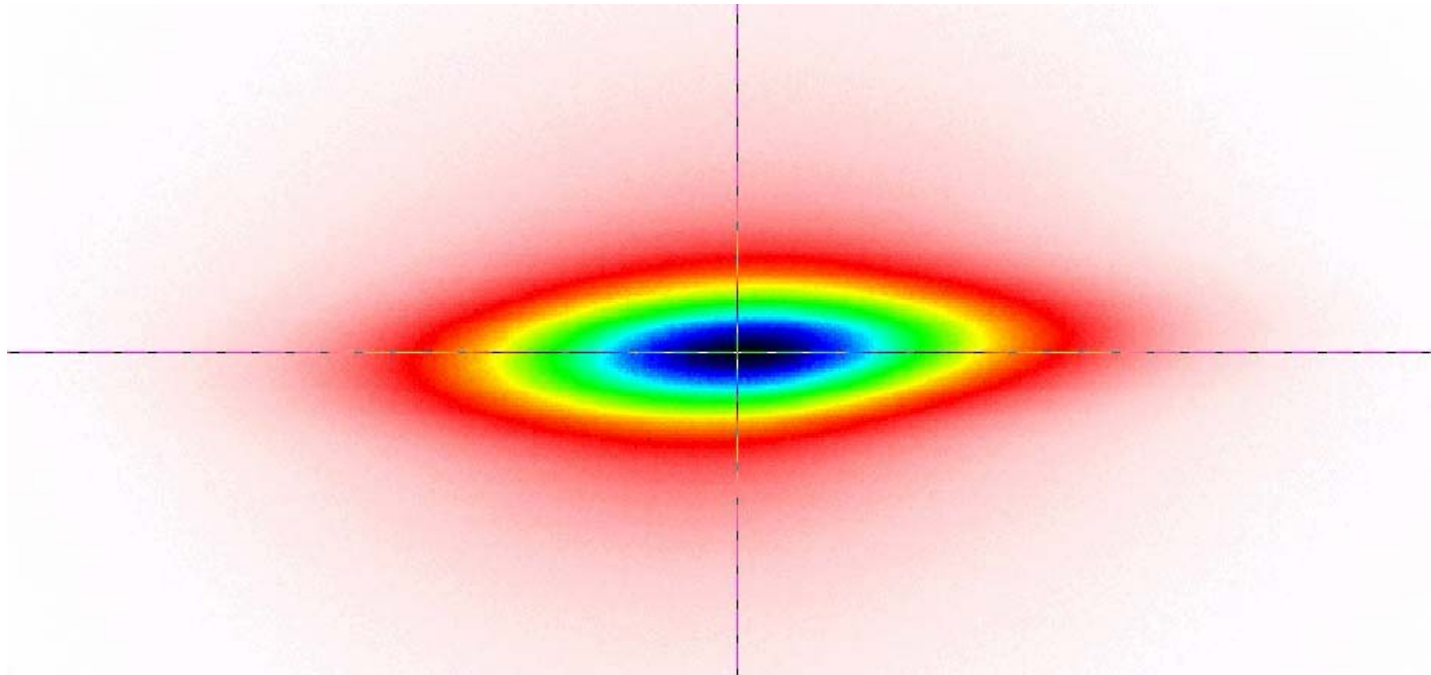


Design and Performance of GSECARS Large KB Focusing Optics

Peter J. Eng

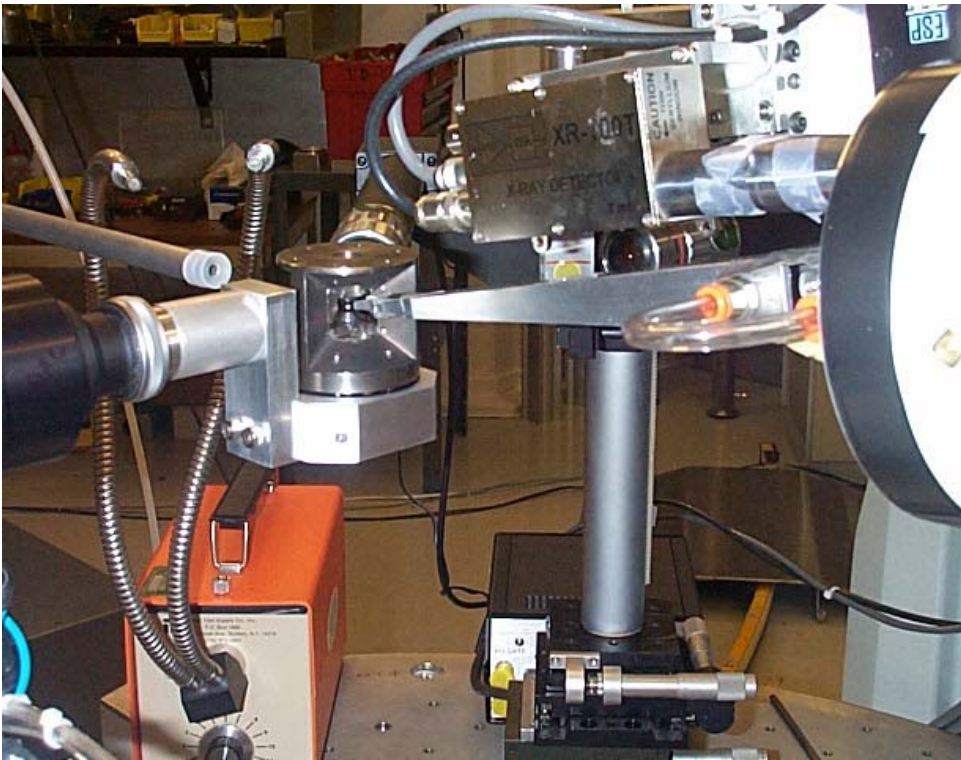
Consortium for Advanced Radiation Sources (CARS)
and The James Franck Institute (JFI)

University of Chicago



- Many earth science problems involve heterogeneous systems on length scales ranging from 500 μm to 0.5 μm .
- The high brilliance of the APS undulator allows us to strongly focus the beam while keep the divergence to levels acceptable to most of our measurements.
- Achromatic focusing needed to support spectroscopy, and multi wave length scattering experiments.
- Techniques:
 - Micro-crystal diffraction
 - Ambient conditions mounted on tapered glass fiber
 - DAC single crystals up to 20Gpa
 - Surface Scattering
 - CTR
 - Reflectivity
 - Surface Spectroscopy
 - Micro-Probe
 - Elemental mapping
 - Spectroscopy
 - Tomography
 - Q-dependent inelastic scattering

