

# P0 Transverse feedback development

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# Contributors

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# Acknowledgements

Leonard Morrison, Suk Kim, Yong-chul Chae, Chuck Gold, Bob Laird, Pat Dombrowski, Louis Emery, Frank Lenkszus, Randy Zabel, Glenn Decker, Hang Bui, Bob Lill, M. Borland, T. Nakamura, J. Fox, Louis Emery.

# Outline

- Project history
- Recent test results
- Some background on feedback systems
- System description
- Further upgrade plan



# System objective

- APS storage ring beam instabilities are mainly controlled with chromaticity adjustment:
  - Chromaticities of 6 to 7 are necessary for 24 singlet fill
  - and 11 to 12 for hybrids fill due to high single-bunch charge (16mA) in the leading bunch.
  - Some sextupole are at maximum current even after the pole tips are shimmed to increase flux.
- High chromaticity has some side effects:
  - reduces beam dynamic aperture and shortens beam lifetime.
  - Also makes the injection close-bump hard to match.
  -
- New development of APS upgrade lattice requires to use feedback system to stabilize beam with reduced chromaticity.



## System objective (cont.)

- Reduce chromaticity while keep beam stable.
- Increase beam lifetime.
- Increase single bunch beam current accumulation limit.
- As an additional tool for development of high current or low emittance configurations in the future.



# Project history and status

- 2007 and before: Proposal, design, component test.
- 2008: FPGA development and system integration. Started closed-loop test.
- 2009: major improvement to overcome insufficient horizontal drive.
  - Two new 500-Watt amplifiers.
  - A new longer horizontal kicker stripline.
  - New location in S35 for the horizontal stripline which has high betax.
  - Remote DAC through fiber link to transmit data stream from S2 to S35 with a rate of 2.36 GBS.
- 2010: completed 24-singlet and hybrids-fill test with reduced chromaticity of -2.0 in each plane.
- The system has been evaluated during user operation and will be used for user operations starting coming runs.



# Ring parameters

Beam energy ( $E_0$ ): 7 GeV.

Beta function at pickup ( $\beta_x / \beta_y$ ): 6.28/24.34 m.

Beta function at kicker ( $\beta_x / \beta_y$ ): 20.23/24.91 m (different locations).

Betatron tunes ( $\nu_x / \nu_y$ ): 36.17/19.3.

Synchrotron Damping time ( $\tau_x, \tau_y$ ): 9.6 /9.6 ms.

Harmonic number(h) 1296.

Bucket spacing: 2.84 ns.

Revolution frequency( $f_0$ ): 271 KHz.

Source size ( $\sigma_x, \sigma_y$ ): 270(120)/11  $\mu\text{m}$ .



# System parameters

Required pickup resolution ( $\mu\text{m}$ ): 10/2  
Required noise level ( $\mu\text{m}$ ): 5/2  
Dynamic range ( $\mu\text{m}$ ): 1000/500  
stripline kick strength( $\mu\text{Rad}$ ): 0.78 / 0.26  
Actual A/D bits : 14/14  
Actual DAC bits: 14/14  
Sample rate(MHz): 117 (352\*)  
Damping time: 0.5 ms / 0.05 ms\*\*

\* with FPGA upgrade  
\*\* Measured.



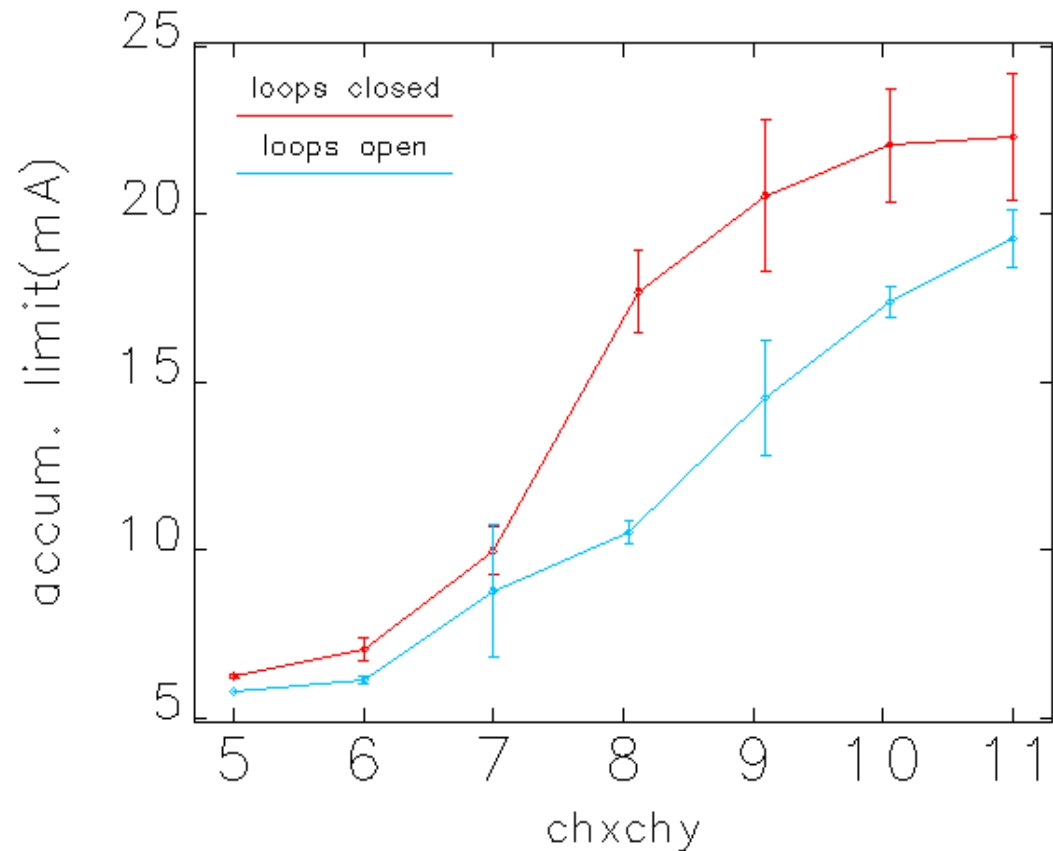
# Recent test results

Table1: Beam parameters of 24-singlet fill with and without feedback.

	Loops open	Loops closed
chx/chy	7/6	3/2
x-emitt.(nm)	2.45	2.5
y-emitt.(nm)	0.054	0.06
coupling(%)	2.2	2.22
xRMS-30Hz (um)	2.73	2.45
xRMS-full BW(um)	8.72	6.05
yRMS-30Hz (um)	1.24	0.75
YRMS-full BM(um)	2.96	3.17
Beam life(min.)	443	878

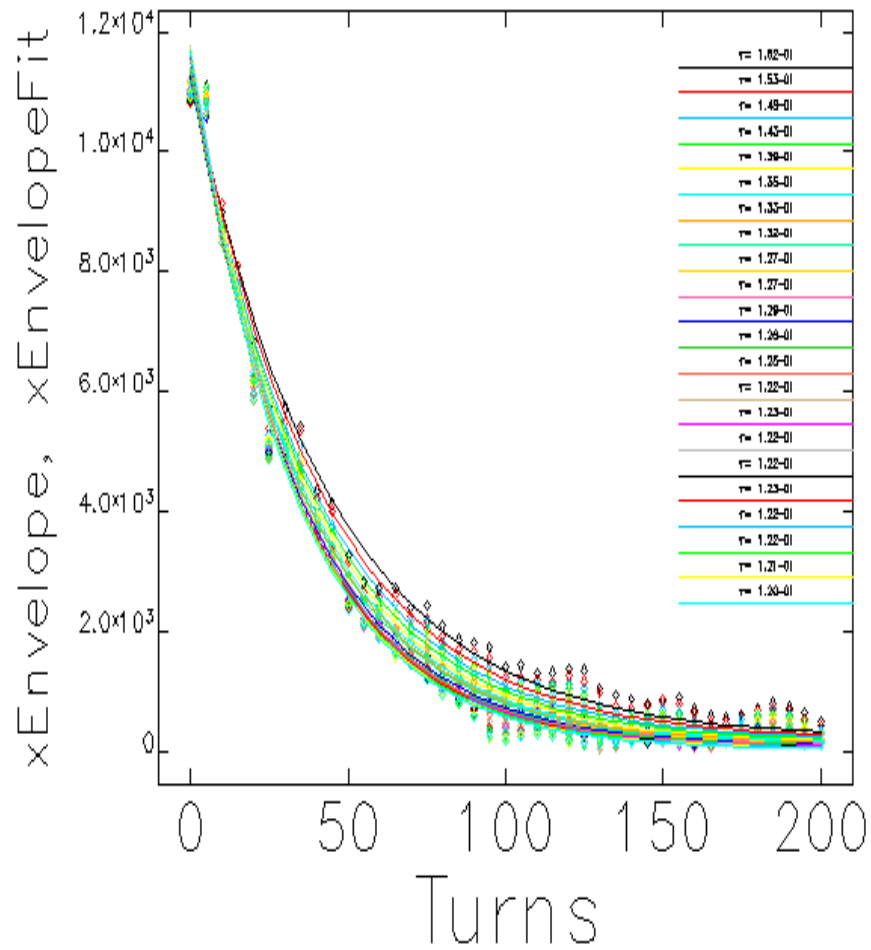
# Single-bunch accumulation limits

- Usable configuration for hybrids pattern
  - Chx=8.34
  - Chy=8.76
  - Accumulation limits > 20 mA
- Without feedback:
  - Chx =10
  - Chy =11
- Data taken before the vertical steering effect was discovered and corrected<sup>1</sup>.

