

Coaxial Elliptic Helical Undulator

A design concept for an undulator that generates polarized magnetic fields of linear, circular, and elliptical modes

Suk Hong Kim

Magnetic Devices Group

August 22, 2011

Outline

- Motivated from “Is it possible to change the nature of the circular polarization and to obtain linearly polarized radiation from the same undulator?” [1]
- Magnetic field of a solenoid
- Characteristics of helical undulator magnetic field
- Coaxial (circular) helical undulator
- Coaxial elliptic helical undulator
- Compare the polarized fields with those of an APPLE-II
- Conclusion

[1] D.F. Alferov *et al.*, Sov. Phys. Tech. Phys. 21 (1976) 1408

Magnetic field of an infinitely long helical solenoid

- One-layer solenoid is always helical with a winding pitch angle
- The helix is wound on radius r_0 with a filamentary wire
- Calculate on-axis transverse fields from the Biot-Savart law [2]

$$B_{axis}^z = \frac{\mu_0 I_1}{4\pi} \int \frac{[d\mathbf{s} \times \mathbf{r}]_z}{r^3} = \mu_0 n_s I_1$$

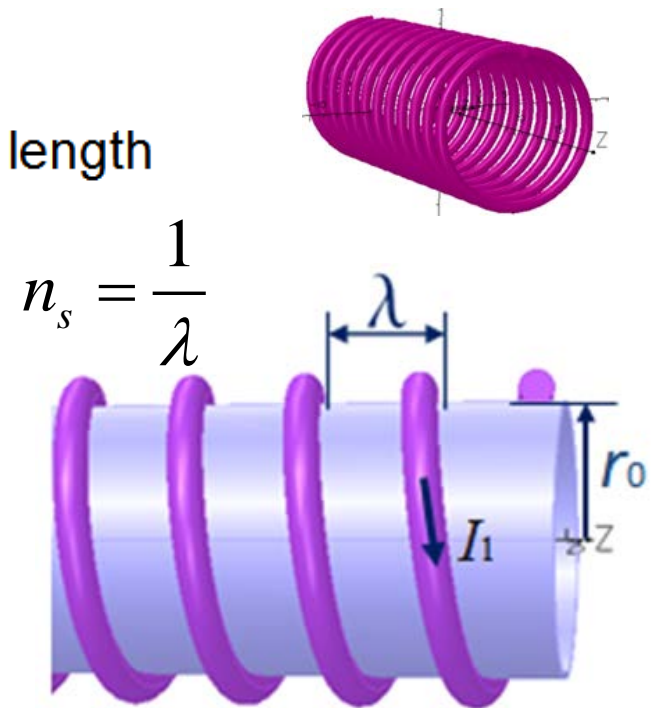
$n_s = \#$ of turns per unit length

$$B_{axis}^y = \frac{\mu_0 I_1}{4\pi} \int \frac{[d\mathbf{s} \times \mathbf{r}]_y}{r^3}$$

$$= \frac{\mu_0 I_1}{\lambda} \left\{ \left(\frac{2\pi}{\lambda} r_0 \right) K_0 \left(\frac{2\pi}{\lambda} r_0 \right) + K_1 \left(\frac{2\pi}{\lambda} r_0 \right) \right\}$$