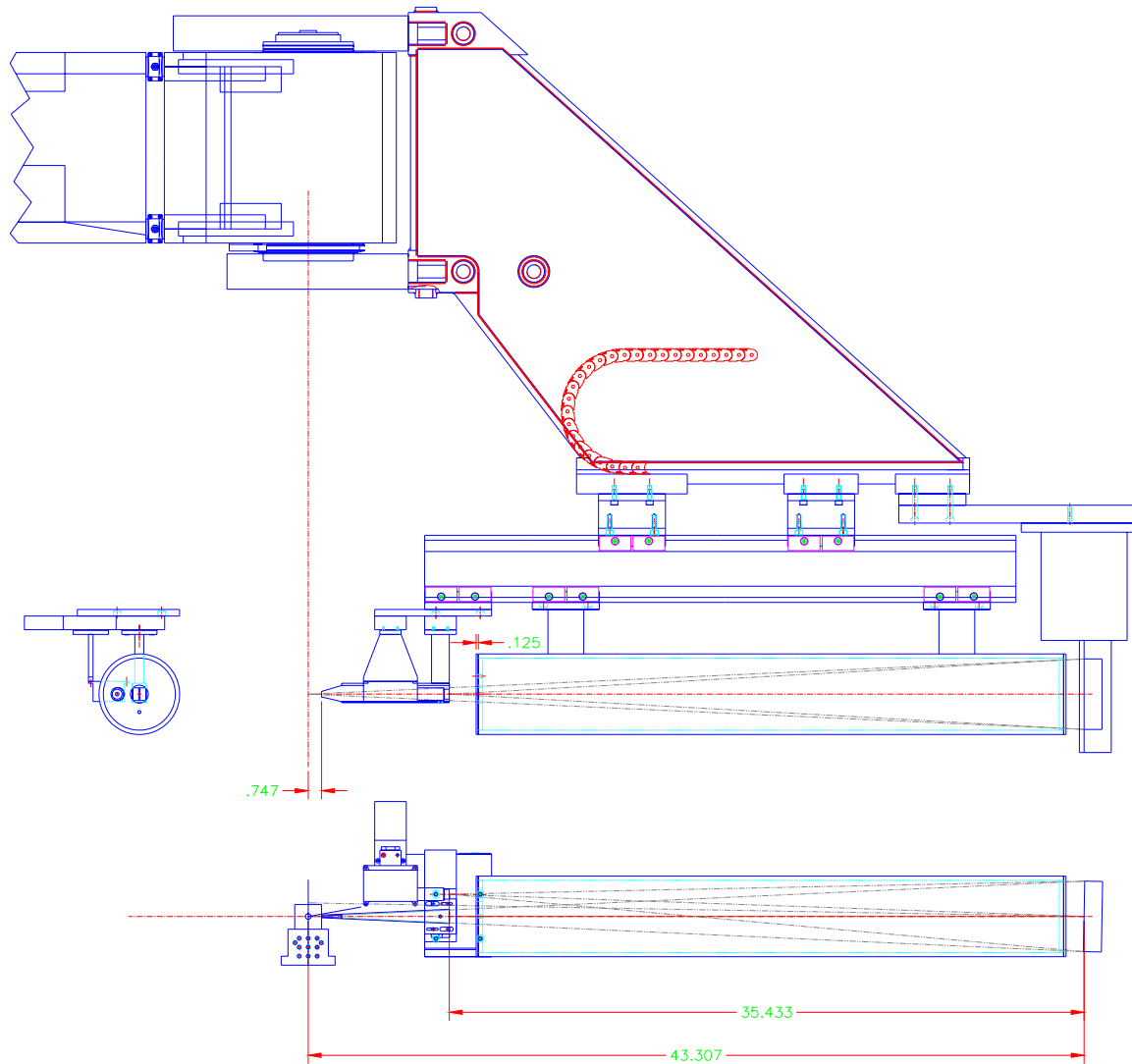




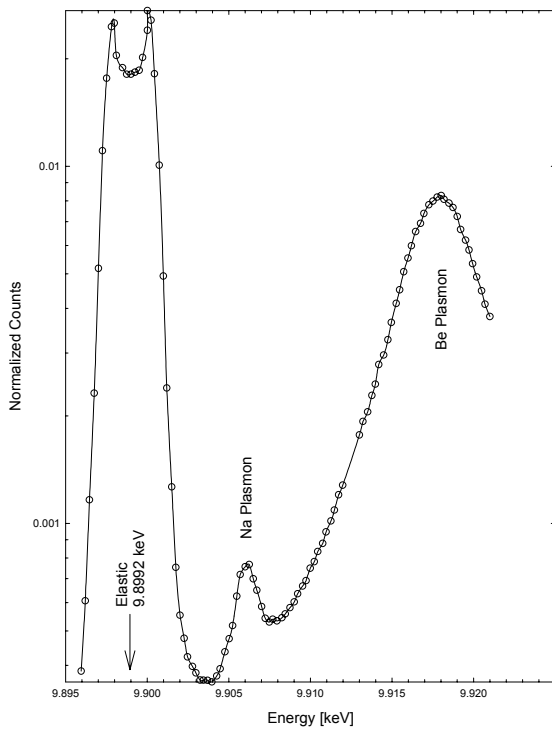
GeoSoilEnviroCARS

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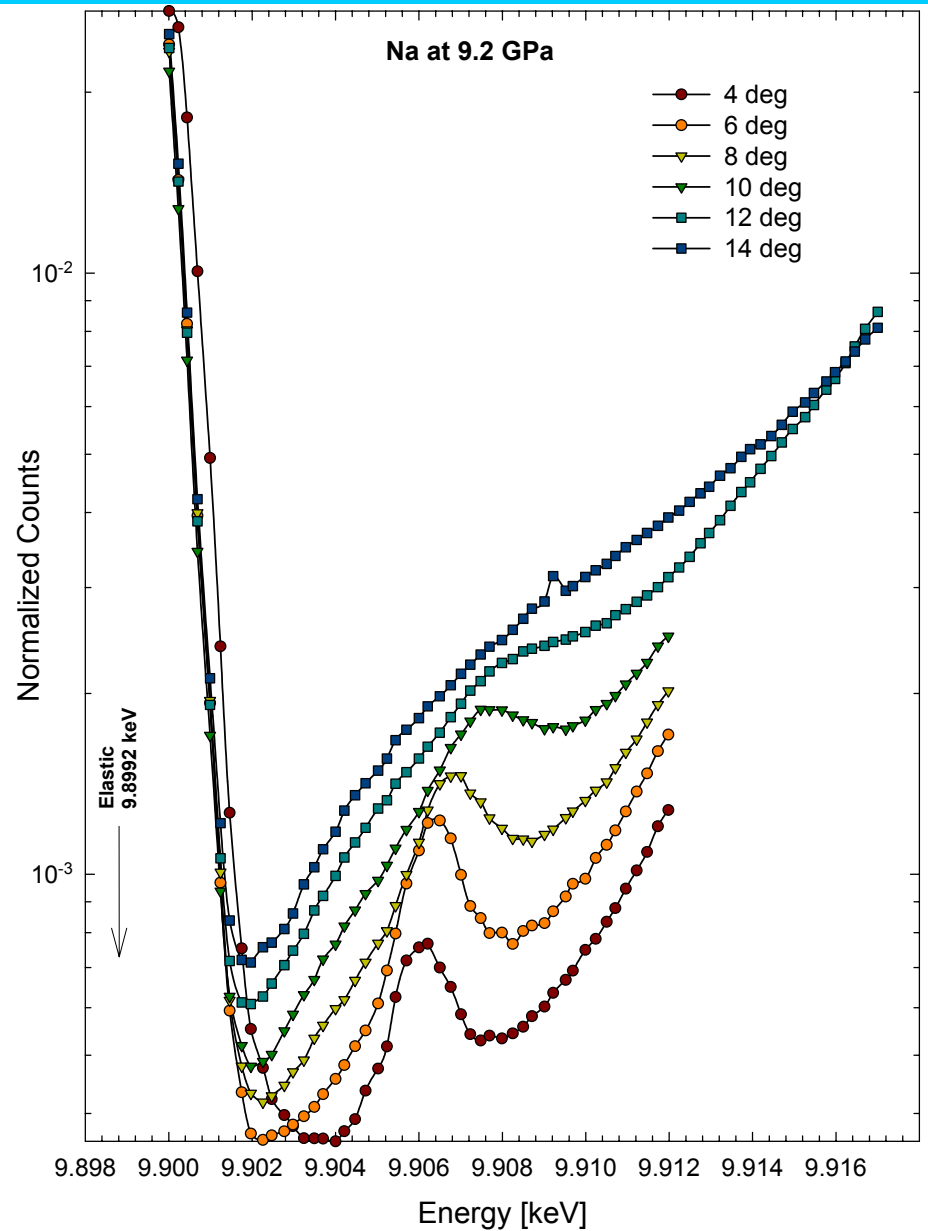
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- Inelastic scattering at high pressure:
 - Na plasmon
 - Boron Nitride: Boron K-edge, Nitrogen K-edge
 - Water plasmon and oxygen K-edge