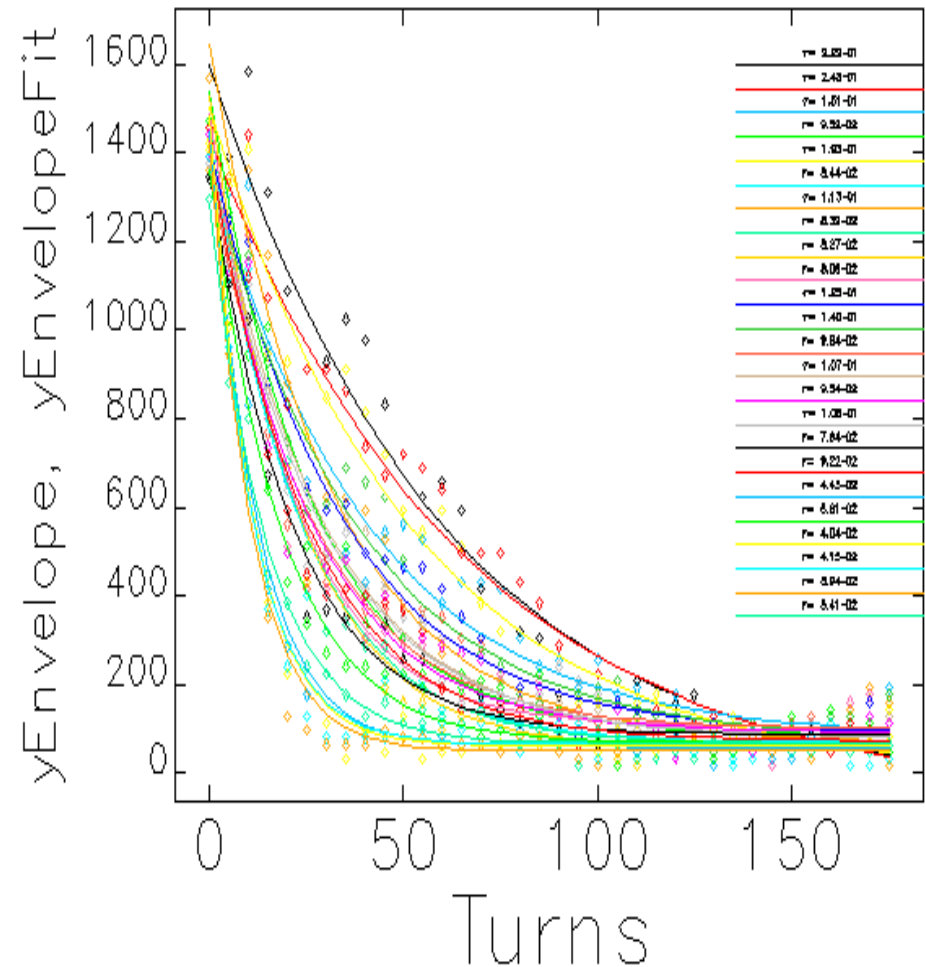


<sup>1</sup> Vadim Sajaev and Louis Emery

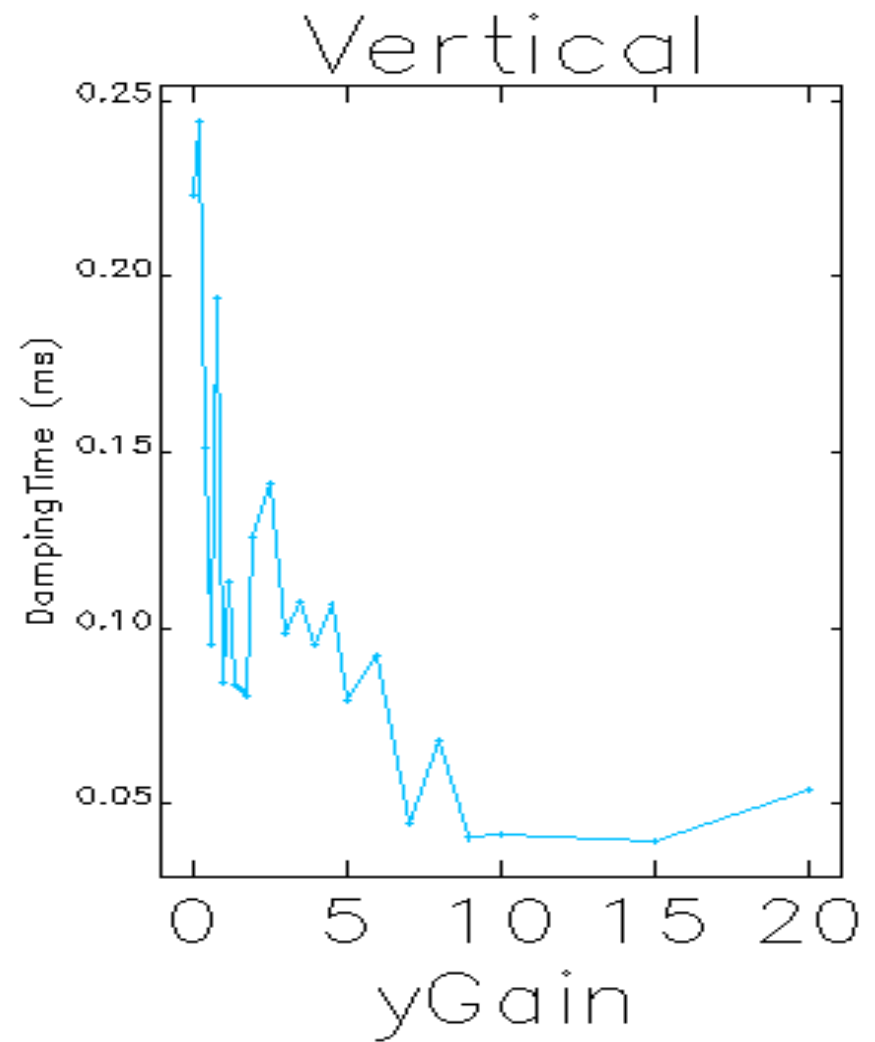
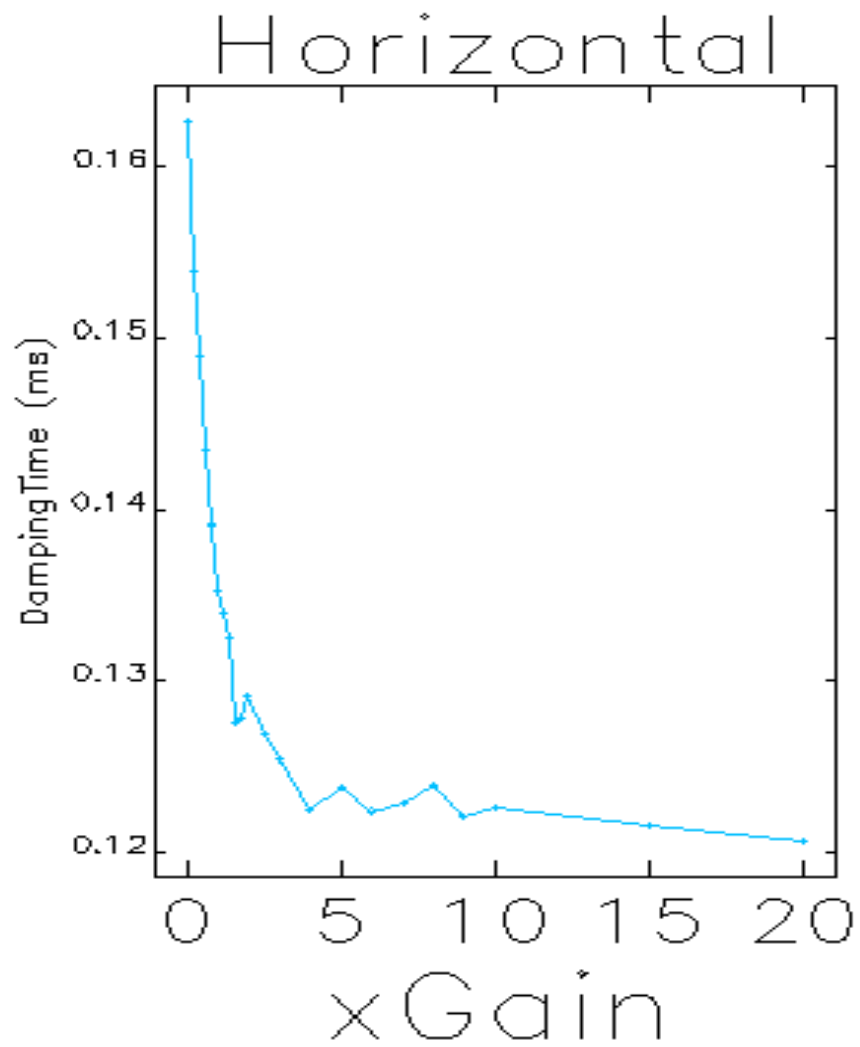
# Damping measurement with kicking method



**Horizontal plane**

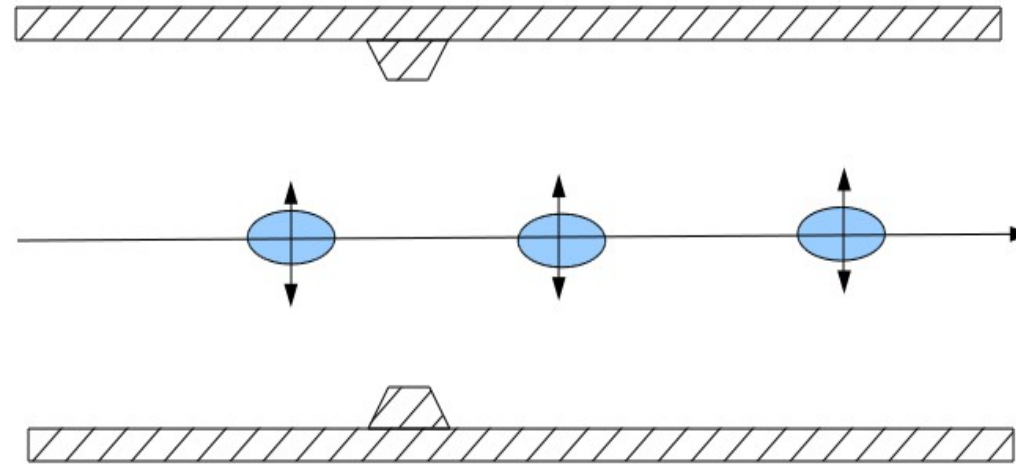


**Vertical plane**



# A simple physics model of transverse feedback system

- Bunches move along the vacuum chamber. They also go through betatron oscillations.
- Bunch interacts with vacuum chamber impedance and produce both longitudinal and transverse fields.
- These field interacts with the bunches and causes feedback to bunches and instability.
- A feedback system detects the beam motion and produces a damp term that is proportional to  $X'$ .



$$X'' + \omega_x^2 X + (G + D)X' = 0$$

# Mode-based and bunch-by-bunch feedback

- Beam instabilities can be separated in modes, characterized by its mode frequency and phase pattern.
- Mode-based feedback system detects oscillation of each mode and damps it with one frequency channel.
- It is also called frequency-domain method.
- It is impractical if there are too many unstable coupled bunch modes.
- Bunch-by-bunch feedback works in time domain.
- It detects oscillation of each bunch and damps each bunch with common feedback channel. Bunches are separated in time slots.
- The physics base is that if the motion of all bunches are damped individually all the modes will also be damped.



# Digital and analog feedback

- Analog feedback systems use stripline and BPM and RF filter, attenuator, delay line, and amplifiers to detect beam motion and process feedback output signal.
- Digital feedback systems first sample pickup signal into digital data and process data digitally, and then convert output data to analog waveform to drive beam.

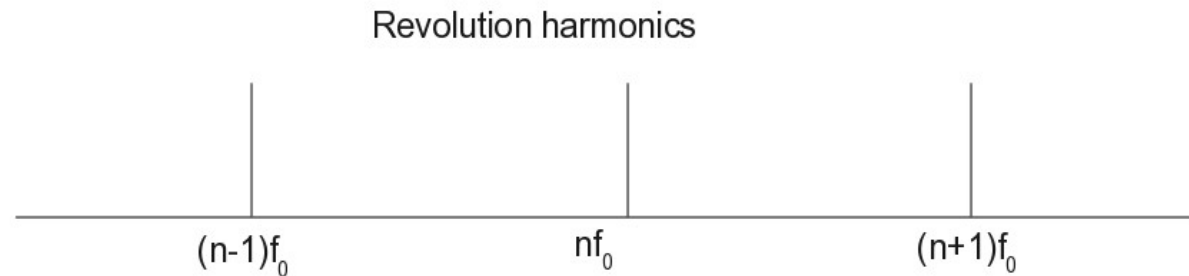


# Spectrum of bunched electron beam

Without transverse oscillation:

$$i(t) = i_0 \sum_{n=-\infty}^{+\infty} \delta(t - nT_0)$$

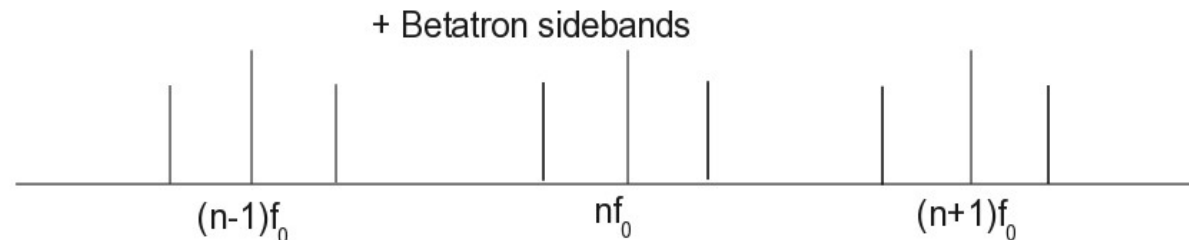
$$I(\omega) = I_0 \sum_{n=-\infty}^{+\infty} \delta(\omega - 2\pi n f_0)$$



