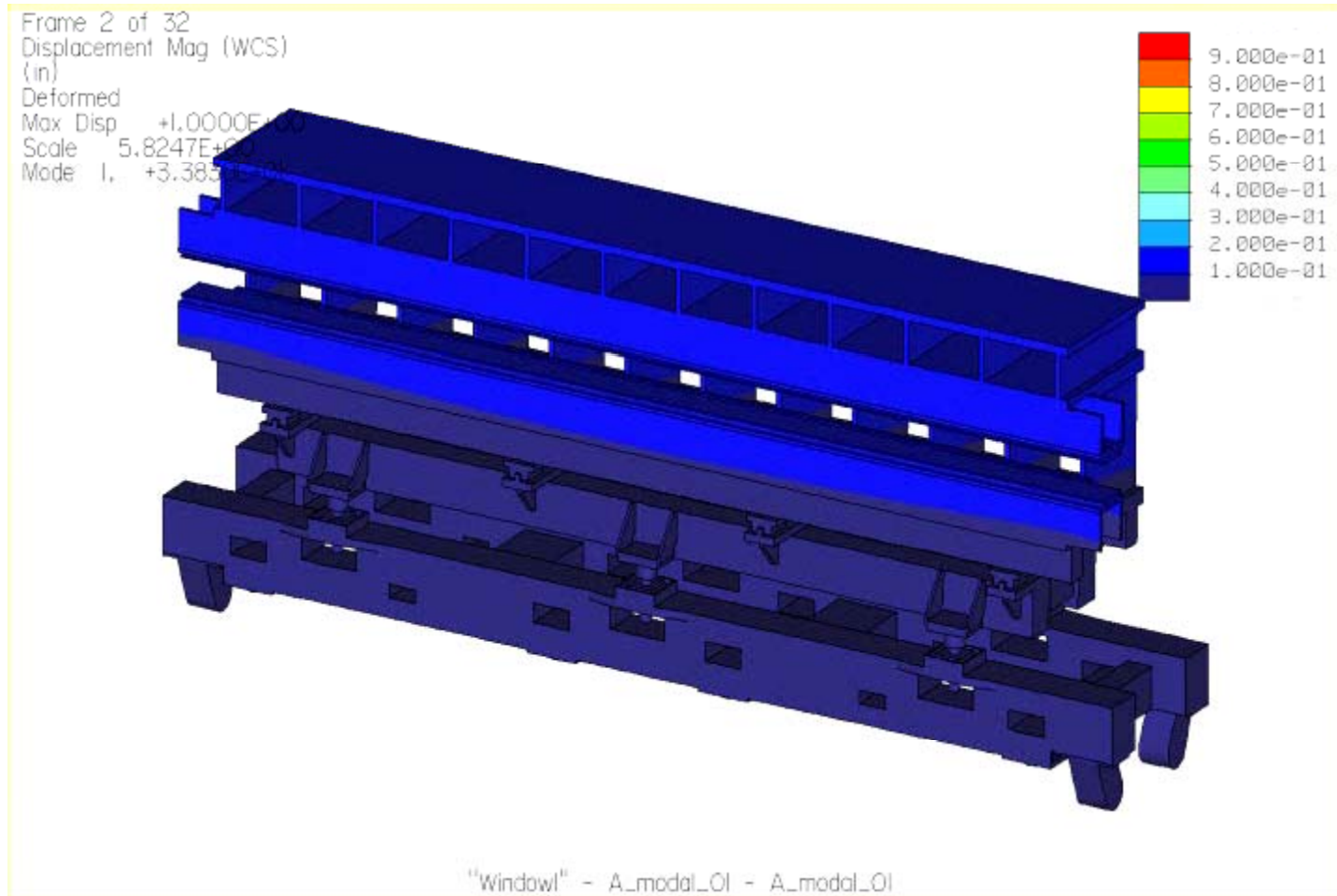
Assembled Position (out position)



Jaw drops 10 microns (0.00040") from out to in.