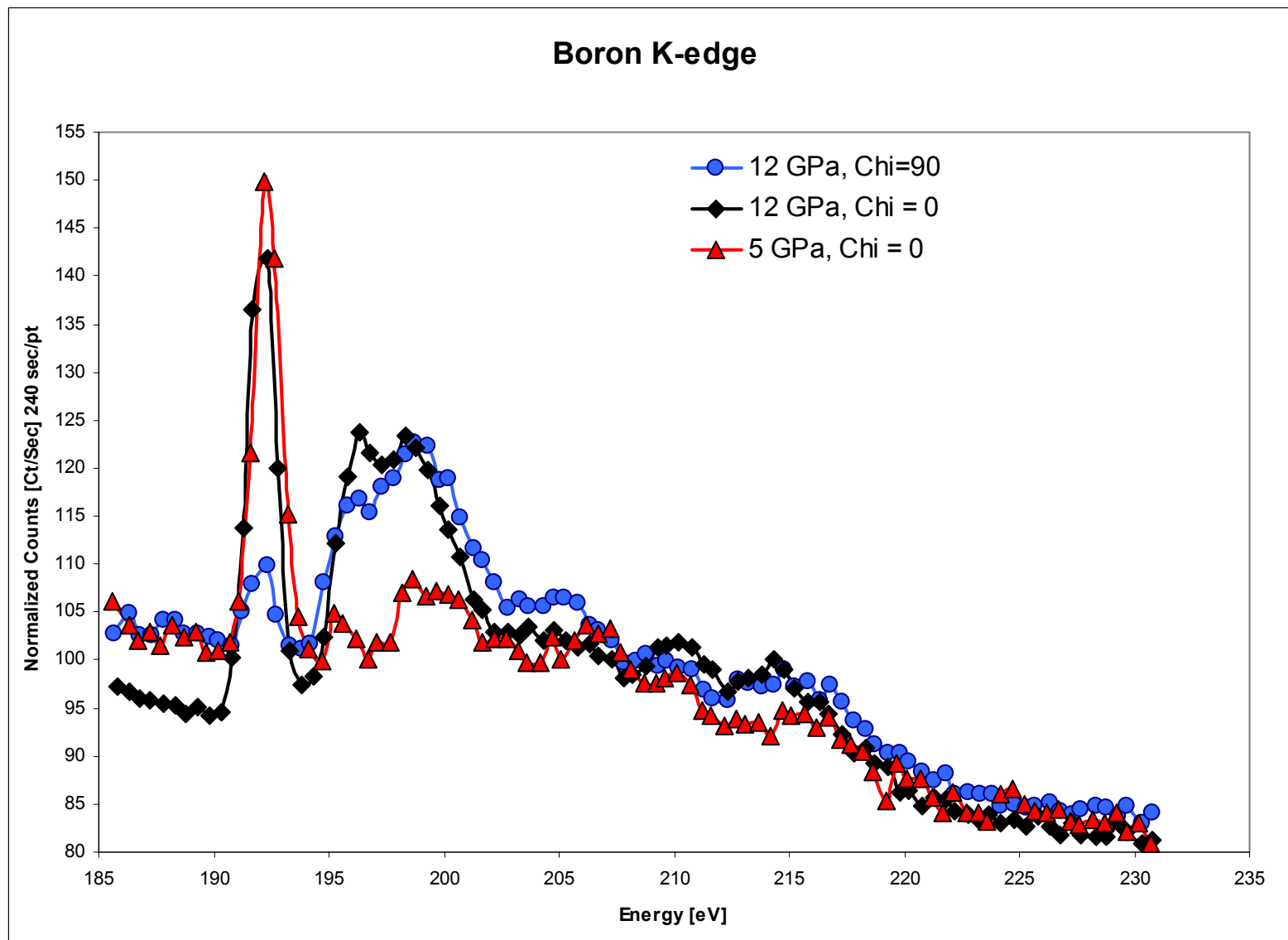


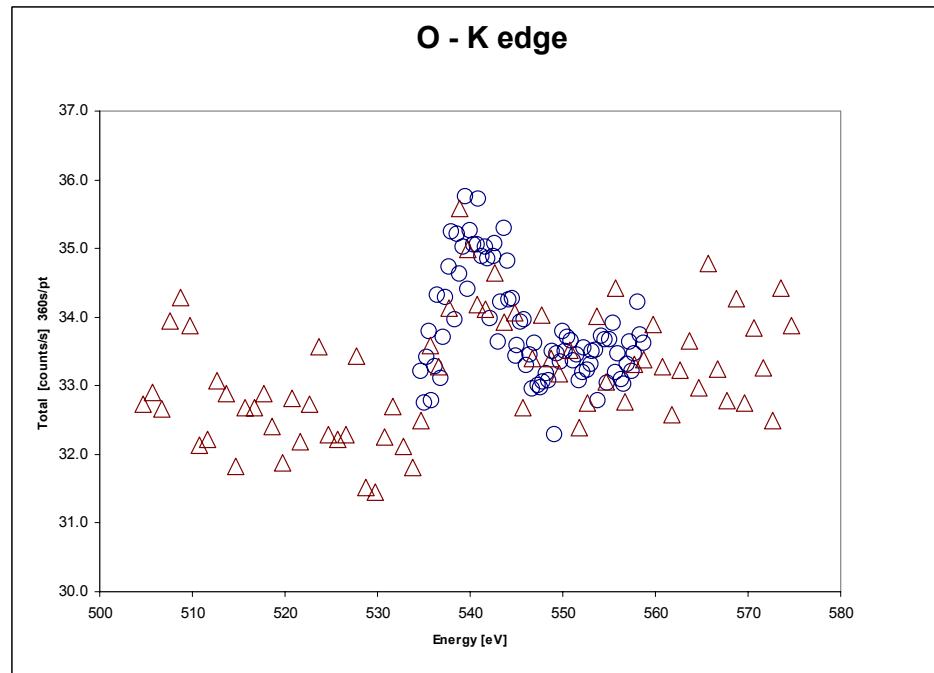
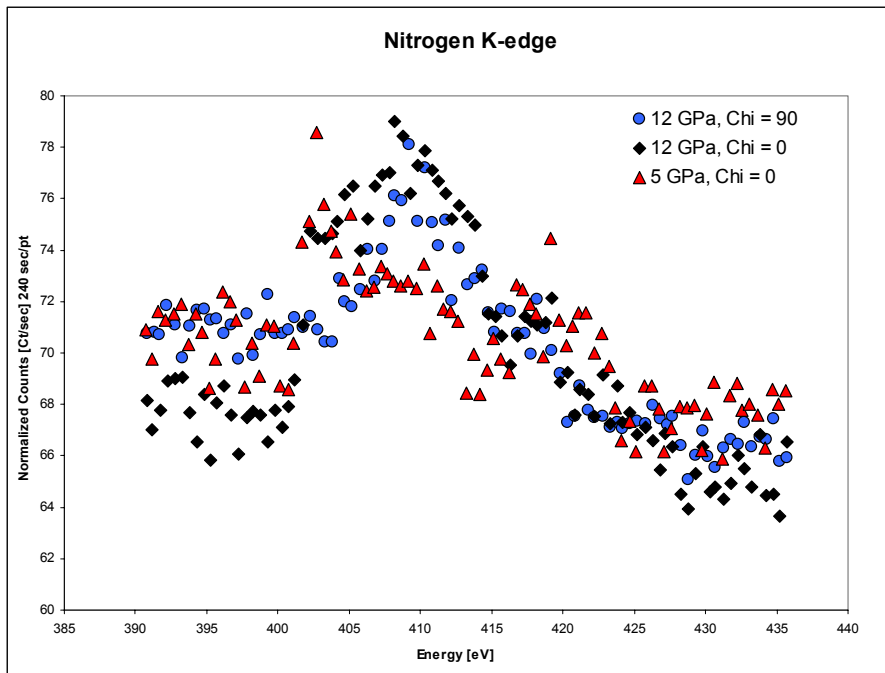
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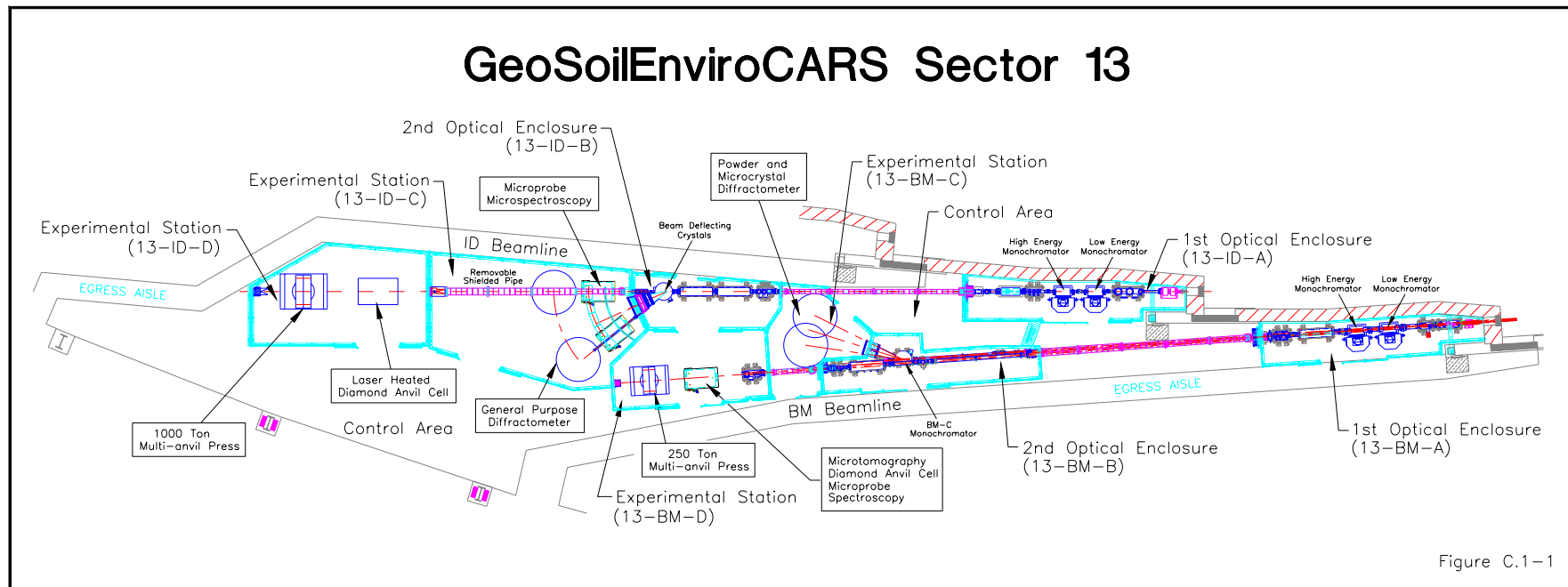


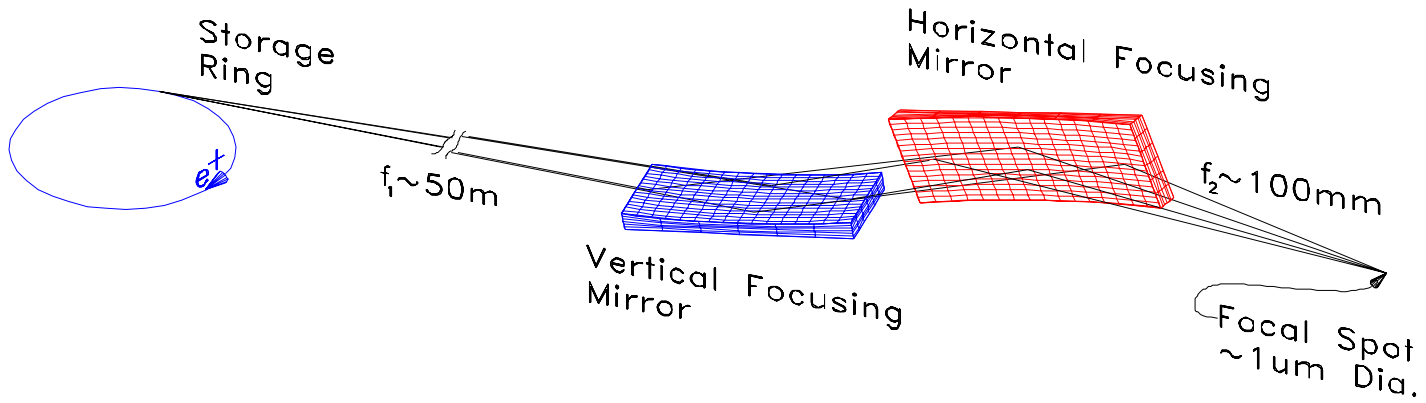
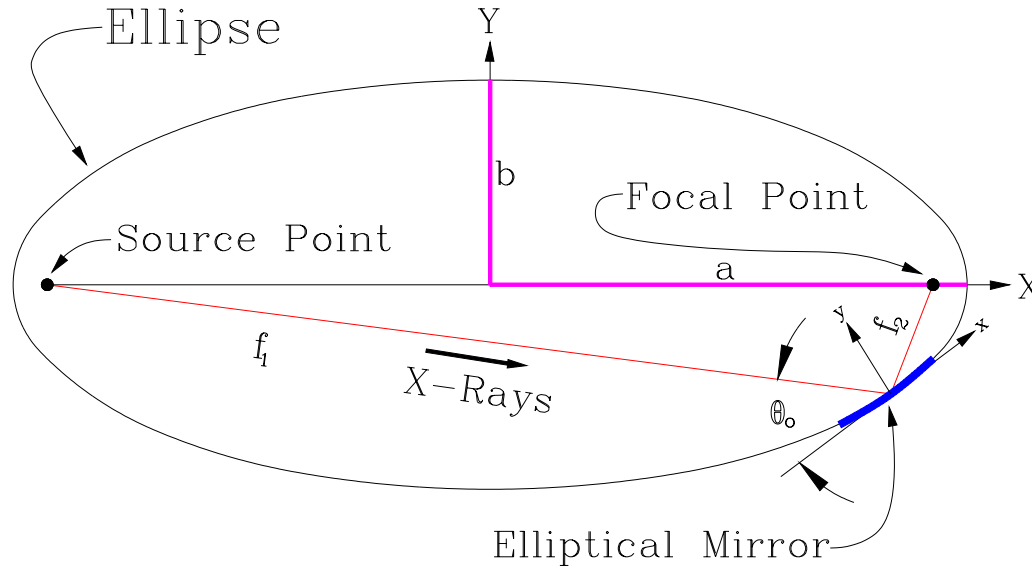
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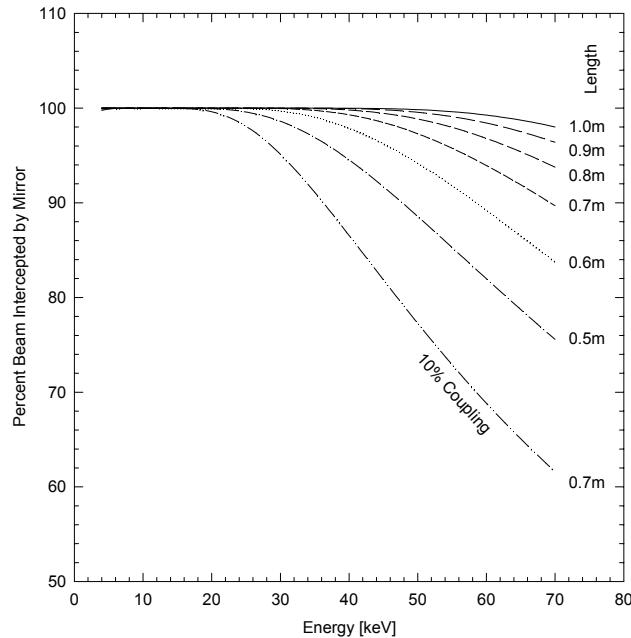




- Length

- Fraction of the beam intercepted over the desired energy range.

$$F = \text{erf} \left[\frac{\sqrt{2} \cdot 0.9 \cdot \alpha \cdot L}{4 \cdot \Sigma'_y} \right]$$