With transverse oscillation:

$$i(t) = i_0 \sum_{n=-\infty}^{+\infty} \delta(t - nT_0) e^{-j\omega_x t}$$

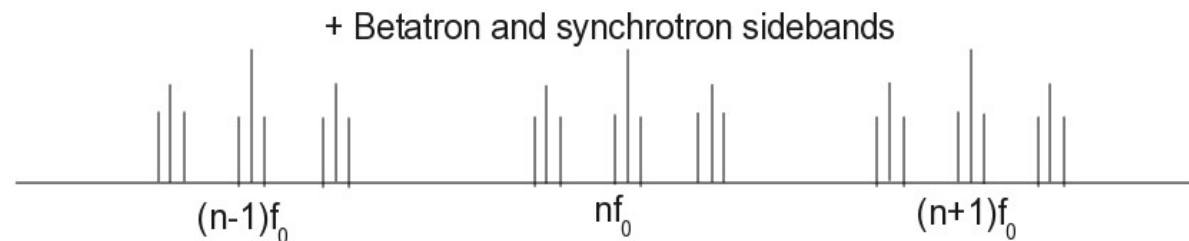
$$I(\omega) = I_0 \sum_{n=-\infty}^{+\infty} \delta(\omega - 2\pi n f_0 - \omega_x)$$



With longitudinal time oscillation:

$$i(t) = i_0 \sum_{n=-\infty}^{+\infty} \delta(t - nT_0 - \tau \cos(\omega_s t))$$

$$I(\omega) = I_0 \sum_{m=-\infty}^{+\infty} (-j)^k J_m(\omega \tau) \sum_{n=-\infty}^{+\infty} \delta(\omega + m\omega_s - 2\pi n f_0)$$





# FIR generation

- The FIR filters are at the core of a feedback system.
- There are two basic methods in FIR generation:
- Frequency domain method:
  - specify desired frequency character.
  - derive the filter coefficients with DFT.
- Time domain least square fitting (TDLSF) method<sup>1</sup>:
  - Specify time domain character.
  - Derive filter coefficients by least square fitting.
- We implemented the TDLSF method.

<sup>1</sup> T. Nakamura

$$\begin{bmatrix} x_{n-k} \\ x'_{n-k} \end{bmatrix} = M^{-k} \begin{bmatrix} x_n \\ x'_n \end{bmatrix}$$

$$M^{-k} = \begin{bmatrix} \cos(2\pi\nu k) + \alpha \sin(2\pi\nu k) & \beta \sin(2\pi\nu k) \\ -\gamma \sin(2\pi\nu k) & \cos(2\pi\nu k) - \alpha \sin(2\pi\nu k) \end{bmatrix}$$

$$\chi^2 = \sum_{k=0}^{k=M-1} [x(n-k) - C_k x_n - \alpha S_k x_n - \beta S_k x'_n]^2$$

$$C_k = \cos(2\pi\nu k)$$

$$S_k = \sin(2\pi\nu k)$$

$$x'_n = \sum_{k=0}^{k=M-1} A_k x(n-k)$$

$$x_n = \sum_{k=0}^{k=M-1} B_k x(n-k)$$

# Ideal phase response

Two sampled sequences:

$x(n)$  beam position at pick-up

$x'(n)$  beamslope at kicker

The phase difference between the two sequences can be expressed analytically as:

$$\Delta \theta = \frac{\pi}{2} + \tan^{-1} \alpha_k + \Delta \psi$$

$\alpha_k$  - alpha function at kicker

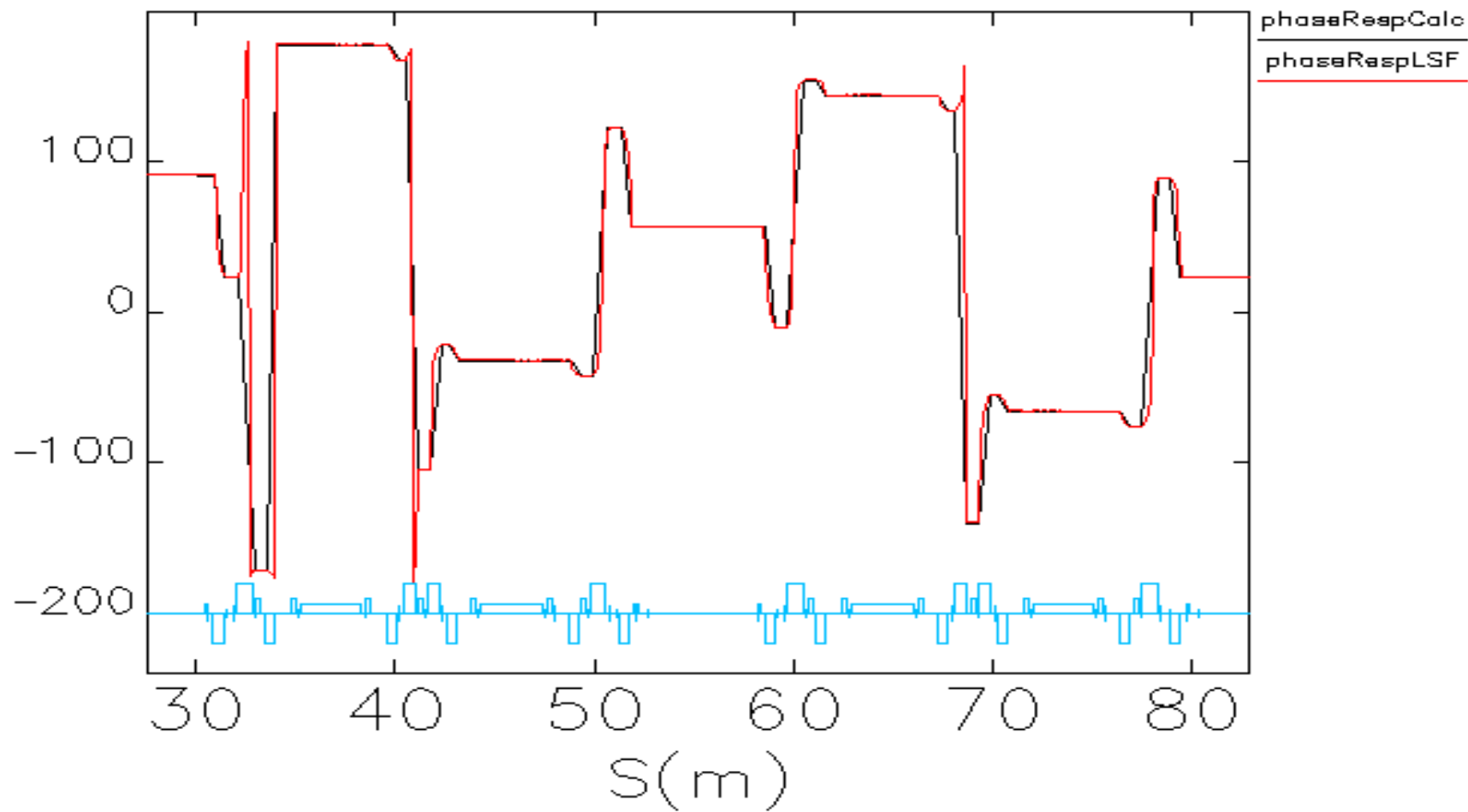
$\Psi$  - betatron phase difference between kicker and pick-up

A simplest case:  $\alpha_k=0$  and  $\Delta\psi=0$ :

$$\Delta \theta = \frac{\pi}{2}$$

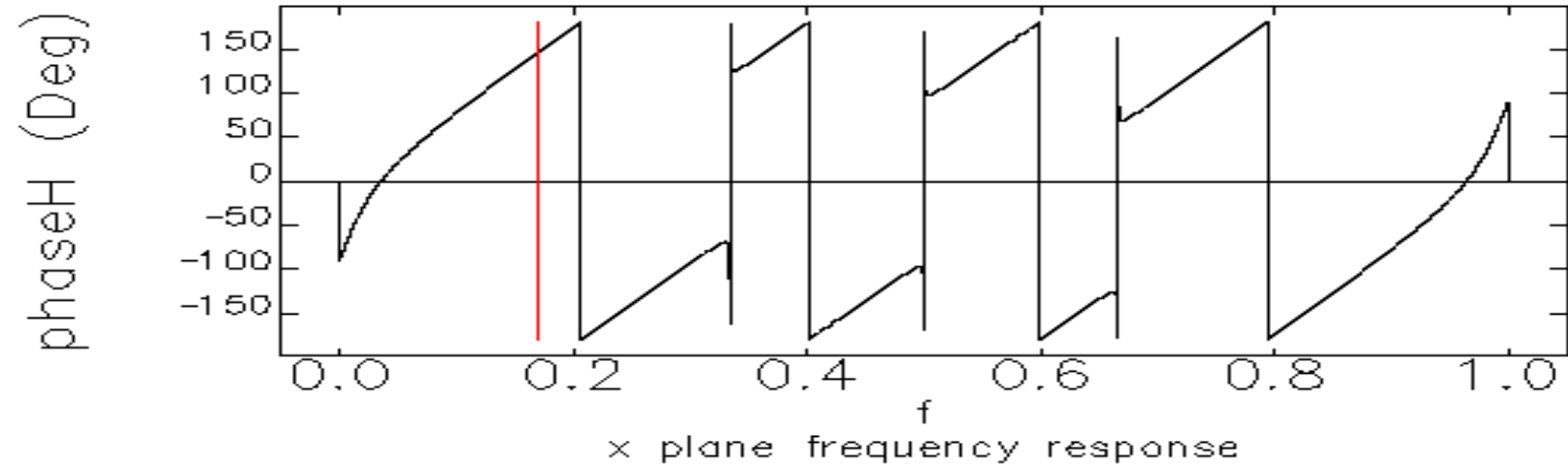
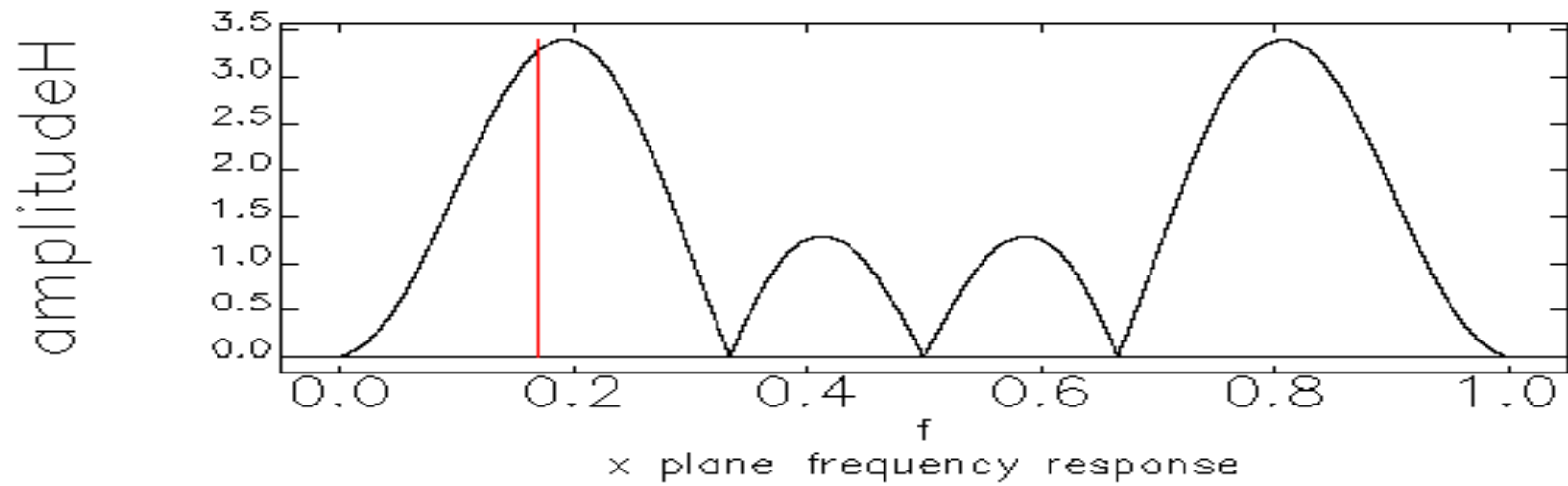
It is verified numerically that when turns number is larger than 3 the filter generated with TDLSF produces an exact phase response.