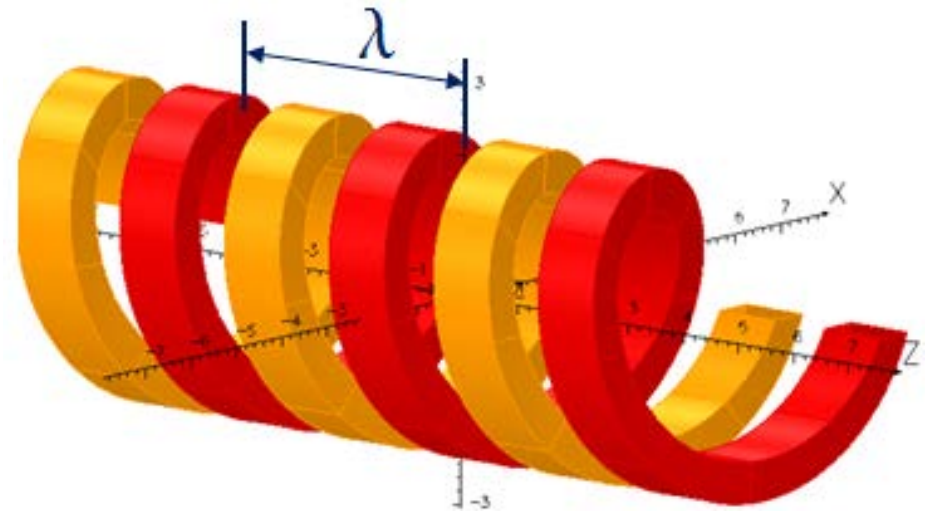
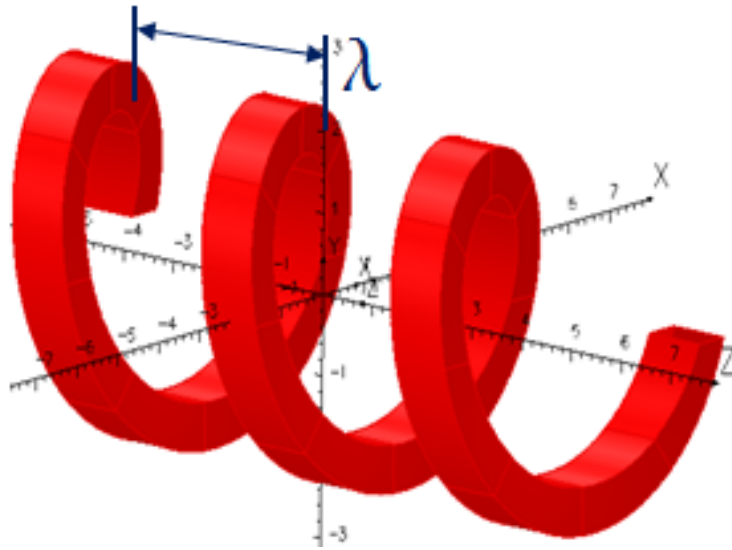
$$B_{axis}^x = 0 \quad \sim \exp\left(-2\pi \frac{r_0}{\lambda}\right)$$

$$\mathbf{B}_{axis}^{tran} = B_{axis}^{tran} \left\{ \hat{x} \cos\left(\frac{2\pi}{\lambda} z\right) + \hat{y} \sin\left(\frac{2\pi}{\lambda} z\right) \right\}$$



[2] W.R. Smyth, *Static and Dynamic Electricity* (McGraw-Hill, New York, 1939), p. 272

Rectangular conductors



B_x in the previous slide at $z = 0$ is zero because the x-axis goes through the both red and yellow conductors and the field integral of the Biot-Savart law is anti-symmetrical with respect to the coil-winding pitch angle.

Bifilar Helix as a Helical Undulator

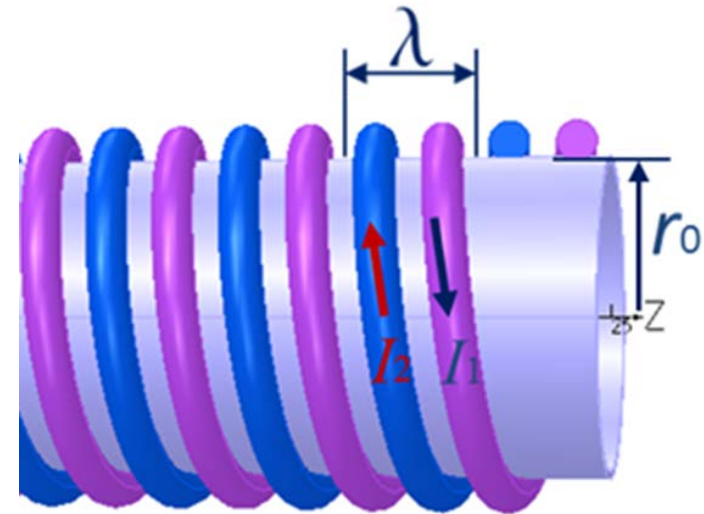
$$\mathbf{B}_{axis}^{tran} = B_{axis}^{tran} \left\{ \hat{r} \cos\left(\frac{2\pi}{\lambda} z - \phi\right) + \hat{\phi} \sin\left(\frac{2\pi}{\lambda} z - \phi\right) \right\}$$