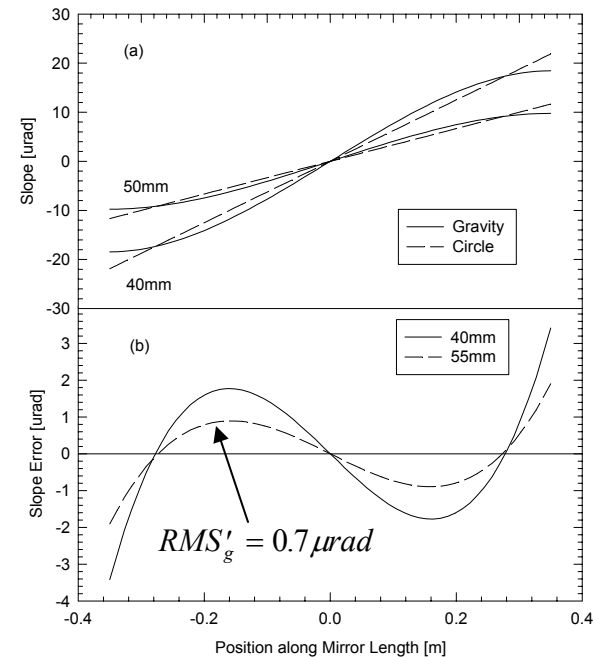


- Thickness

- Maximal allowable figure error due to gravitational sag.
- Maximal safe Bending stress

$$RMS'_g = \left(\frac{1}{\sqrt{L}} \right) \sqrt{\int_{-L/2}^{L/2} (Slope_Gravity(x) - Slope_Circle(x))^2 dx}$$

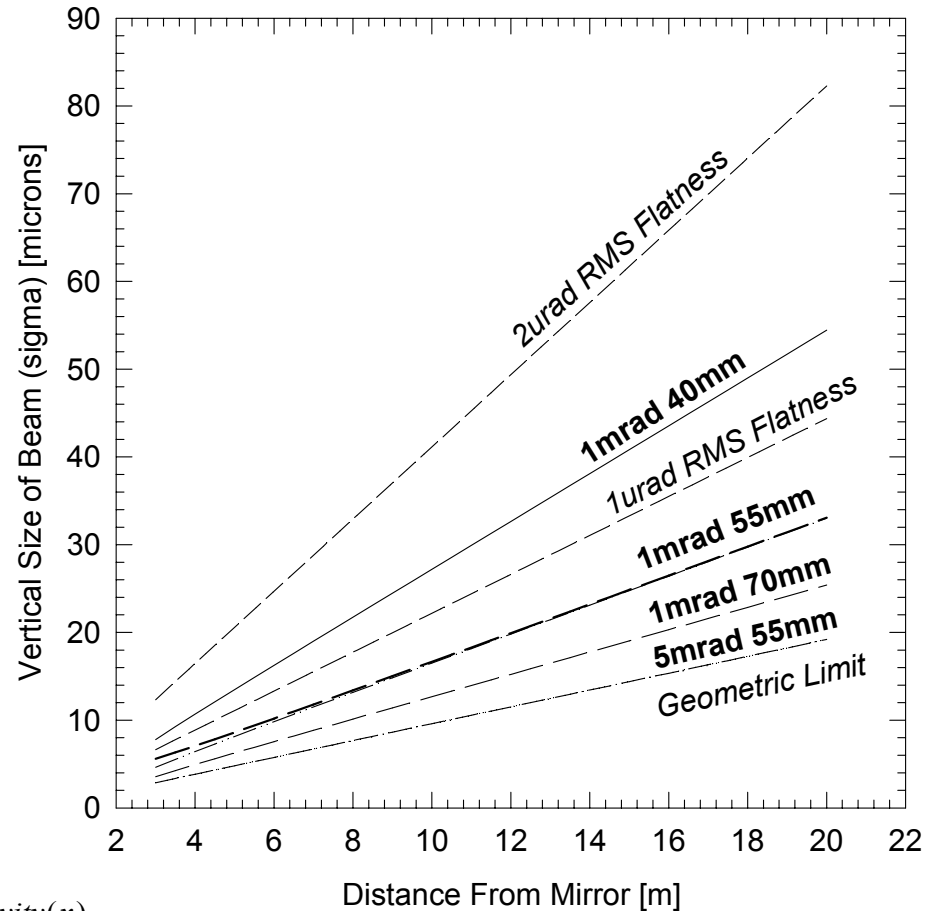
$$RMS'_g [\mu rad] = 6.5 \cdot 10^{-6} \frac{(L[mm])^3}{(c[mm])^2} \quad \leftarrow \text{For Si}$$



Design Philosophy - Mirror Dimensions – Predicted Performance

We Compute RMS slope error of the mirror by performing a non-linear LSQ fit to an ideal ellipse of the beam weighted two moment slope function and gravitational sag.

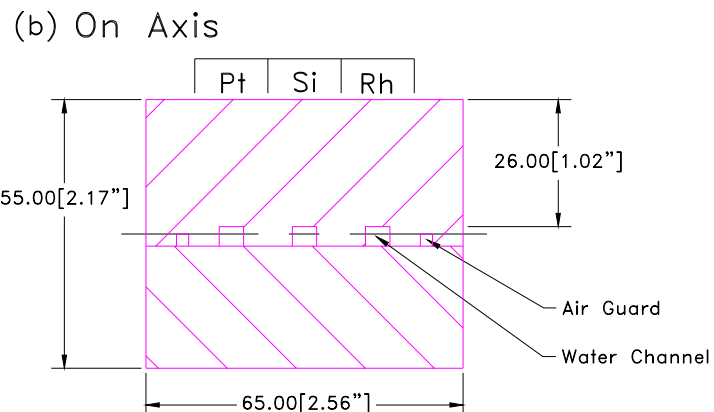
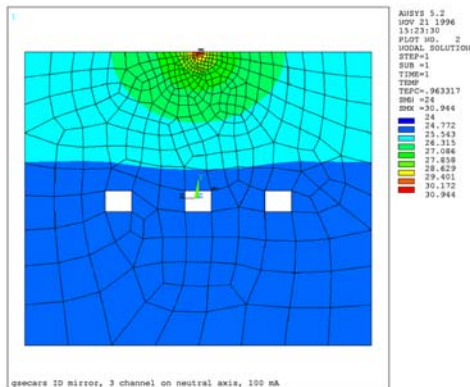
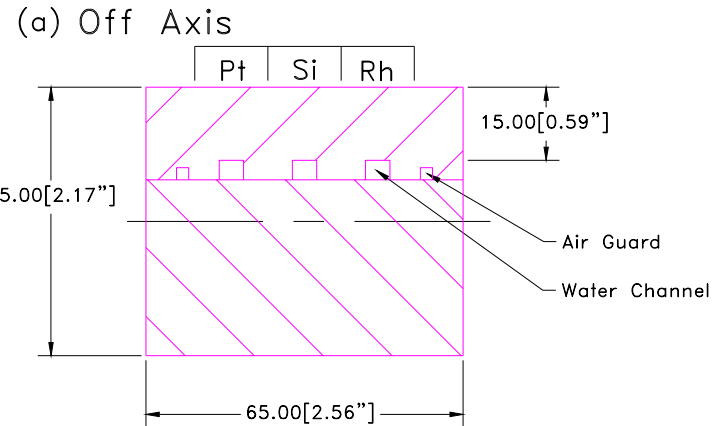
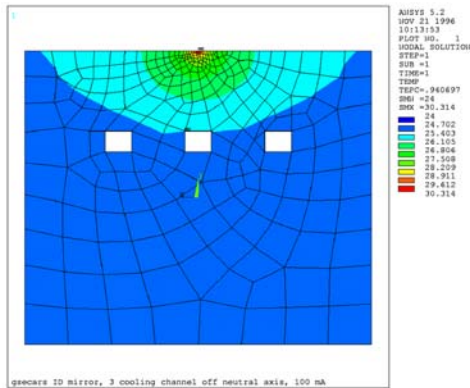
$$W(x) = \frac{\sin(\theta_o) \cdot e^{-\frac{1}{2} \left(\frac{x \sin(\theta_o)}{\Sigma'_y \cdot S} \right)^2}}{\sqrt{2\pi} \cdot \Sigma'_y \cdot S \cdot \text{erf} \left(\frac{\sqrt{2} \sin(\theta_o) L}{4 \Sigma'_y \cdot S} \right)}$$



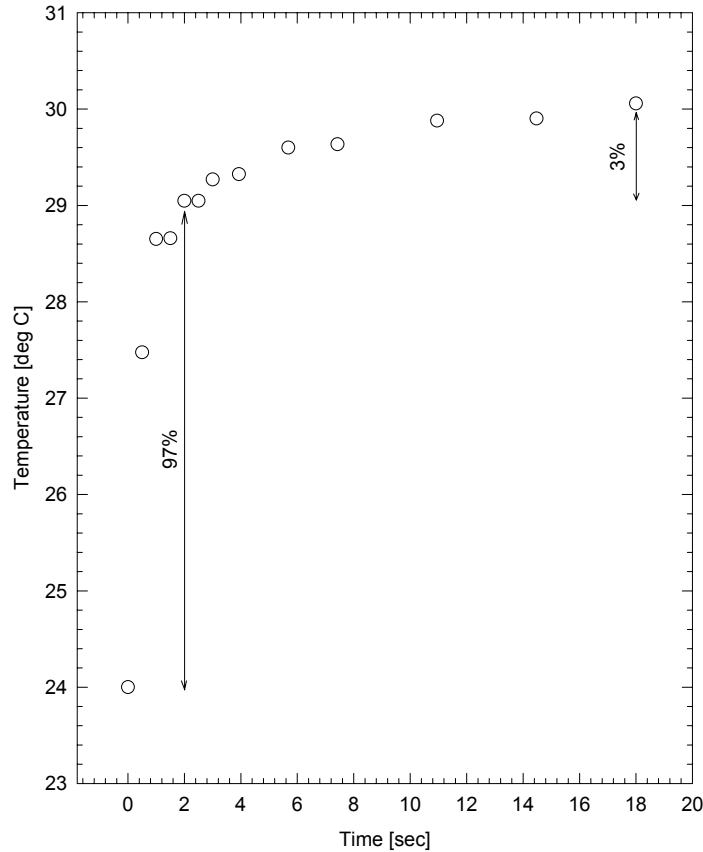
$$\text{Slope_Mirror}(x, K, \eta) = \text{Slope_Bender}(x, K, \eta) - \text{Slope_Gravity}(x)$$