This validates that TDLSF method and frequency domain method are equivalent.



Twiss parameters—input /home/helioa/daqData/er/calibratedModels/twisa.ale lattice: apa.lta

**Ideal phase response (black) calculated from APS model lattice parameters and phase response of a 6-tap filter generated with TDLSF method (red).**



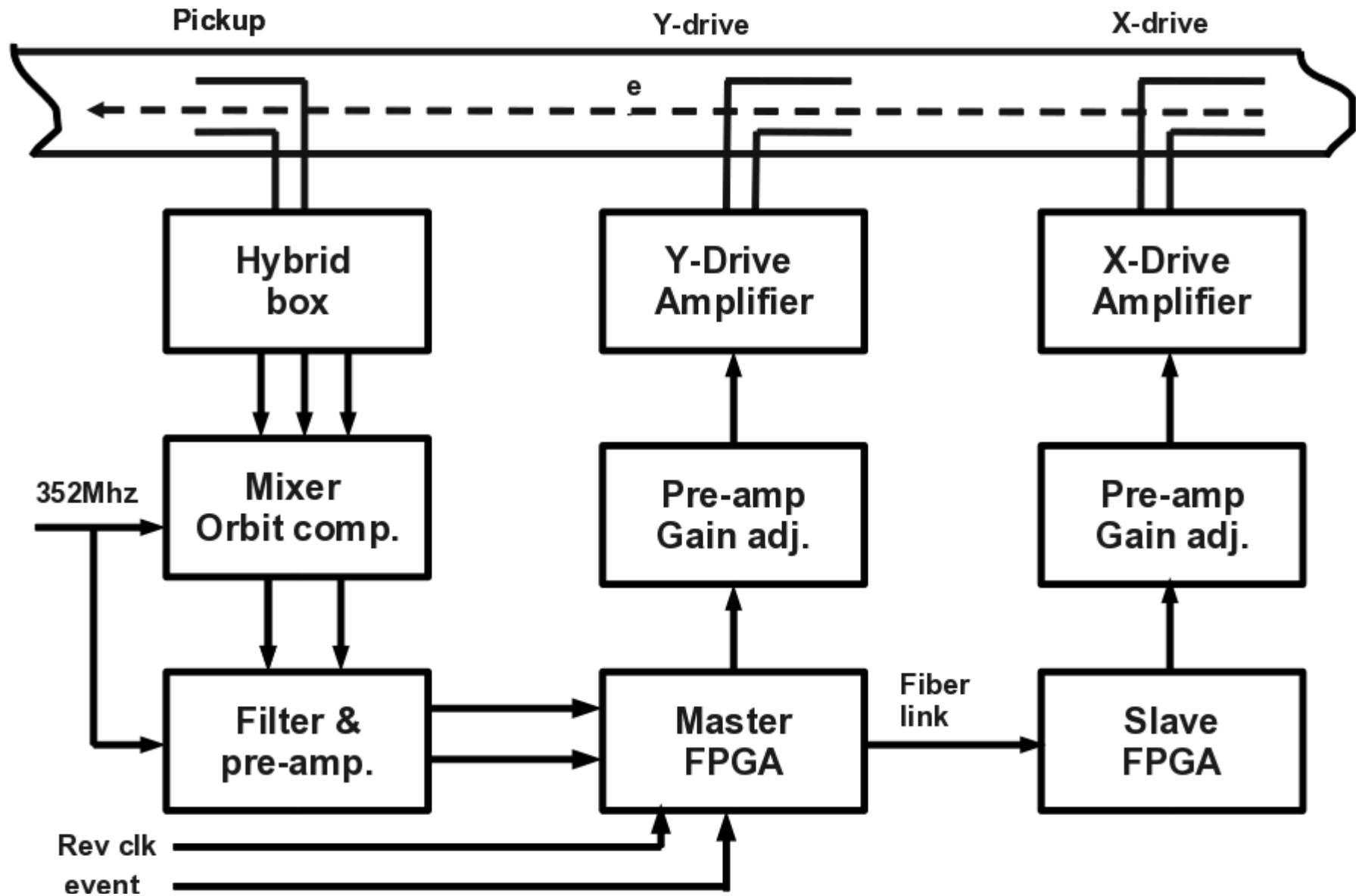
Frequency response 6-tap filter

# Advantages and limitations of TDLSF

- Advantages:
  - Directly generates FIR from lattice file.
  - Close to ideal phase response.
  - Applies to locations where  $\alpha$  is non-zero for pick-up and driver.
- Limitations:
  - The linear matrix does not include damping effect of the feedback. It is only applicable if the effect is relatively weak.
  - The method applies linear lattice model to centroid motion, which does not include tune shift produced by impedance or non linearity of lattice.



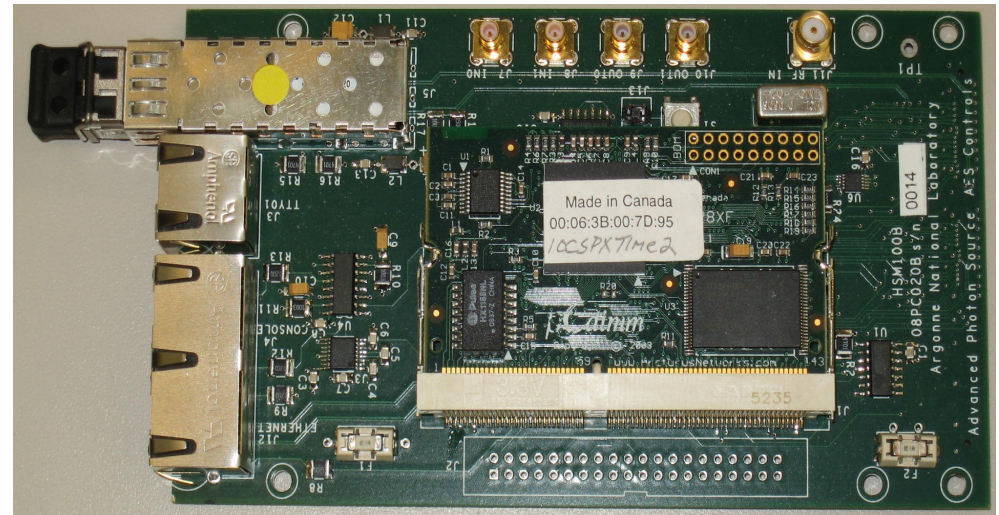
# System Diagram



# FPGA hardware config.

- Altera stratixII-GX DSP development kit
- PCI Express Fast Lane for digital communication between the master and slave processors.
- SLS HSMC data conversion card:
  - 2x 14-bit A/D, max. sample rate 150 MSPS
  - 2x 14-bit DAC max. sample rate 250 MSPS
- Coldfire card as EPICS processor
- Home made HSMC daughter card for:
  - Clock/timing input
  - Fibre interface for event inputs
  - Ethernet connection
- An upgraded spare is under development:
  - StratixIV-GX DSP kit.
  - PCIE fiber interface for up to 8 GBS digital synchronous communication.
  - A home design data conversion board with 2x 14-bit and 2x 14-bit DAC with sample rate 400 MSPS.





# Firmware features

- Up to 32-tap FIR filters.
- Filter coefficients are loaded on the fly.
- 2 channel waveforms for input data.
- 2 channel output data.
- Programmable output control pattern for output manipulation and diagnostics.
- Adjustable DAC delay in steps of clocks.
- Integrated Event Timing for synchronization to external event such as top-up injection.
- Built-in EPICS interface .

## Sample control

+D	Normal
-D	Negate
CL	Copy last
NL	Negate last
Z	Zero
+V	Fixed positive
-V	Fixed negative

# Drive system

- Amplifier:
  - 4 x 150-W, 10 Khz to 220 Mhz for vertical drive (diagonal 4 blades).
  - 2 x 500-W, 10 Khz to 250 Mhz for horizontal drive.
- Striplines:
  - Sector 4 for vertical drive:
    - Four-blade geometry.
    - Length: 16.7 cm
    - Measured kick: 0.26  $\mu$ Rad
  - Sector 35 horizontal drive:
    - Two blades geometry.
    - Length: 34 cm
    - Measured kick: 0.78  $\mu$ Rad