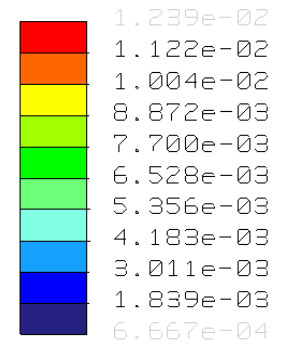
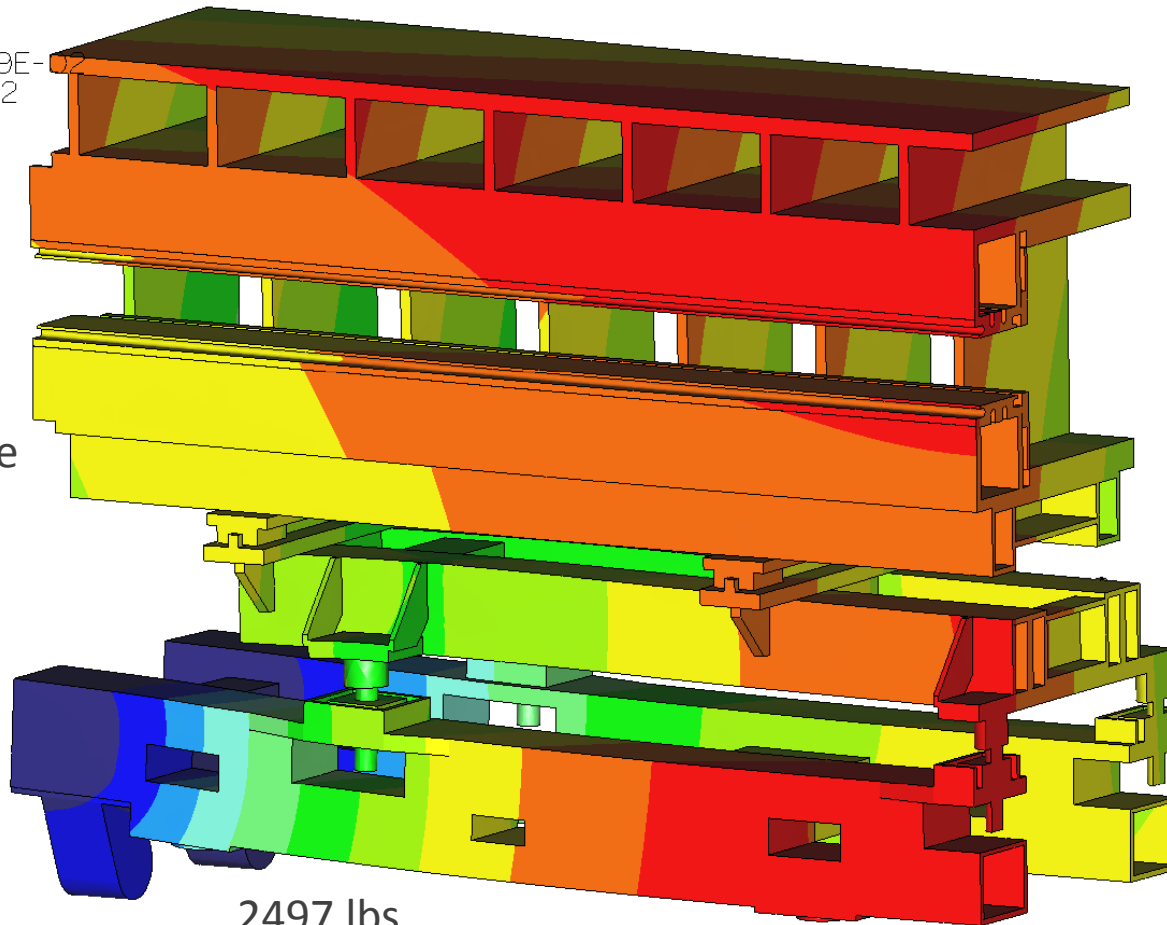


Fundamental Harmonic 33.8 Hz.