$$\mathbf{B}_{axis}^{tran} = B_{axis}^{tran} \left\{ \hat{x} \cos\left(\frac{2\pi}{\lambda} z\right) + \hat{y} \sin\left(\frac{2\pi}{\lambda} z\right) \right\}$$

$$B_{axis}^z = \frac{\mu_0}{\lambda} (I_1 - I_2) \rightarrow 0$$

$$\rightarrow 2I$$

$$B_{axis}^{tran} = \frac{\mu_0 (I_1 + I_2)}{\lambda} \left\{ \left(\frac{2\pi}{\lambda} r_0\right) K_0\left(\frac{2\pi}{\lambda} r_0\right) + K_1\left(\frac{2\pi}{\lambda} r_0\right) \right\}$$



- Assumes infinitesimal cross section of the wire
- The on-axis field is proportional to the current in the wire

[3] B.M. Kincaid, J. Appl. Phys. 48 (1977) 2684

[4] J.P. Blewett and R. Chasman, J. Appl. Phys. 48 (1977) 2692



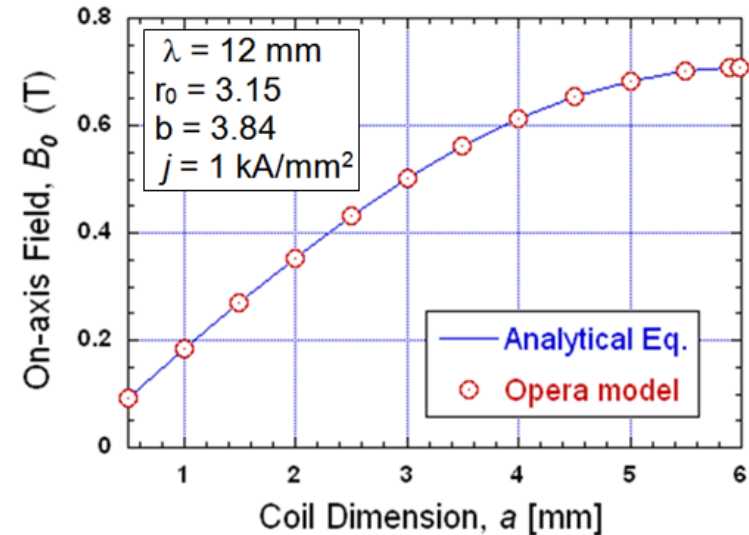
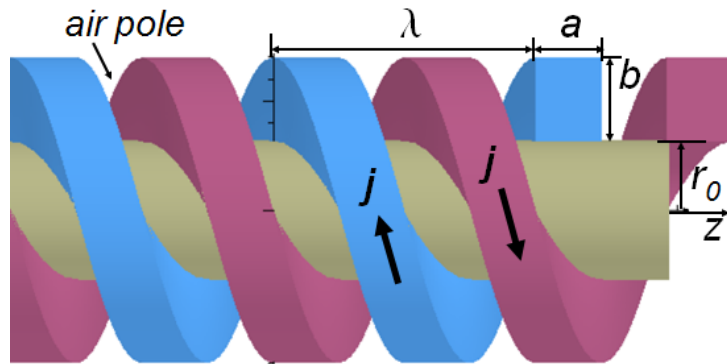
(Circular) Helical Undulator

$$B_{axis}^{n=1} = \frac{\mu_0 2 j \lambda}{\pi} \sin\left(k \frac{a}{2}\right) \int_{r_0}^{r_0+b} \left\{ kr K_0(kr) + K_1(kr) \right\} \frac{dr}{\lambda}$$

$$(k = \frac{2\pi}{\lambda})$$

j : coil current density

$$\mathbf{B}_{axis}^{tran} = B_{axis}^{n=1} \{ \hat{x} \cos(kz) + \hat{y} \sin(kz) \}$$



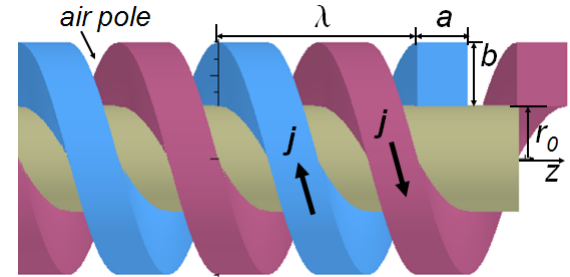
- We have an analytical expression with coil cross sections [4]
- Agrees with model calculations: field within 3×10^{-5} , higher harmonics $\ll 2 \times 10^{-7}$
- When undulator dimensions are scaled according to λ , the field remains unchanged for $j\lambda = \text{constant}$