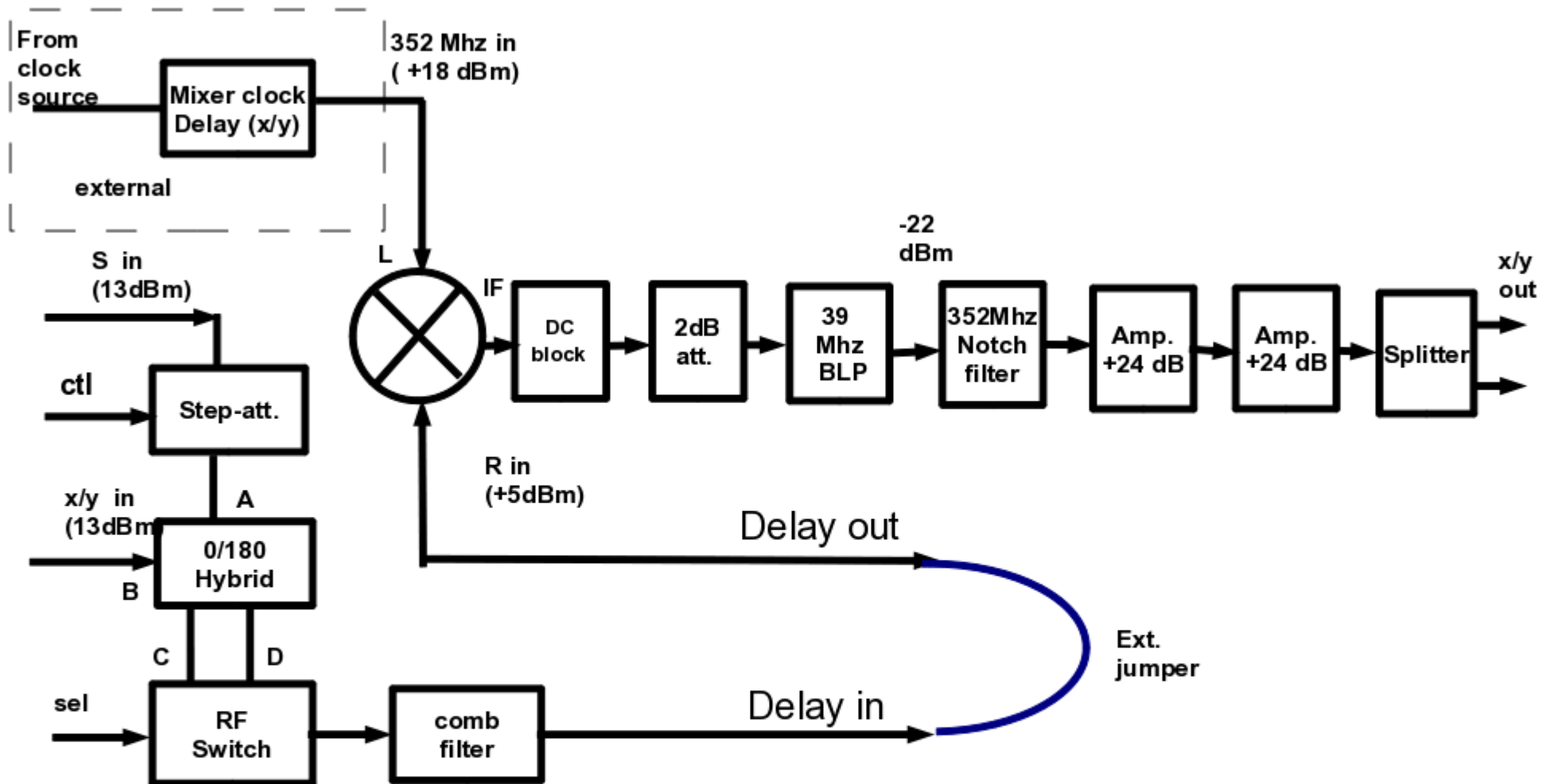


# Front-end electronics

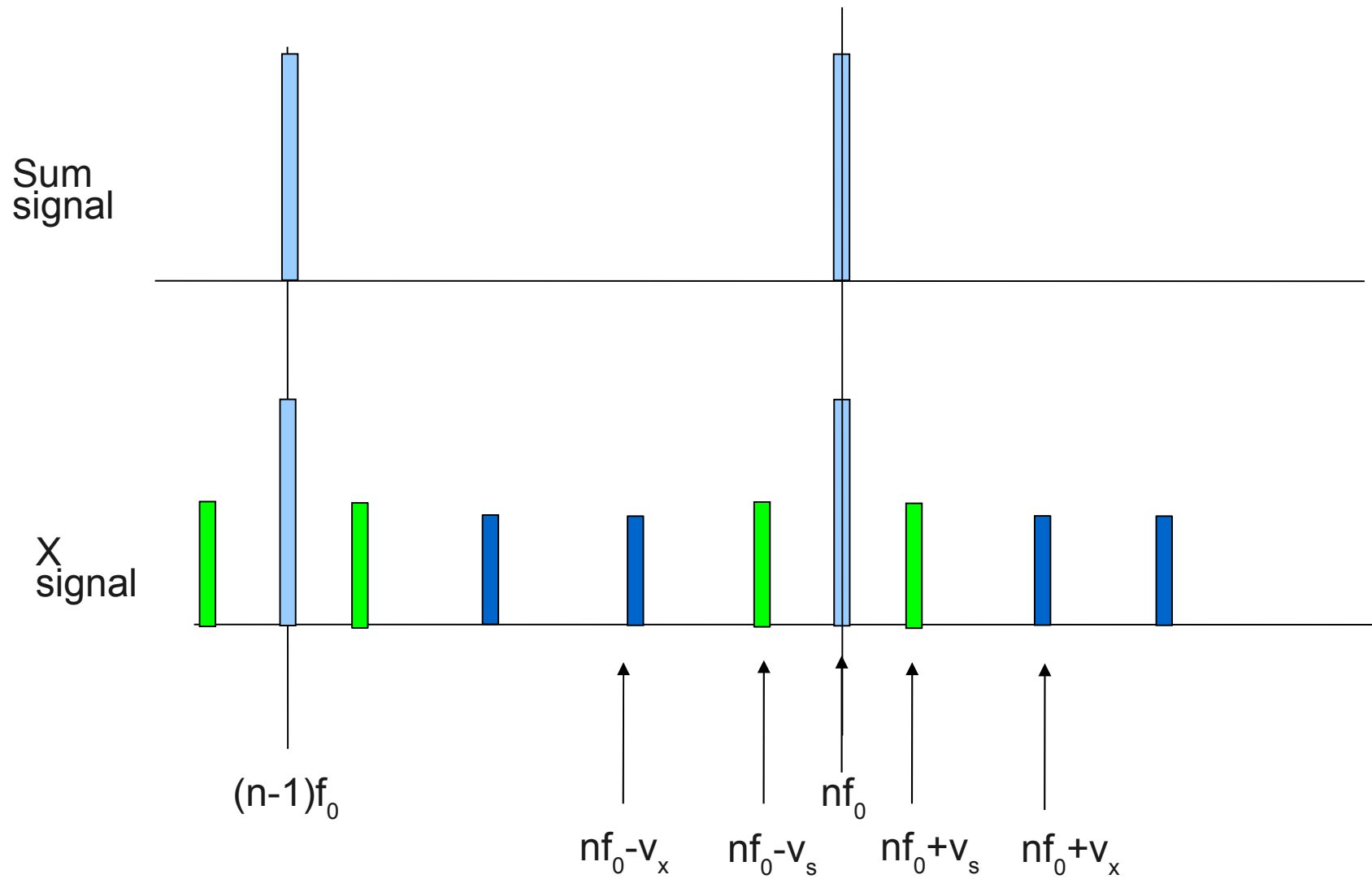
- Mixer/filter down converter.
- High level mixer (ZFY-2, 23 dB, 0.1 to 1000 MHz).
- 352 MHz LO input.
- Programmable delay for timing adjustment of LO input relative to beam signal
- Orbit component compensation circuit.
- Comb filter on stripline input signal.
- Bessel type LP filter on IF output.
- Low noise amplifiers.



# Mixer /filter configuration



# Spectrum of stripline signals

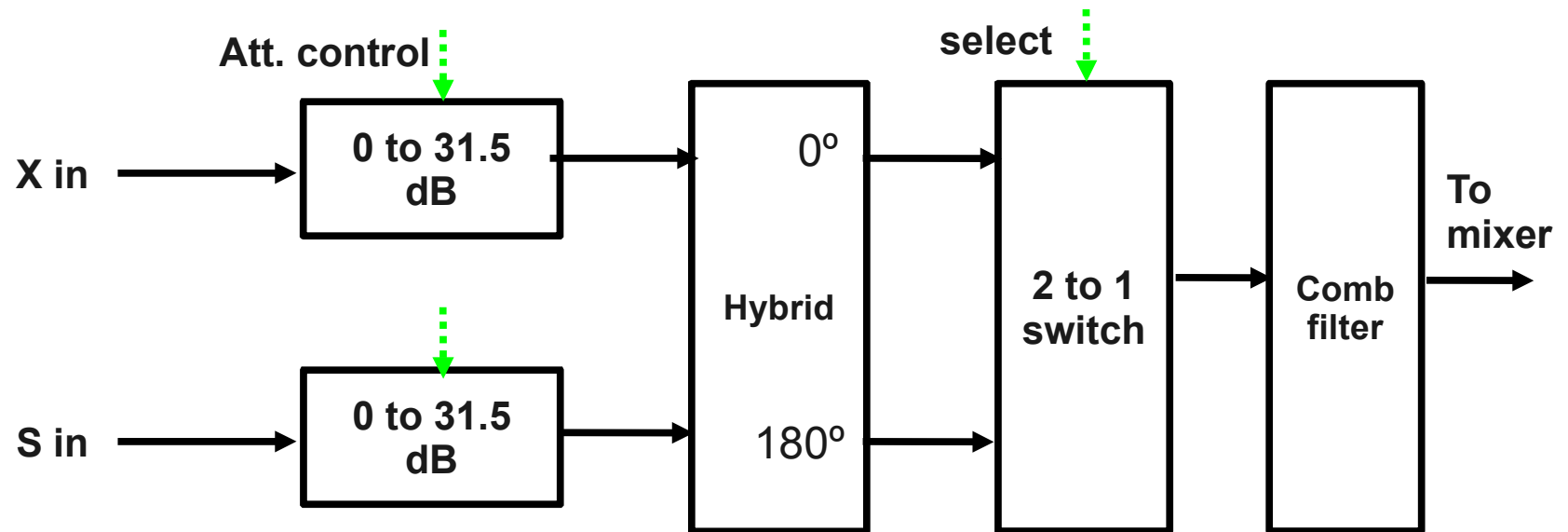


# Orbit component compensation with sum signal

- Orbit offset and gain asymmetry produce revolution harmonics in the x/y signal.
- The component is sampled into a DC value.
- It is filtered out by The feedback FIR filter.
- However if the offset is large it can saturate the input ADC and lose useful spectrum.
- Two approaches:
  - Notch filter with a one-turn delay.
  - Gain adjustment of individual blades.
- Our approach is equivalent to the latter.
- Low cost and works for light source because the DC orbit is well controlled and does not change during run period.