Load on casters (in position)

Displacement Mag (WCS)
 (in)
 Deformed
 Max Disp +1.2389E-02
 Scale 2.3431E+02
 Loadset:LoadSet1



A 1400 lb force at the top will cause this device to tip.

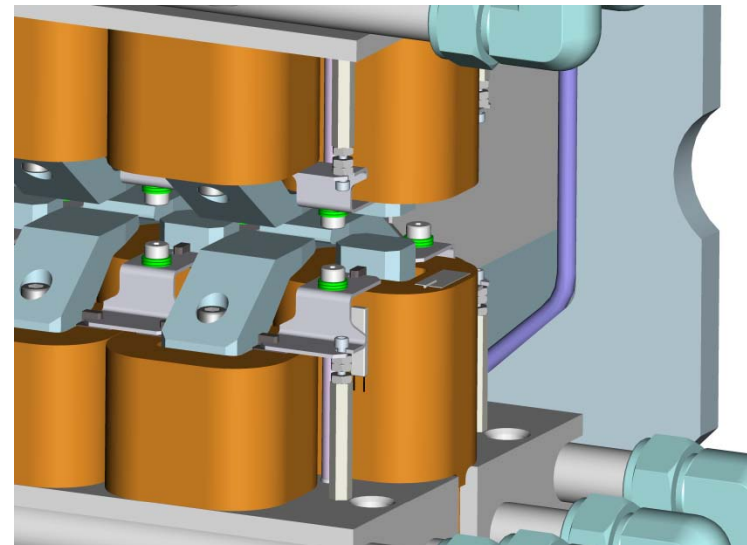
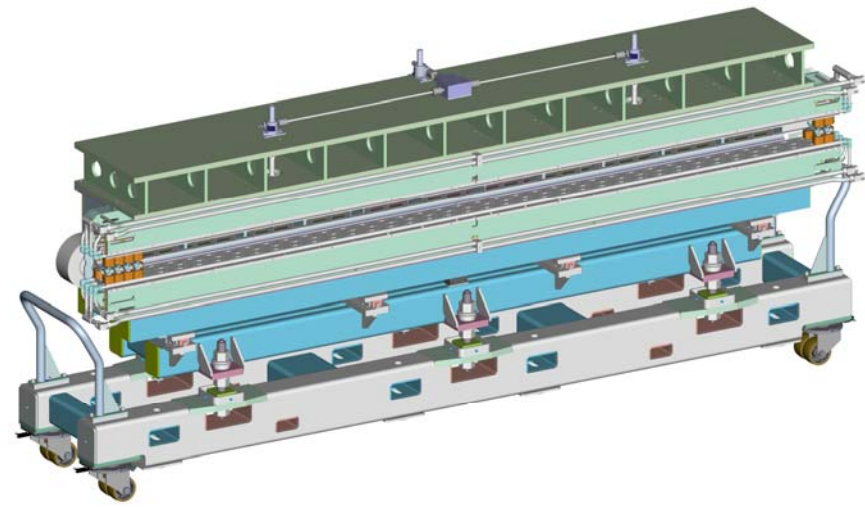


A double wheel caster with a 5,000 lb rating will be used.