[5] S.H. Kim, Nucl. Instr. and Meth. A 584 (2008) 266

(Circular) Helical Undulator: off-axis field

$$B_{axis}^n = \frac{2\mu_0 j \lambda}{\pi} \sin\left(\frac{nka}{2}\right) \int_{r_0}^{r_0+b} \{nkrK_{n-1}(nkr) + K_n(nkr)\} \frac{dr}{\lambda} \quad (k = \frac{2\pi}{\lambda})$$

$$\mathbf{B}(0 \leq r < r_0) = \sum_{n=1,3,5..}^{\infty} B_{axis}^n \cdot \{\hat{r}B_r^n + \hat{\phi}B_{\phi}^n + \hat{z}B_z^n\}$$

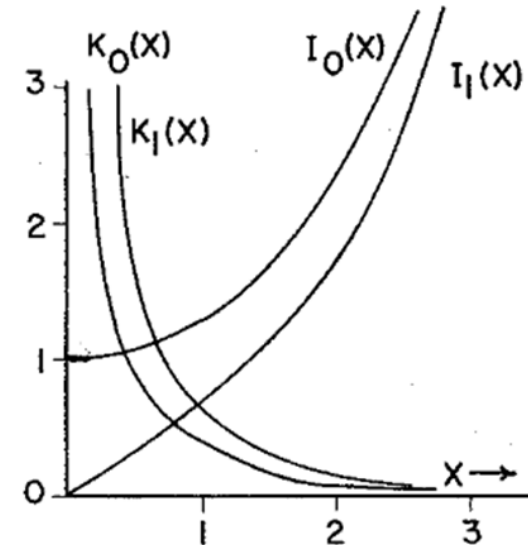


$$B_r^n = [I_{n-1}(nkr) + I_{n+1}(nkr)] \cdot \cos[n(kz - \phi)]$$

$$B_{\phi}^n = \left(\frac{2}{kr}\right) I_n(nkr) \cdot \sin[n(kz - \phi)]$$

$$B_z^n = (-2) I_n(nkr) \cdot \sin[n(kz - \phi)]$$

I_n, K_n : modified Bessel functions



$$B_r^1 = \left[1 + \frac{3(kr)^2}{8} + \frac{5(kr)^4}{192} + \dots\right] \cos(kz - \phi)$$

$$B_{\phi}^1 = \left[1 + \frac{(kr)^2}{8} + \frac{(kr)^4}{192} + \dots\right] \sin(kz - \phi)$$

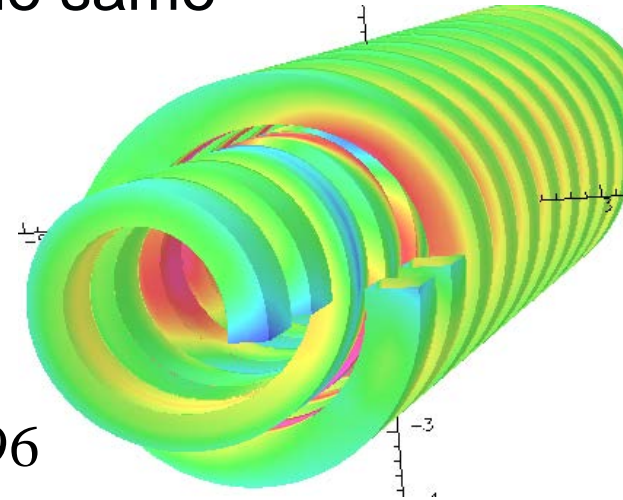
$$B_z^1 = -\left[kr + \frac{(kr)^3}{8} + \dots\right] \sin(kz - \phi)$$