# Orbit component compensation circuit



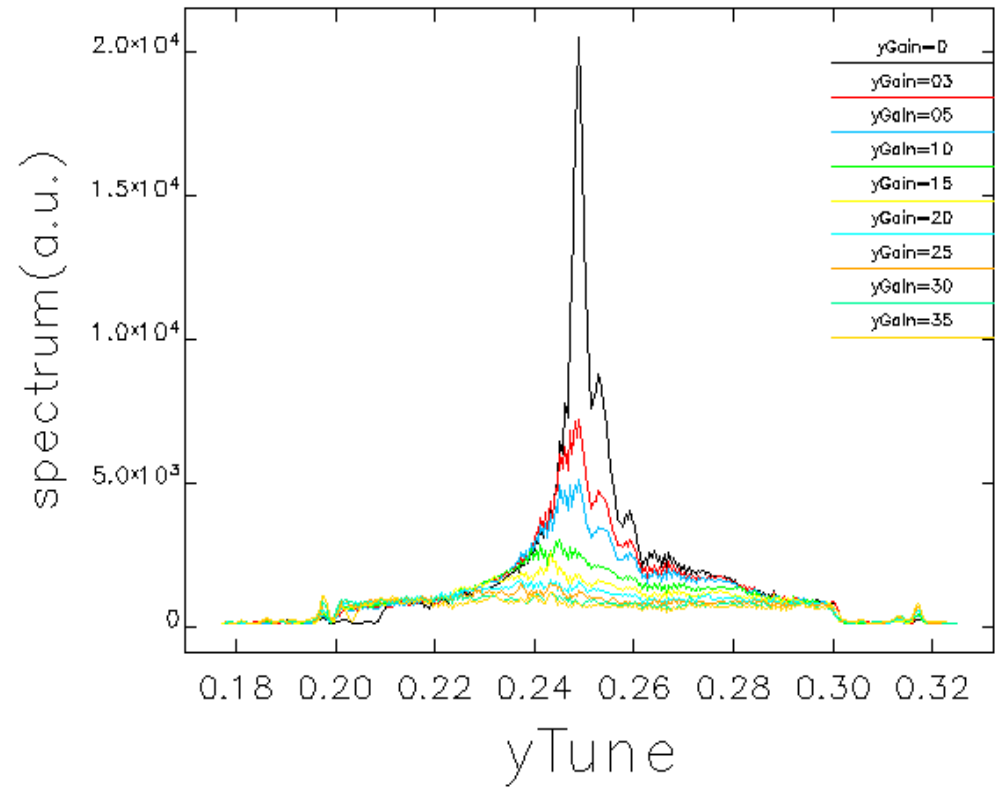
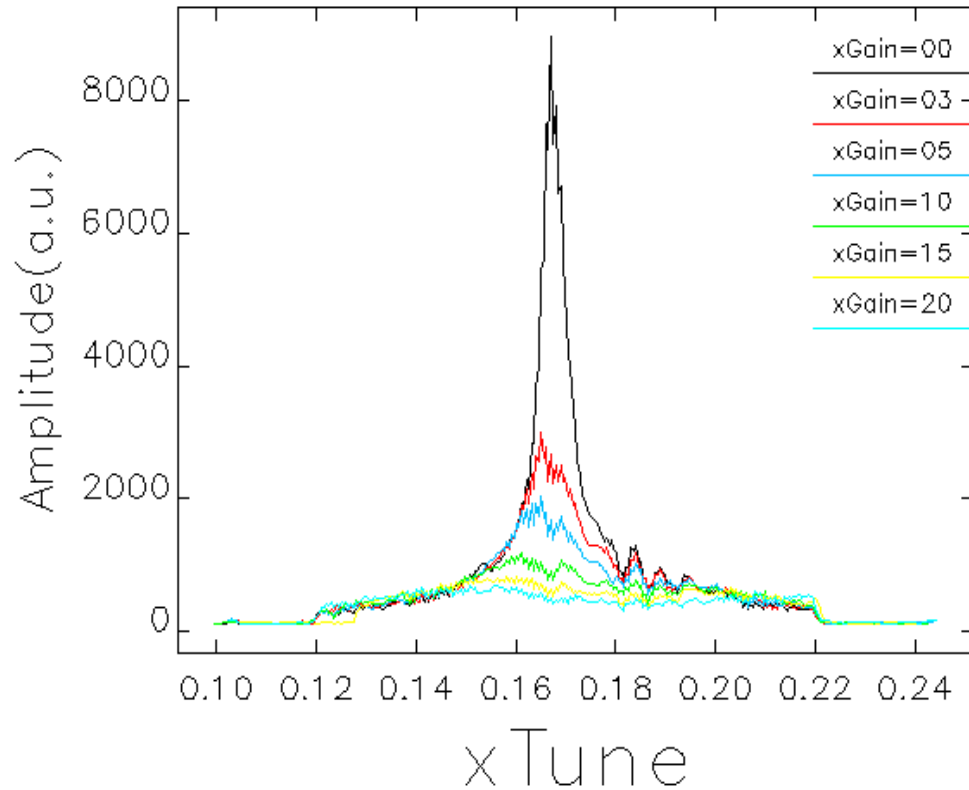


# Independent bunch-by-bunch tune measurement system

- Separate processor: Altera Stratix-II DSP kit.
- Shared front-end and clock source.
- Recorders for raw ADC sample waveforms.
- Turn-by-turn waveforms.
- FFT waterfall waveforms.
- Event receiver interface that allows synchronization of the tune acquisition with many events such injection, booster extraction, top-up injection, etc.
- For feedback system diagnostics and front-end tuning.
- Can be used for tune measurement and other studies, such as fast ion and e-cloud, etc.



# Check damping effect with tune-gain scan

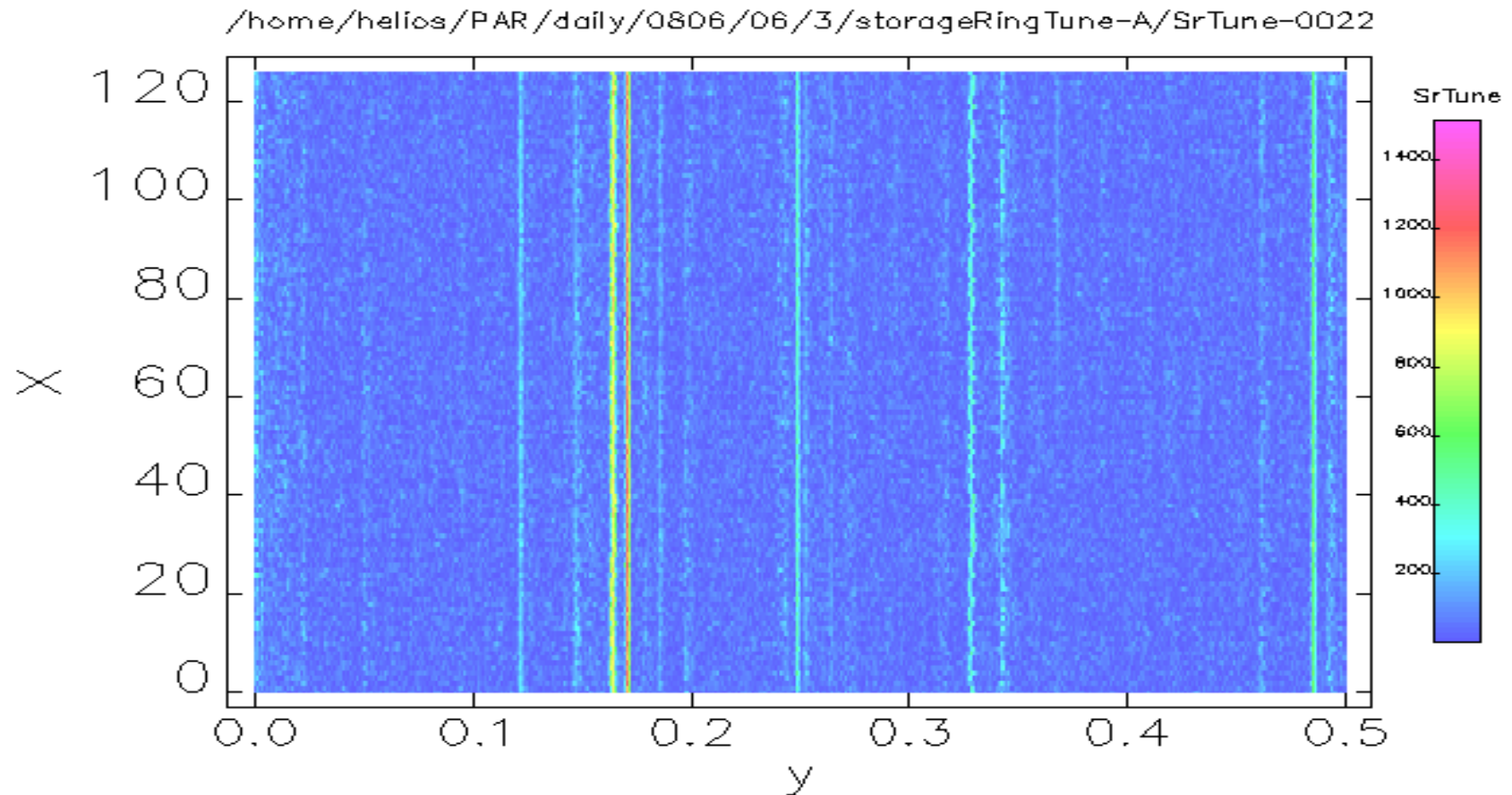


# Noise analysis and reduction

- Noise signal contributes to the close-loop beam emittance. Reducing noises is essential.
- Noise analysis was performed using both an Agilent MXA signal analyzer and the FPGA-based tune measurement system.
- Identified most of the sidebands:
  - 40 Khz sidebands from faster correctors switching supplies.
  - 20KHz noise sidebands from the quads and sextupoles supplies. Could be directly coupled electronically.
  - Jitter in the sample clock, P0 and mixer LO clock source.
  - Noises generated in the FPGA electronics.
  - Many sidebands are aliased into multiple sidebands and hard to trace original source.
  - PS group has implemented filtering circuits to all fast corrector power supplies, which reduced noise spectrum by 20 dB.