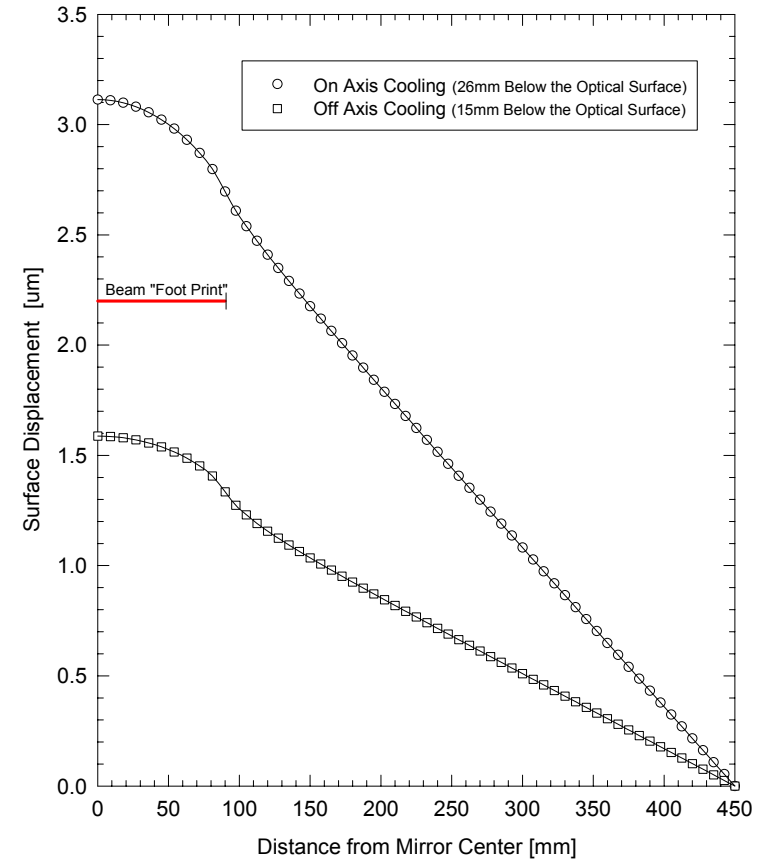
- White beam operation
 - Limited to 100W with a power limiting aperture.
 - For the modeling we used a foot print at 5mrad of 1.5 mm wide by 180 mm long resulting in a worst case power density of 0.4 W/mm².
- Mirror is internally water cooled.

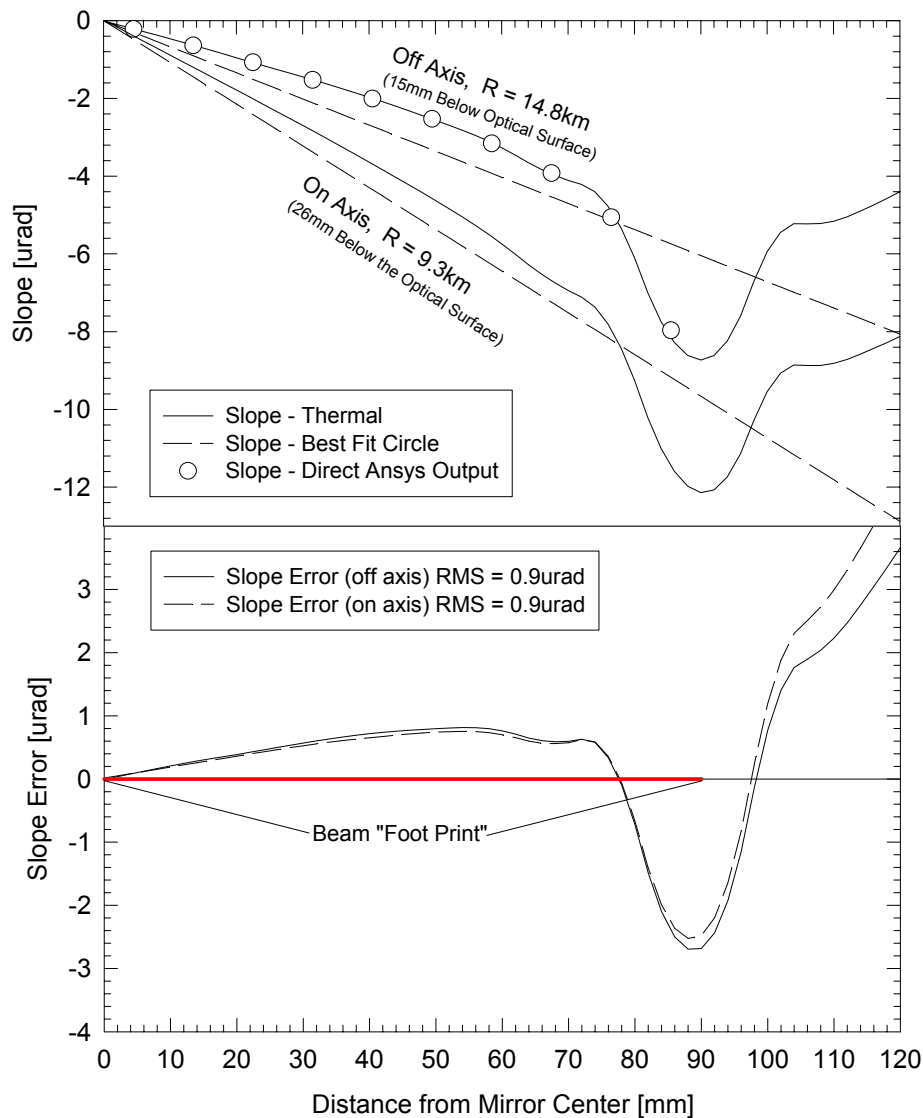


- Thermal Transient
 - Mirror achieves 97% of the max Temperature in 2 sec
 - Achieves steady state in approximately 18 sec



- Thermal Displacement
 - Determined by feeding the thermal results into ANSYS structural package





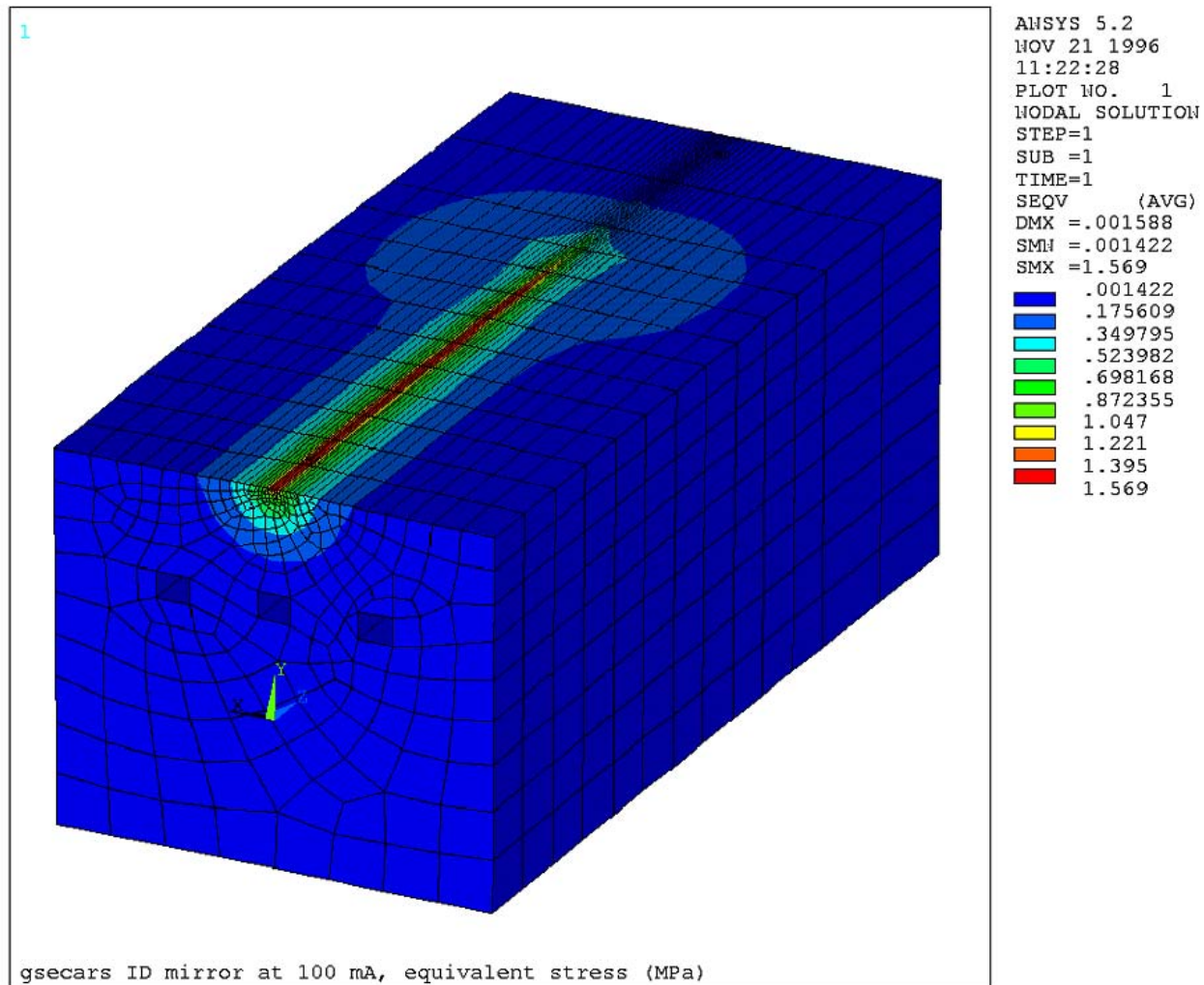
- Slope Error
 - Over the beam foot print the slope error is the same
 - Off axis cooling
 - R = 14.8 km
 - Slope Error = 0.9urad
 - On axis cooling
 - R = 9.3 km
 - Slope Error = 0.9urad
- Thermal Stability
 - For ring current starting at 100ma and dropping to 50ma with an initially corrected thermal bump R and foot print x_o the slope error would increase to:

$$RMS' = \frac{x_o}{4\sqrt{3} \cdot R}$$

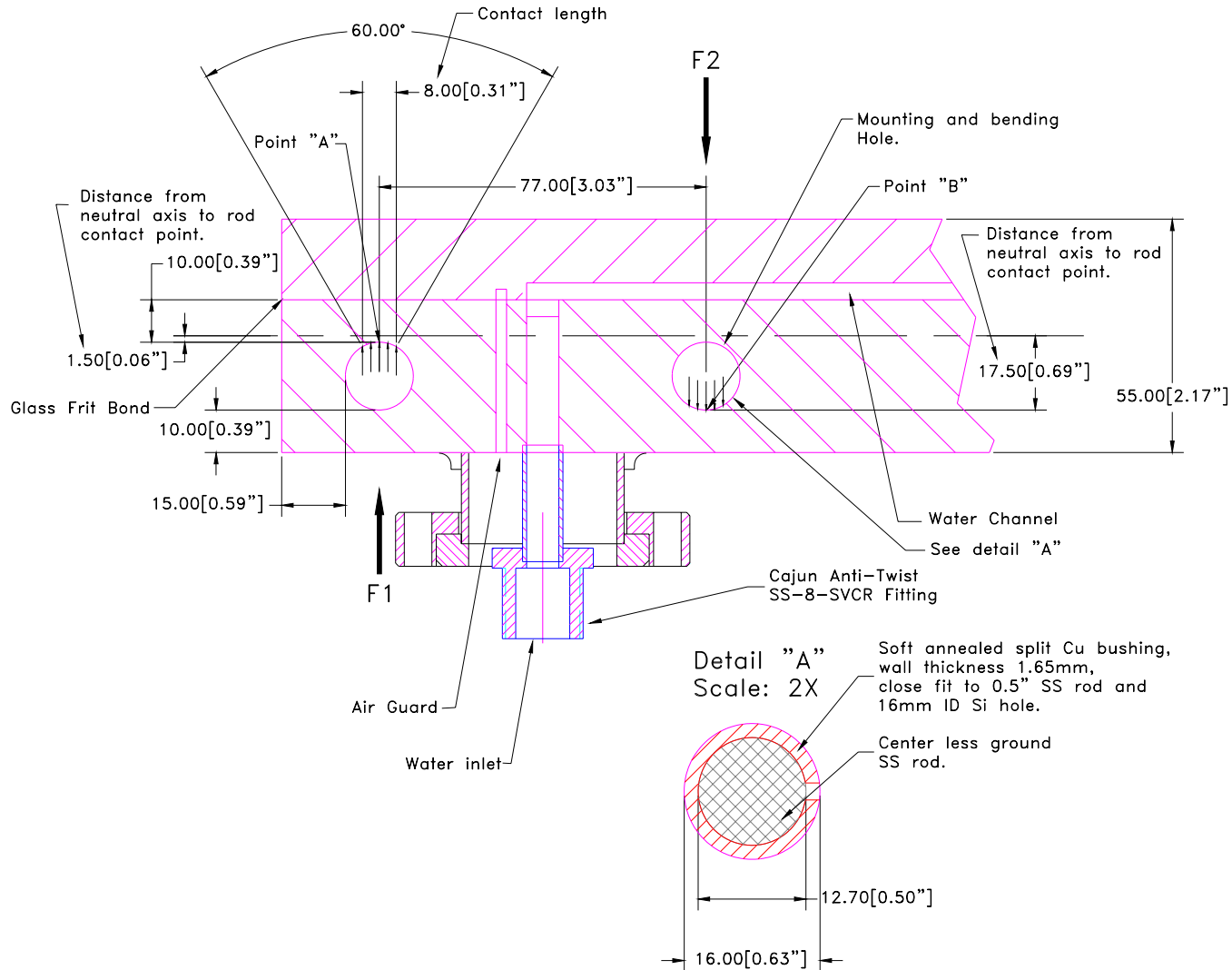
- For the off axis case $RMS' = 1.8\mu rad$
- Resulting in a increase in focal size by a factor of 4!



- The maximum thermal equivalent stress for off axis cooling is 1.57 MPa (228 psi) well below the safe limit for Si of 100 psi.



- Once the length, thickness and cooling geometry are determined, the mirror support and bender interface can be designed.



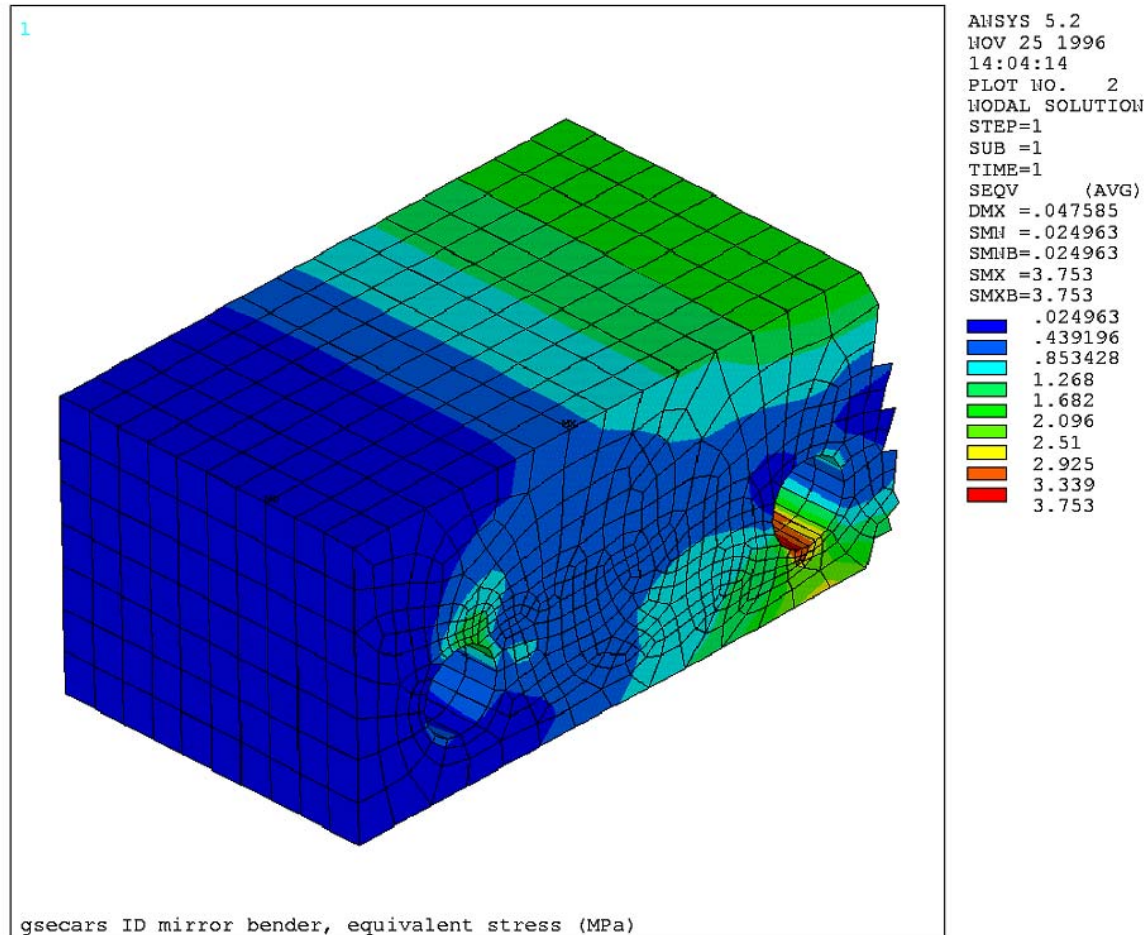
- A simple expression for the maximum contact pressure of the bending rod is:

$$P = \frac{M}{d \cdot Area} = \frac{Y \cdot c^3}{12 \cdot R \cdot d \cdot g}$$

- For our mirror dimensions we find assuming a contact angle of 60deg at maximum curvature ($R = 1.8$ km) the maximum:
 - contact force is 200 lb
 - pressure 239 psi



- Performing ANSYS modeling we find:
 - Maximum equivalent stress to be 3.8 MPa (544 psi) just below the inner bending hole contact point.
 - The stress then drops to 2.9 Mpa (424 psi) on the back surface near the bending hole.