Coaxial (Circular) Helical Undulator

- Inner/outer two helical undulators have coil-winding pitch angles in the opposite directions along the same undulator axis

$$\begin{cases} \mathbf{B}_{in} = B_{axis}^{in} \{ \hat{r} \cos(kz - \phi) + \hat{\phi} \sin(kz - \phi) \} \\ \mathbf{B}_{out} = B_{axis}^{out} \{ \hat{r} \cos(kz + \phi) - \hat{\phi} \sin(kz + \phi) \} \end{cases}$$

$$\begin{cases} \mathbf{B}_{in} = B_{axis}^{in} \{ \hat{x} \cos(kz) + \hat{y} \sin(kz) \} \\ \mathbf{B}_{out} = B_{axis}^{out} \{ \hat{x} \cos(kz) - \hat{y} \sin(kz) \} \end{cases} \quad \begin{cases} B_{axis}^{in} (T) = 0.8696 \\ B_{axis}^{out} (T) = 0.4881 \end{cases}$$

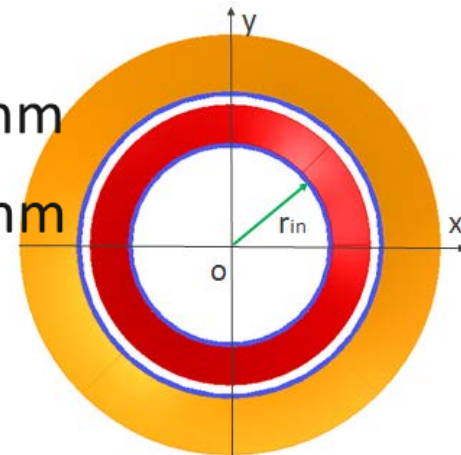


- Calculated $\sim j(\text{critical})$ @4.2 K
- Linear polarizations, for example:

$$I_{in} \rightarrow \frac{B_{axis}^{out}}{B_{axis}^{in}} I_{in} \quad I_{out} \rightarrow \pm I_{out}$$

Period = 38 mm

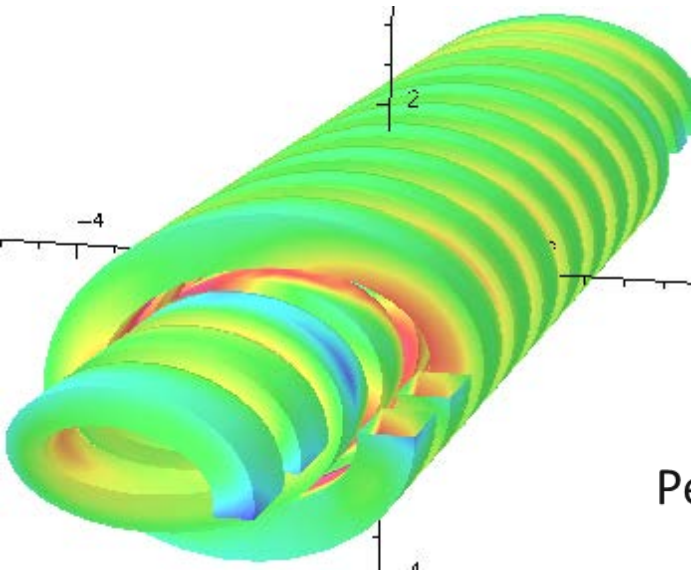
$r_{in} = 11$ mm



Coaxial Elliptic Helical Undulator

- Could not derive an analytical expression yet for an ellipse
- By modifying the cross section from the circular to an ellipse,

 $B_x \rightarrow \sim 1.2 B_x$ $B_y \rightarrow \sim 2 B_y$



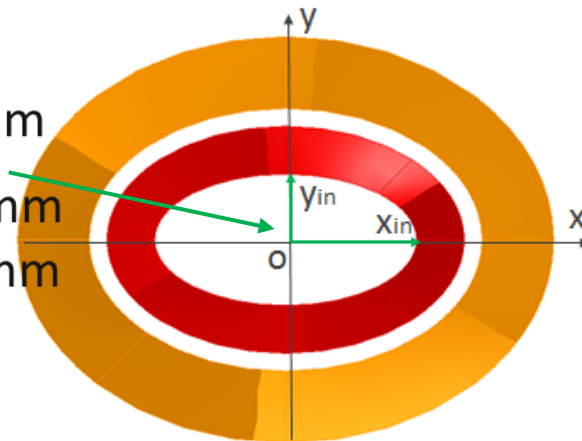
$$\left[\begin{aligned} \mathbf{B}_{in} &= B_{axis}^{in} \{ \hat{x} f_{in} \cos(kz) + \hat{y} \sin(kz) \} \\ \mathbf{B}_{out} &= B_{axis}^{out} \{ \hat{x} f_{out} \cos(kz) - \hat{y} \sin(kz) \} \end{aligned} \right.$$