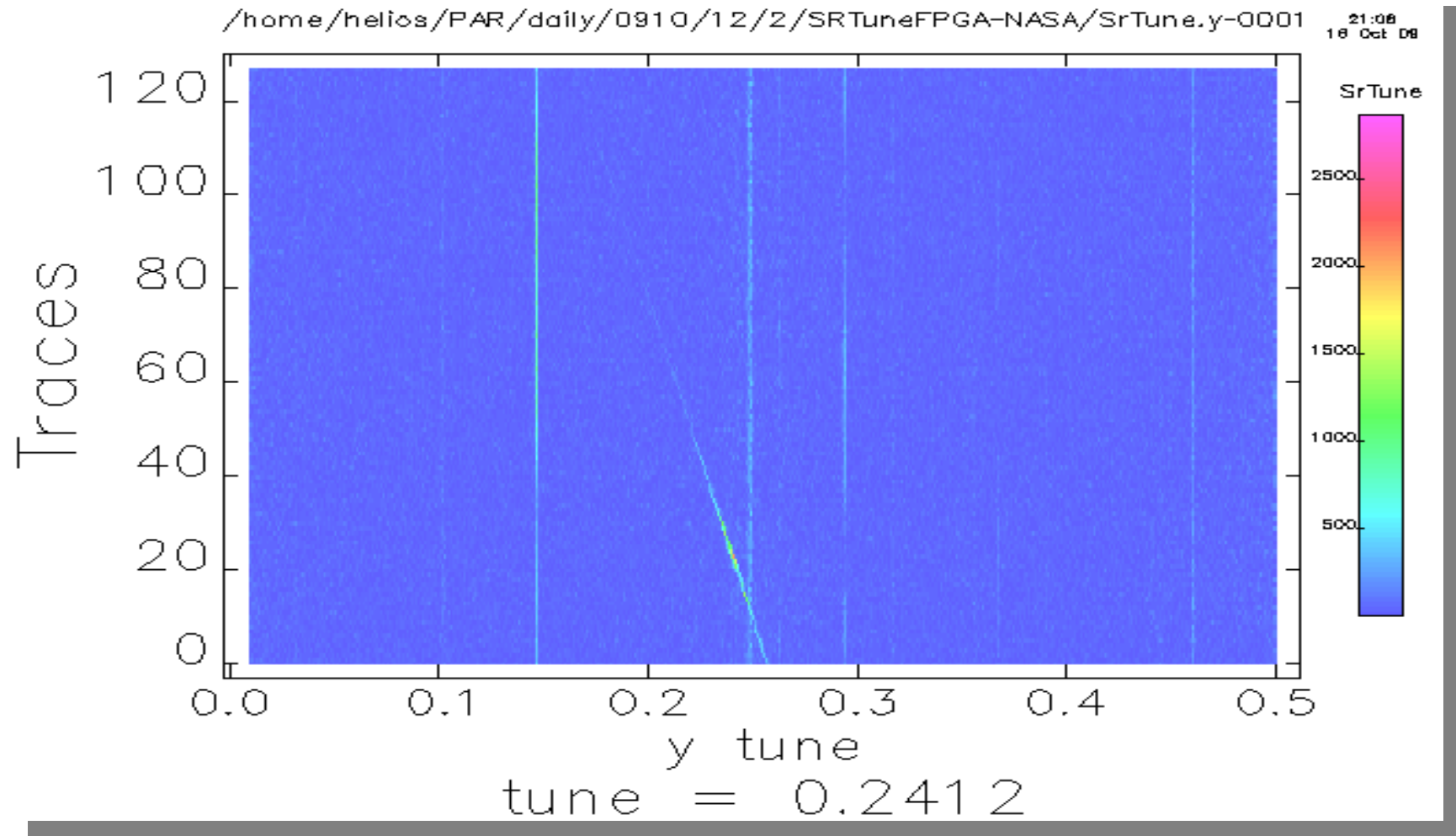


# Beam spectrum taken earlier

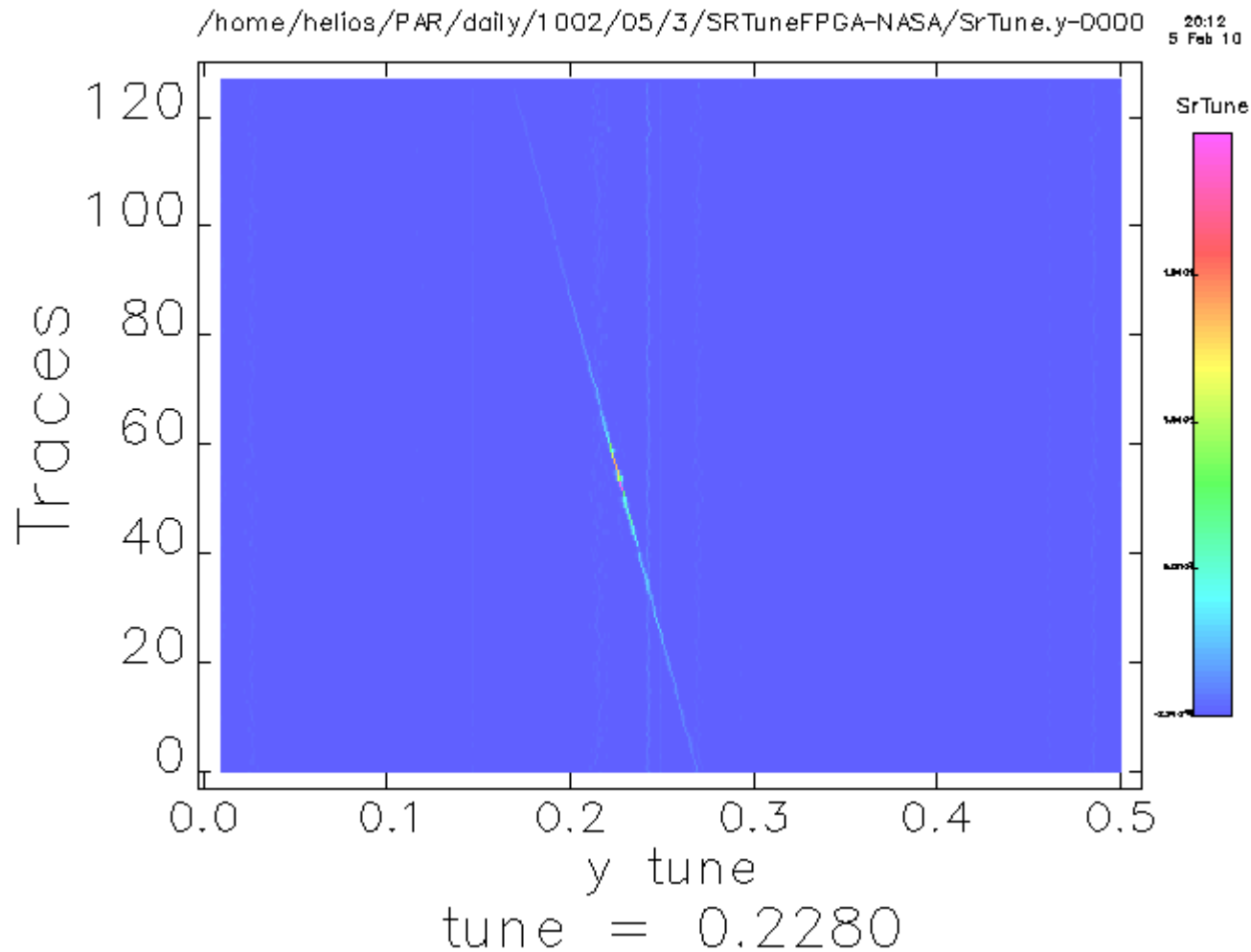


SrTune as a function of  $y$  and  $x$

# Vertical tune spectrum before corrector upgrade

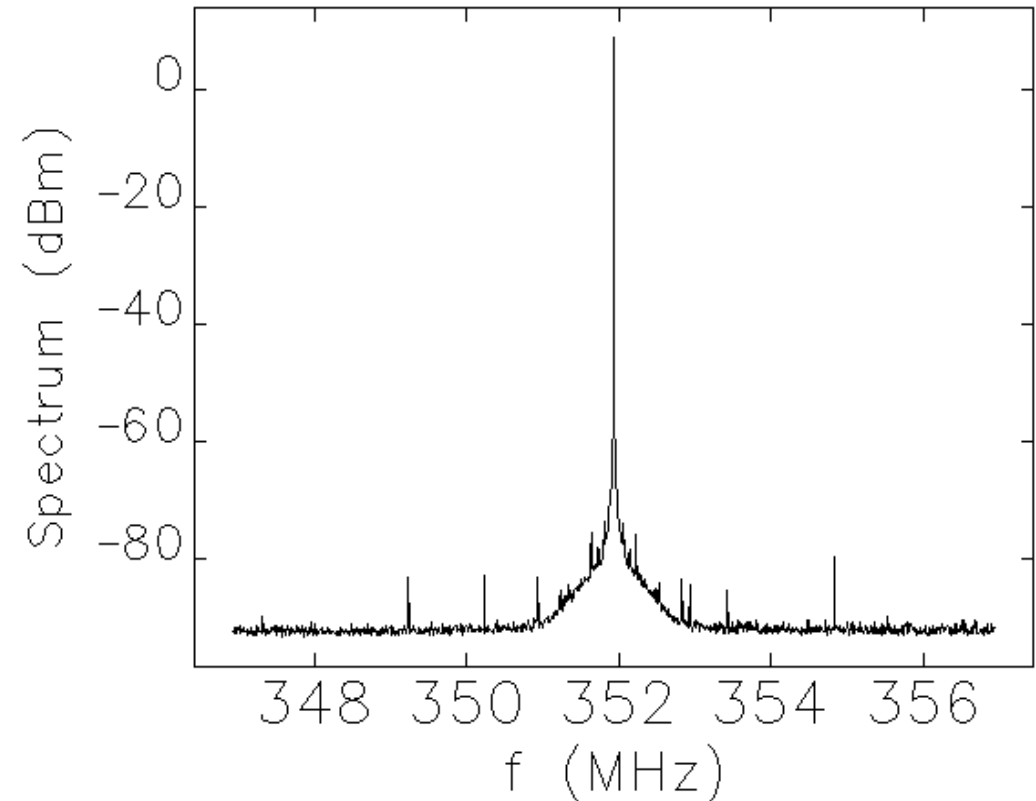


# Vertical tune spectrum taken recently.



# Clock source improvement

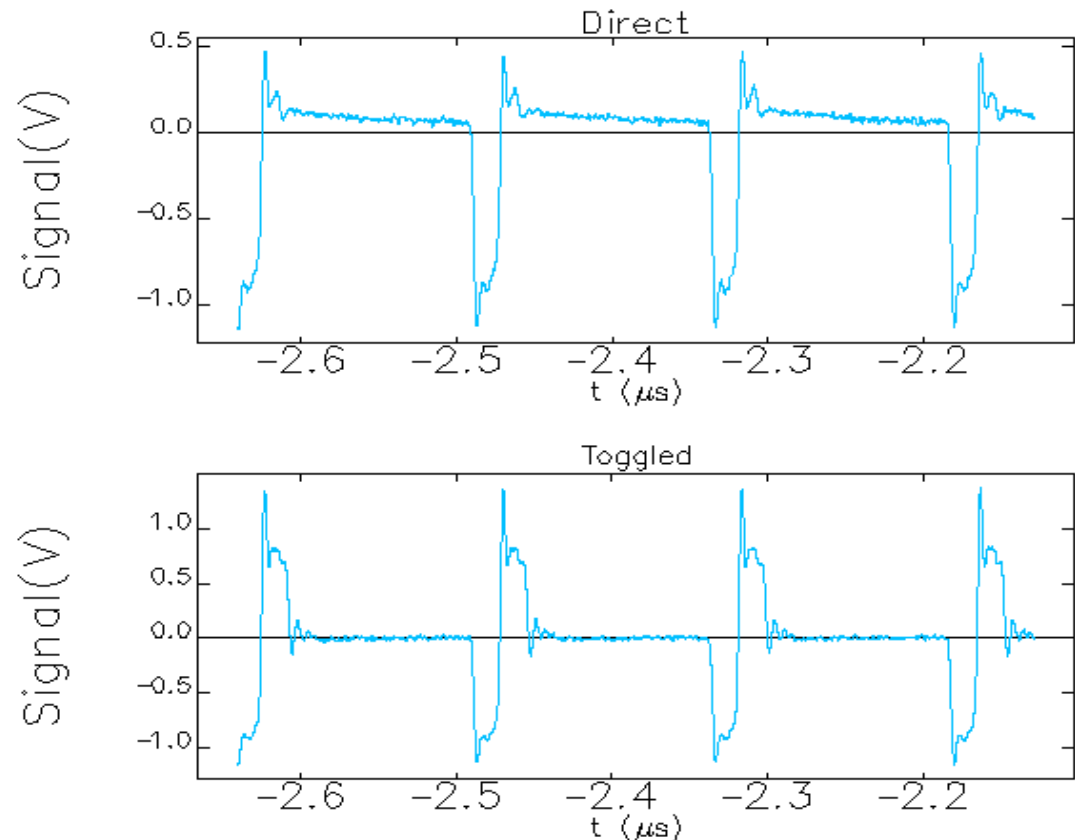
- Clock source cleanness directly impacts system performance and noise level.
- Compared two alternatives:
  - a 352 MHz source transmitted by optic fibre from timing system
  - a source directly from RF system by coax cable
- The direct RF source is currently used.
- A 352-MHz CF and 1 MHz BW BP filter was added to remove a 1 MHz side-band in the source signal.
- An upgrade clock and P0 cleaner circuit is being developed, which will substantially reduce jitters<sup>1</sup>.



<sup>1</sup>Tony Scaminaci

# AC coupling effect of the DAC out and drive circuits

- The FPGA DAC output is transformer-coupled.
- There is baseline shift when the data rate is low.
- We added a toggle option in the DAC output processing to eliminate DC level drift.
- Useful for single bunch or 24 bunch fill pattern.
- Does not work if all the buckets are sampled and processed.





# High level control application

A GUI application is developed for system control:

- Directly reads parameters from a lattice file
- Loads and saves filter files.
- Plot frequency response.
- Also provide bunch pattern, gain and other controls functions.

# High level control application

P0FeedbackControl

File Help

```
update control waveform bits...
done.
Load twiss parameters ...
done.
```

Print Save As... Email... Expand Dialog...

InputProcess \ OutputMode \ Set Pattern & Control \ FIR-X \ FIR-Y \

Twiss Parameters

Twiss file: /home/helios/PAR/feedback/generateFIR/aps\_nux

pickup location(m):	<input type="text" value="7.113932e+01"/>
kicker location(m):	<input type="text" value="9.6535e+02"/>
Betax pickup(m)	<input type="text" value="6.2878076943374"/>
Betax kicker(m)	<input type="text" value="20.231507973948"/>
alphax pickup	<input type="text" value="2.1694582115826"/>
alphax kicker	<input type="text" value="0.0305737679665"/>
psix pickup(rad)	<input type="text" value="14.412674597818"/>
psix kicker(rad)	<input type="text" value="198.77480652241"/>
x tune:	<input type="text" value="3.6168856588211"/>
target nux:(.08-.4)	<input type="text" value="0.0"/>
Order-x (3-32):	<input type="text" value="3"/>
Delay-x(0-10):	<input type="text" value="0"/>

X plane FIR filter

Selected X Coord:

Selected Y Coord:

P0FeedbackControl

File Help

update control waveform bits...  
done.