4141 lbs 2497 lbs
 "Window1" - A_casters__in - A_casters__in

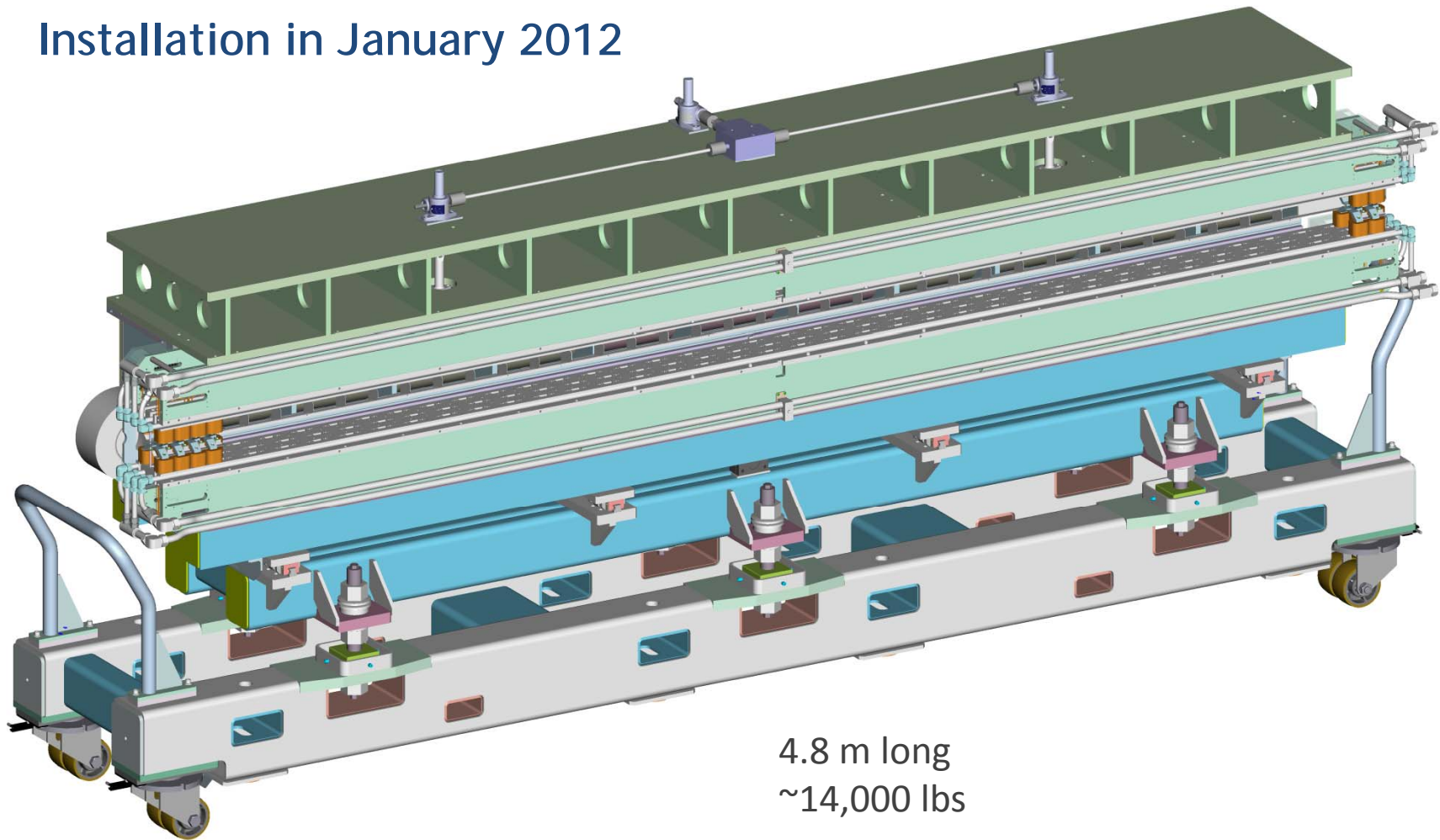
Selected Features

- ~200 lbs to push to get rolling on casters.
- 34" wide, 194" long, 57.2" tall on casters.
- An acme screw will be provided to move the jaws in or out of operating position.
- 456 coils and 16 power supplies.