$$\left[\begin{aligned} \mathbf{B}_{in}(T) &= 1.8175 \cdot \{ \hat{x} \cdot 0.6335 \cdot \cos(kz) + \hat{y} \sin(kz) \} \\ \mathbf{B}_{out}(T) &= 1.0048 \cdot \{ \hat{x} \cdot 0.6216 \cdot \cos(kz) - \hat{y} \sin(kz) \} \end{aligned} \right.$$

Period = 38.0 mm

$x_{in} = 11.0$ mm

$y_{in} = 5.5$ mm



Calculated polarized fields are compared with those of an APPLE-II [6]

Type	Period/gap (mm)	Circular field (T)	Vertical field (T)	Horizontal field (T)	Elliptical field (T)
APPLE-II*	38/9.5	0.566	0.9292	0.7139	$B_y = 0.8486$ $B_x = 0.2908$
Elliptic Helical	38/11	1.407	1.990	1.261	B_y B_x 1.421 0.642 0.422 2.258 1.152 0.818 0.625 -1.005
Elliptic Helical	26.6/11	0.580	1.305	0.696	B_y B_x 0.974 0.533 0.282 1.881 0.628 1.207 0.346 -0.674

*Calculated by S. Sasaki with $B_r = 1.27$ T

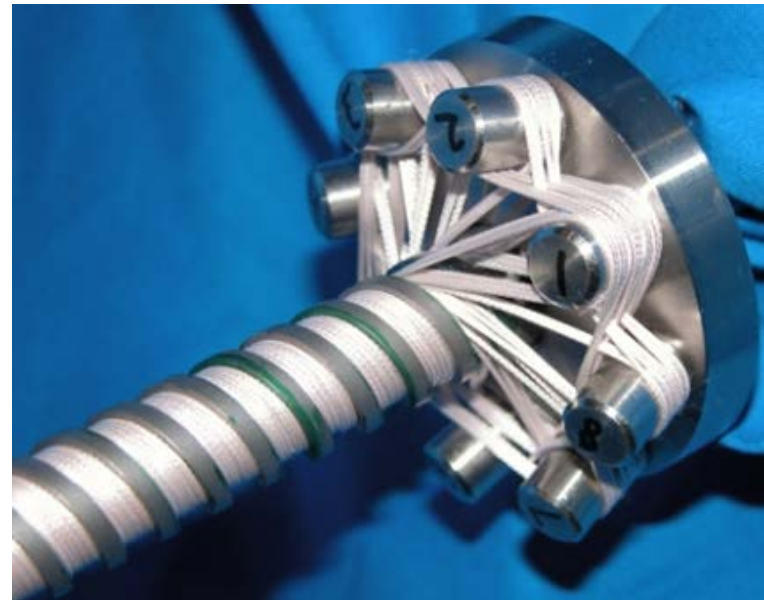
[6] S. Sasaki, Nucl. Instr. And Meth. A 347 (1994) 83

$j \lambda$ constant scaling law for an Elliptic Helical Undulator

- U38: $\lambda = 38$ mm, $j = 1.0$ kA/mm²
- U76: $\lambda = 76$ mm, $j = 0.5$ kA/mm²
- U38x0.7: $\lambda = 26.6$ mm, $j = 1/0.7$ kA/mm²
- $\rightarrow j \lambda = 38$ kA/mm for the three
- Have the same calculated on-axis fields within ~ 1 mT

Issues

- Tolerances for the coaxial alignment
- Effective magnetic lengths of the inner and outer units
- Off-axis field
- One end for the inner unit
- - - -



Conclusion

- Proposed a coaxial elliptic helical undulator for use in a storage ring
- The undulator partially follows the $j\lambda$ constant scaling law
- Calculated polarized fields for a period of 38 mm were about twice of those for an APPLE-II
 - Fields for a period of 26.6 mm were slightly higher than those for the 38-mm APPLE-II
- Need further analysis