Print Save As... Email... Expand Dialog...

InputProcess \ OutputMode \ Set Pattern & Control \ FIR-X \ FIR-Y \

Make Patterns

PatternSelection \ Samples \

	Output Mode	Input Processing
1	<input type="checkbox"/> ZD <input type="checkbox"/> +D <input checked="" type="checkbox"/> -D <input type="checkbox"/> -V <input type="checkbox"/> +V <input type="checkbox"/> NL <input type="checkbox"/> CL	<input checked="" type="checkbox"/> Enable <input type="checkbox"/> Disable
2	<input type="checkbox"/> ZD <input type="checkbox"/> +D <input type="checkbox"/> -D <input type="checkbox"/> -V <input type="checkbox"/> +V <input type="checkbox"/> NL <input checked="" type="checkbox"/> CL	<input type="checkbox"/> Enable <input checked="" type="checkbox"/> Disable
3	<input type="checkbox"/> ZD <input type="checkbox"/> +D <input type="checkbox"/> -D <input type="checkbox"/> -V <input type="checkbox"/> +V <input checked="" type="checkbox"/> NL <input type="checkbox"/> CL	<input type="checkbox"/> Enable <input checked="" type="checkbox"/> Disable
4	<input type="checkbox"/> ZD <input type="checkbox"/> +D <input type="checkbox"/> -D <input type="checkbox"/> -V <input type="checkbox"/> +V <input type="checkbox"/> NL <input checked="" type="checkbox"/> CL	<input type="checkbox"/> Enable <input checked="" type="checkbox"/> Disable
5	<input checked="" type="checkbox"/> ZD <input type="checkbox"/> +D <input type="checkbox"/> -D <input type="checkbox"/> -V <input type="checkbox"/> +V <input type="checkbox"/> NL <input type="checkbox"/> CL	<input type="checkbox"/> Enable <input checked="" type="checkbox"/> Disable
6	<input checked="" type="checkbox"/> ZD <input type="checkbox"/> +D <input type="checkbox"/> -D <input type="checkbox"/> -V <input type="checkbox"/> +V <input type="checkbox"/> NL <input type="checkbox"/> CL	<input type="checkbox"/> Enable <input checked="" type="checkbox"/> Disable

UpdatePattern PlotBunchPattern

Launch medm screen Launch vnc screen

Set DAC and gains

DacDelay-x (clock): 98

DacDelay-y (clock): 352

Set Dac Delays

X gain(0-127): 1.0

Y gain(0-127): 1.0

Set Gains

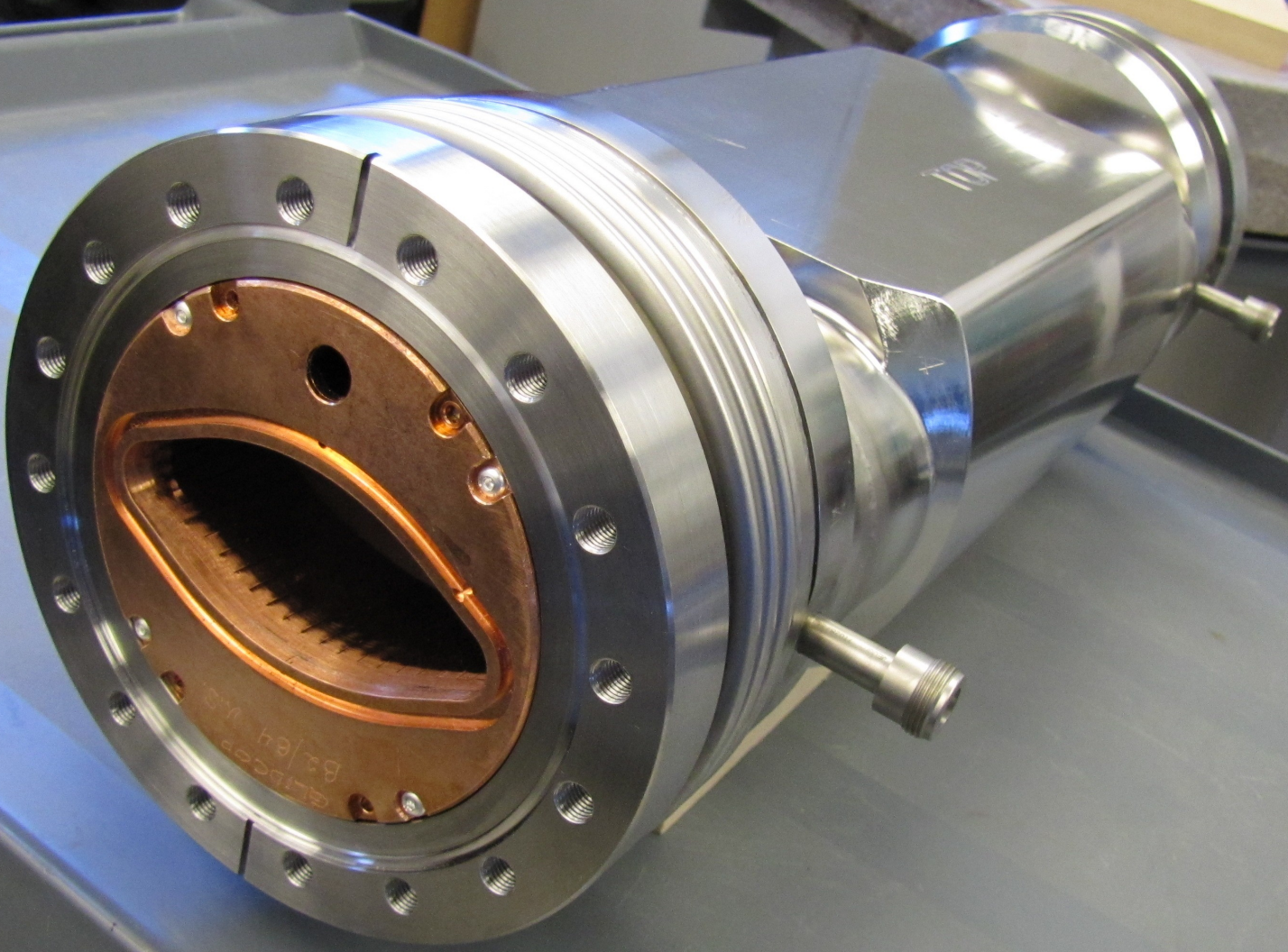
X DacV(0-0.999): 0

Y DacV(0-0.999): 0

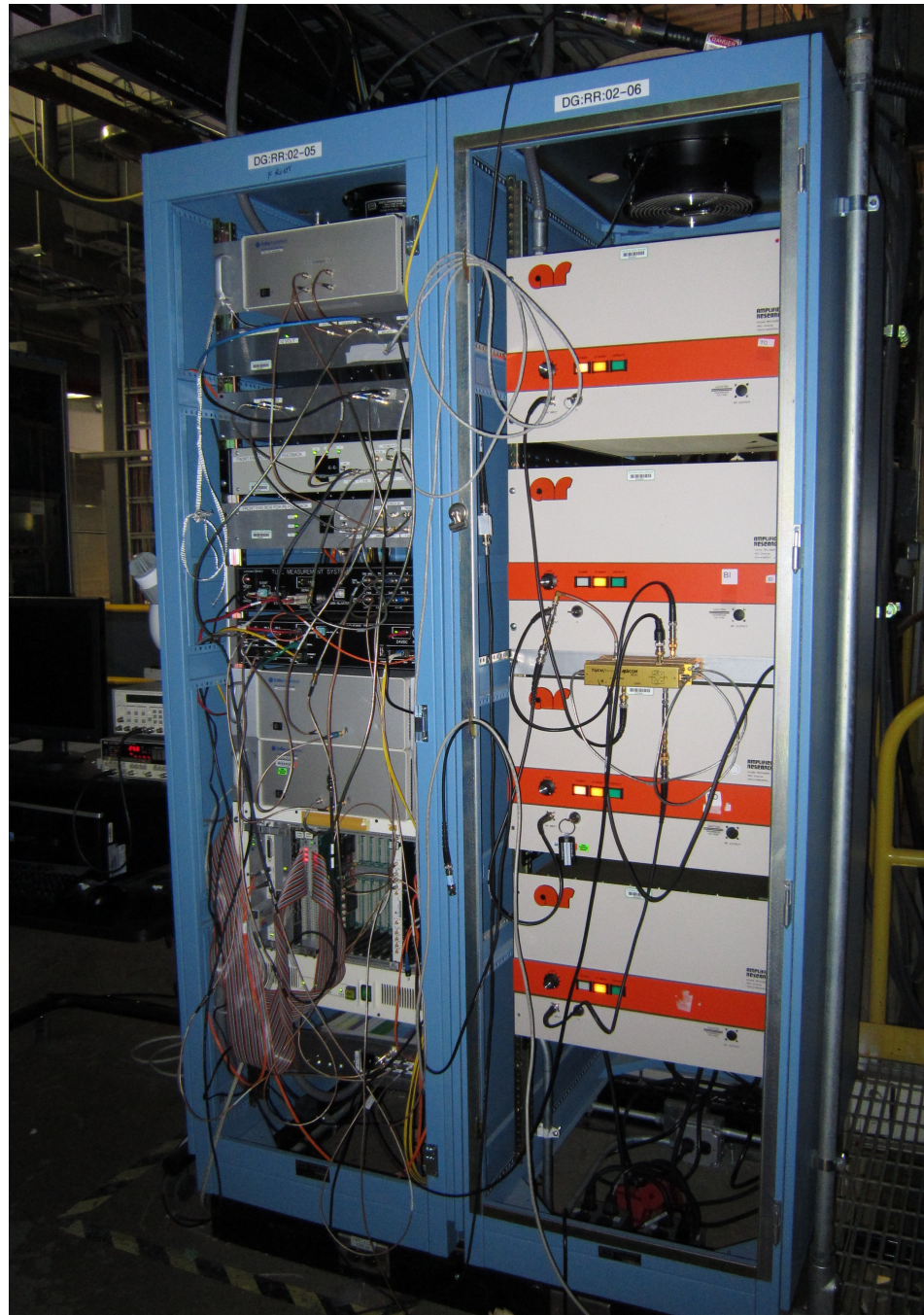
Set Dac Hi/Lo

LoadPatternFile WritePatternFile ReadPattern SetPattern

This lock... only be removed by:  
NAME: \_\_\_\_\_  
RANK: \_\_\_\_\_  
PRINTED NAME: \_\_\_\_\_  
DATE APPLIED: \_\_\_\_\_  
EXPECTED COMPLETION DATE: \_\_\_\_\_



04/26/2010



The Advanced Photon Source is an Office of Science User Facility operated for the U.S. Department of Energy Office of Science by Argonne National Laboratory



# Further upgrade plan

- Further reduce system noise level.
- Explore adaptive filter that deal with tune shift issue.
- Gain control for different bunch charge.
- Increase system bandwidth to full 352 MHz.
- Apply the system to APS upgrade.

# References

- T. Nakamura, private communications.
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- C.-Y. Yao, et al. “An FPGA-based bunch-to-bunch feedback system at the Advanced Photon Source,” PAC07.
- T. Nakamura, “Single-loop two-dimensional transverse feedback for Photon Factory,” EPAC06.