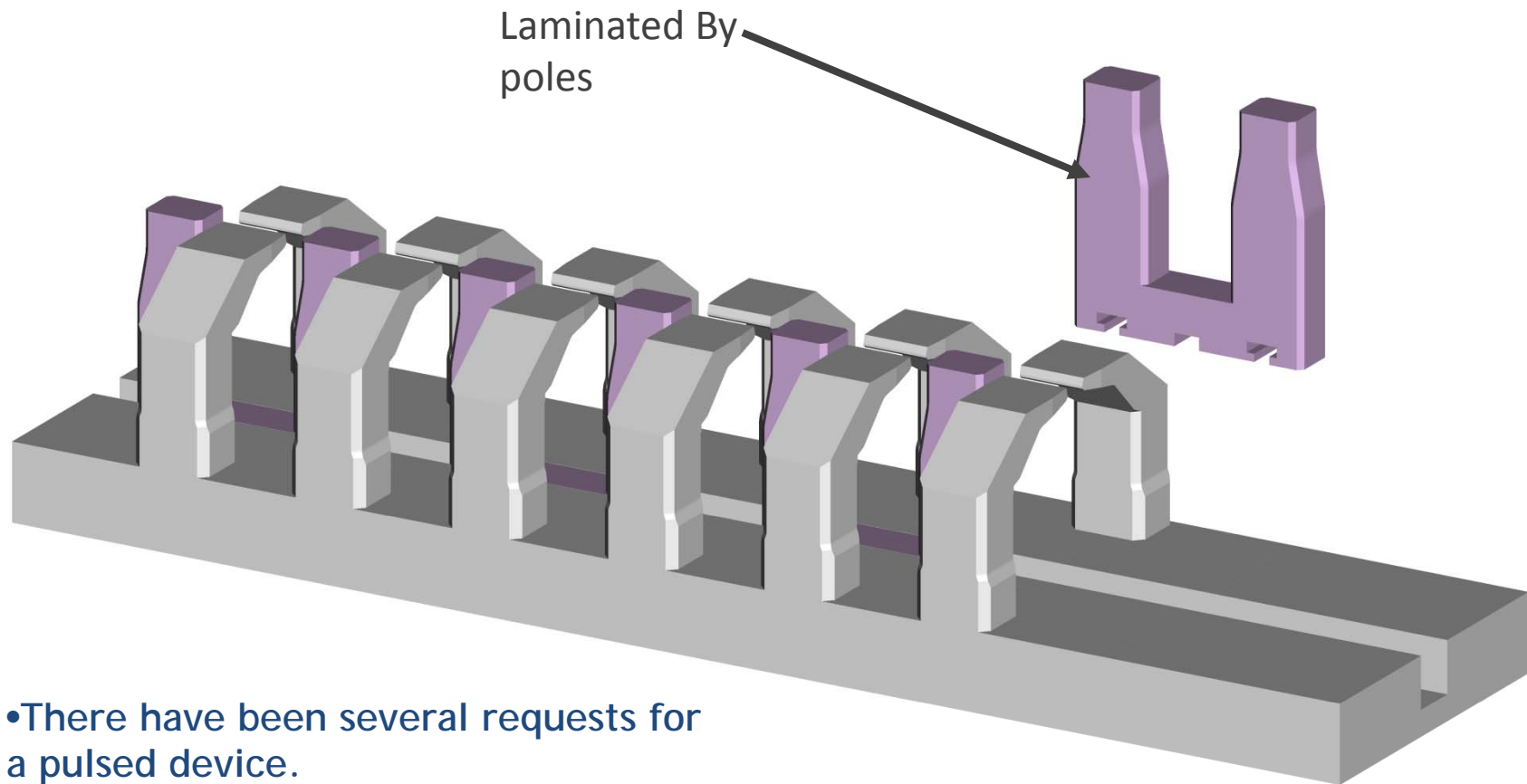
IEX Device

Installation in January 2012



4.8 m long
~14,000 lbs

Laminated Assembly Proposal



- There have been several requests for a pulsed device.



Thank You