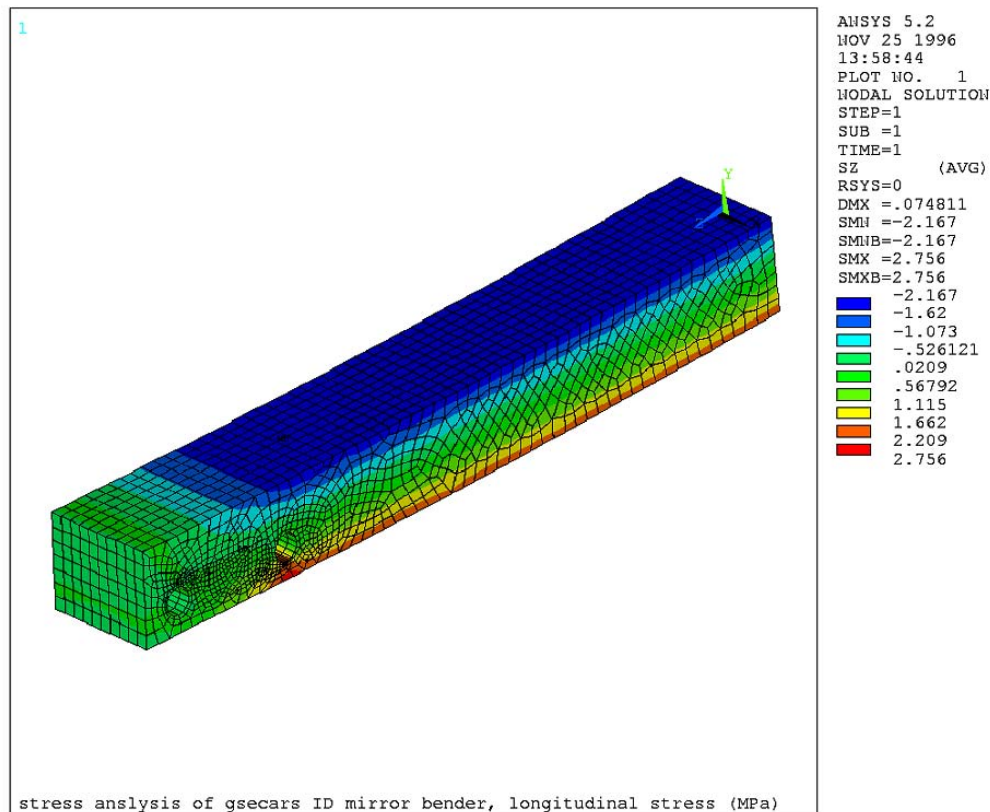


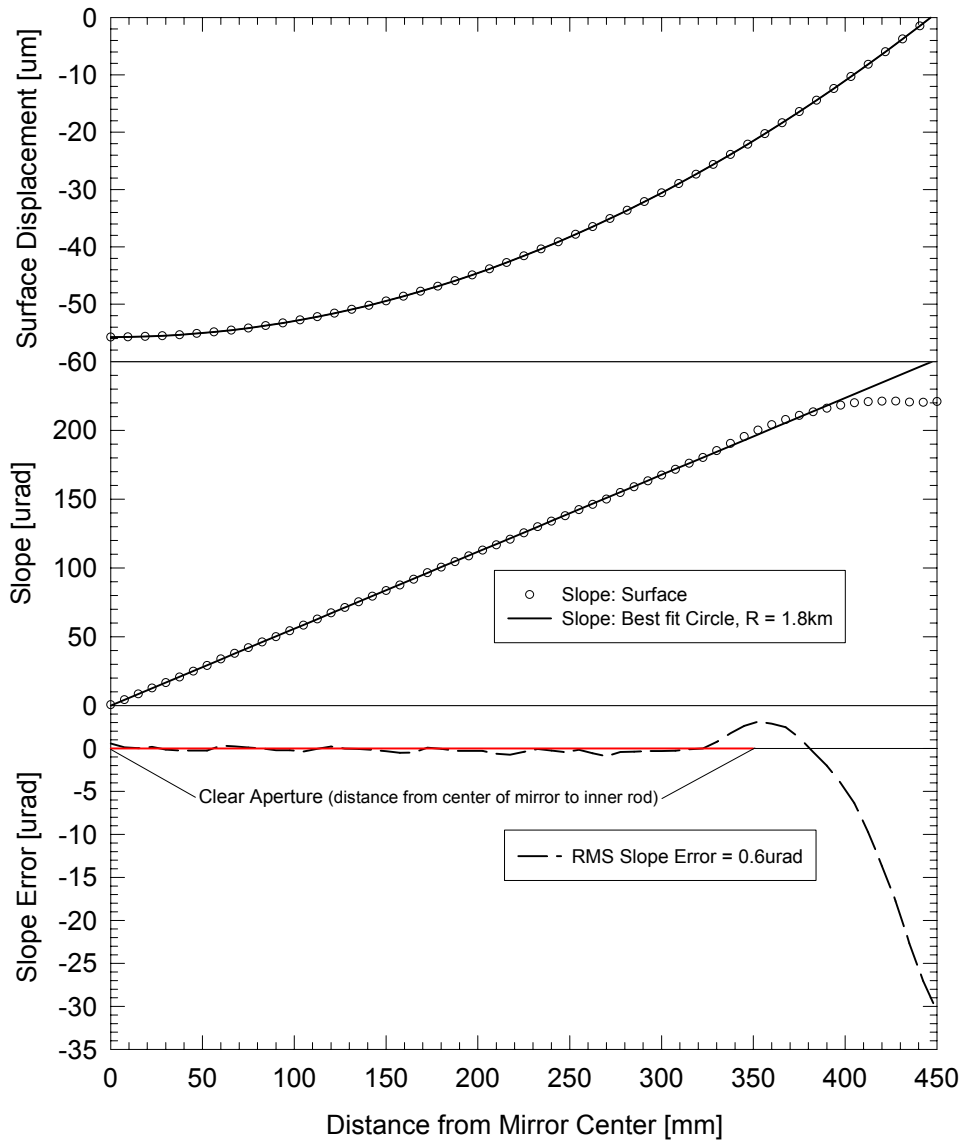
- The longitudinal stress of the bent mirror can be estimated using the analytical expression:

$$\sigma_{Bending} = \frac{M \cdot \frac{c}{2}}{I} = \frac{Y \cdot \frac{c}{2}}{R}$$

Yielding in our case: $\sigma_{Bending} = 292 \text{ psi} = 2 \text{ MPa}$

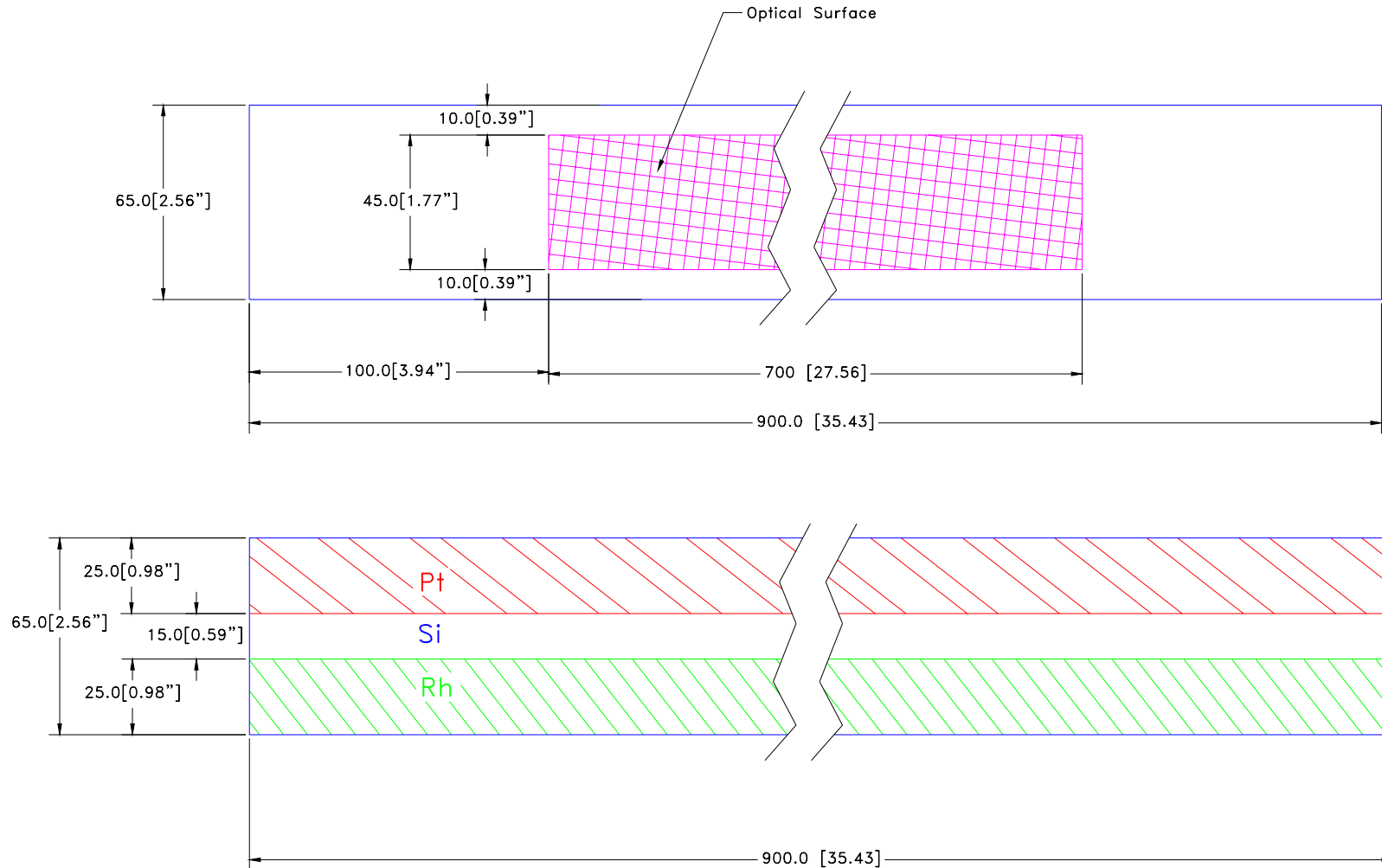
- The analytical result is in good agreement with ANSYS model below resulting in a maximum longitudinal stress component of 2.2MPa

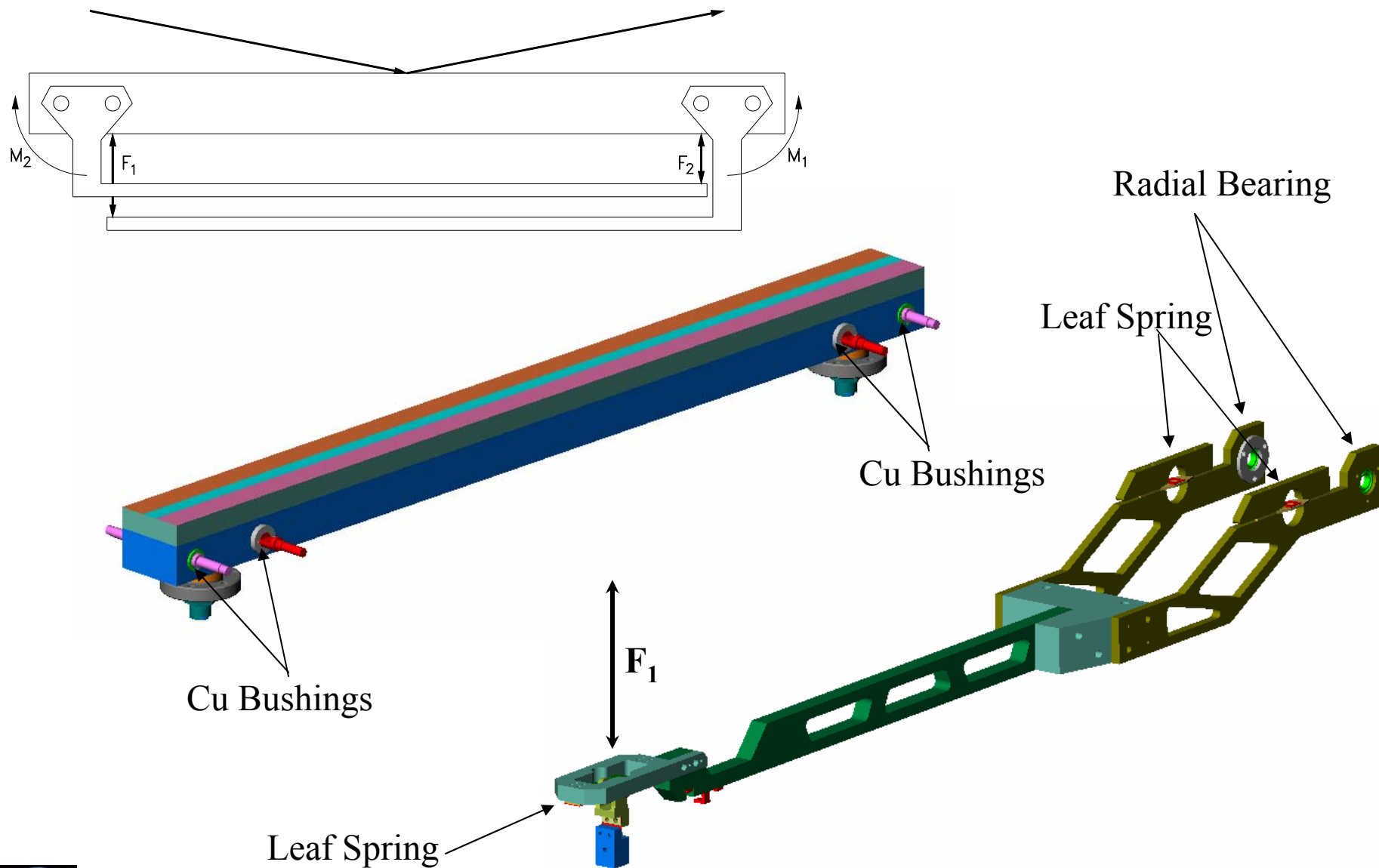


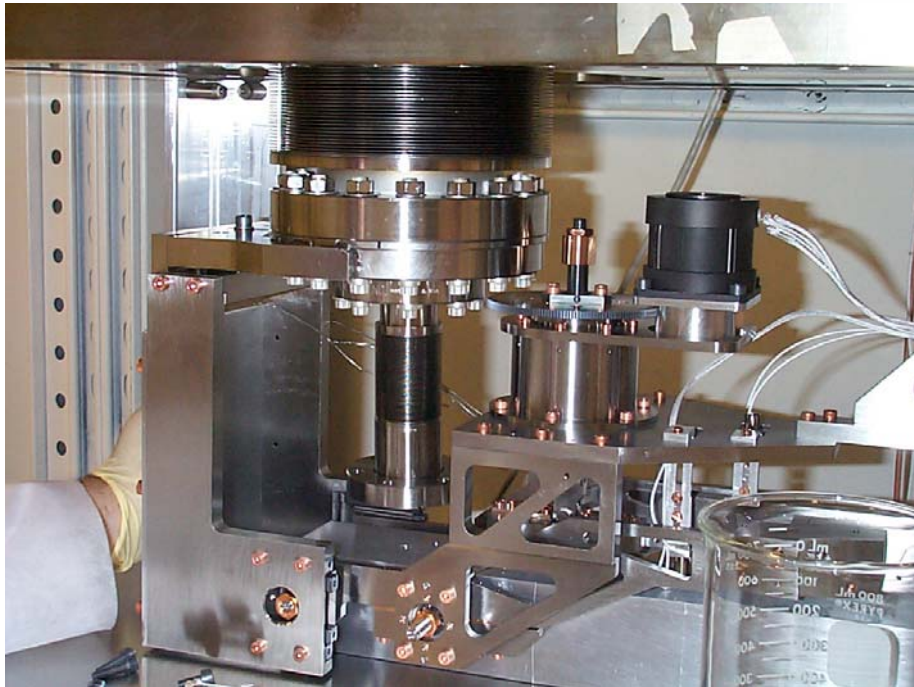
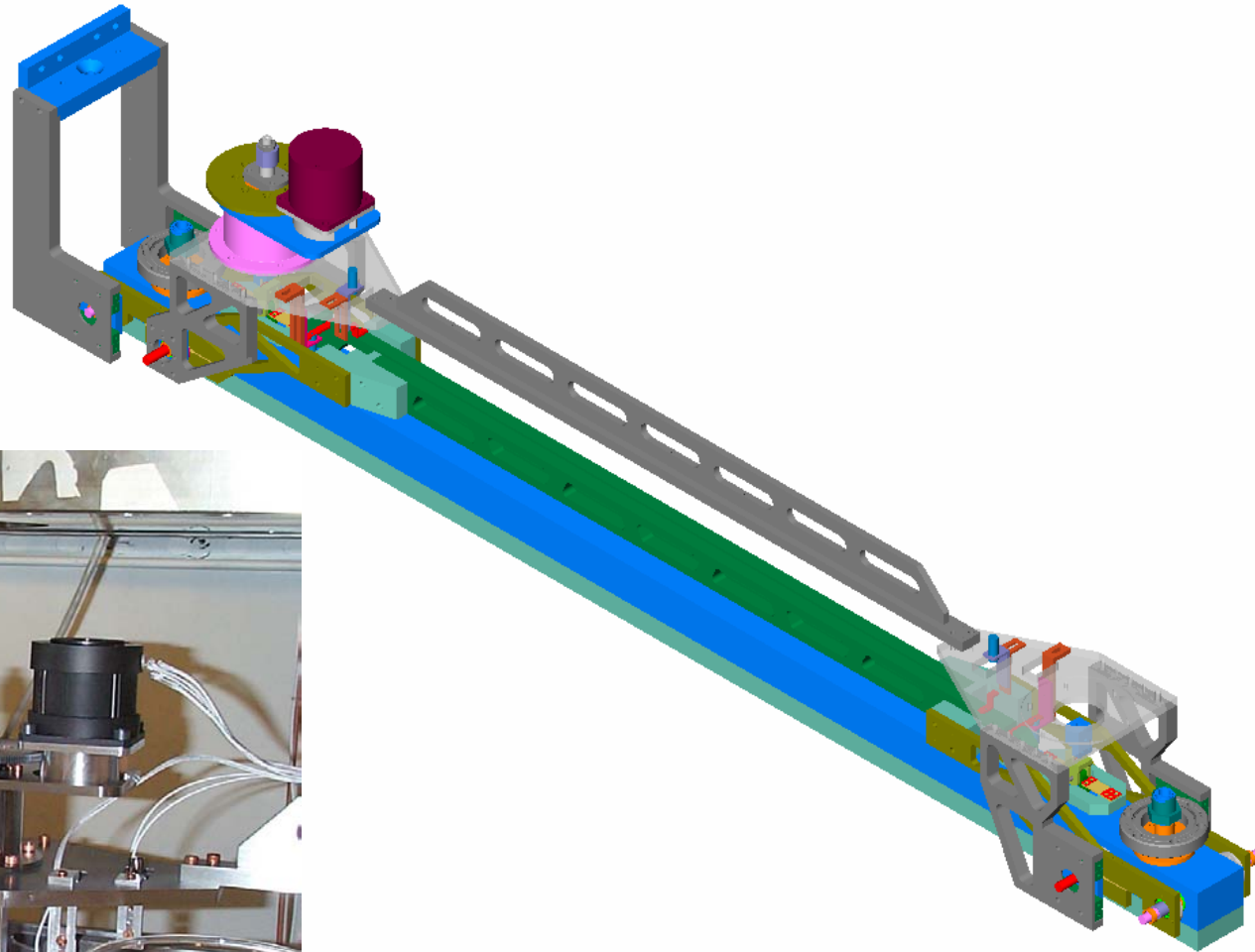


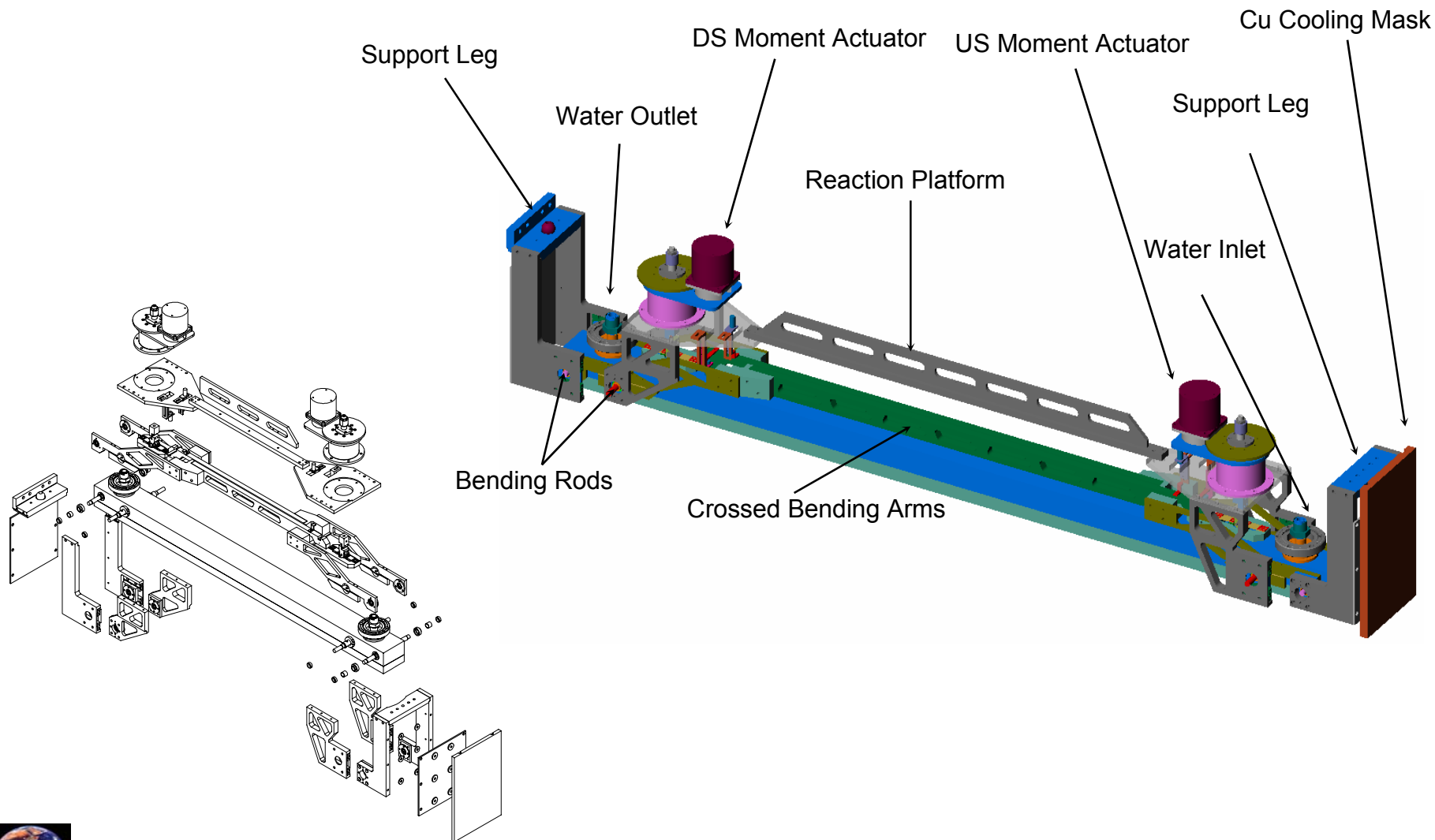
- Optical aperture equal to the distance between the inner bending rods
- Last 25mm contributes about 0.6 μrad of slope error
- Nearly the full length is a perfect circle.



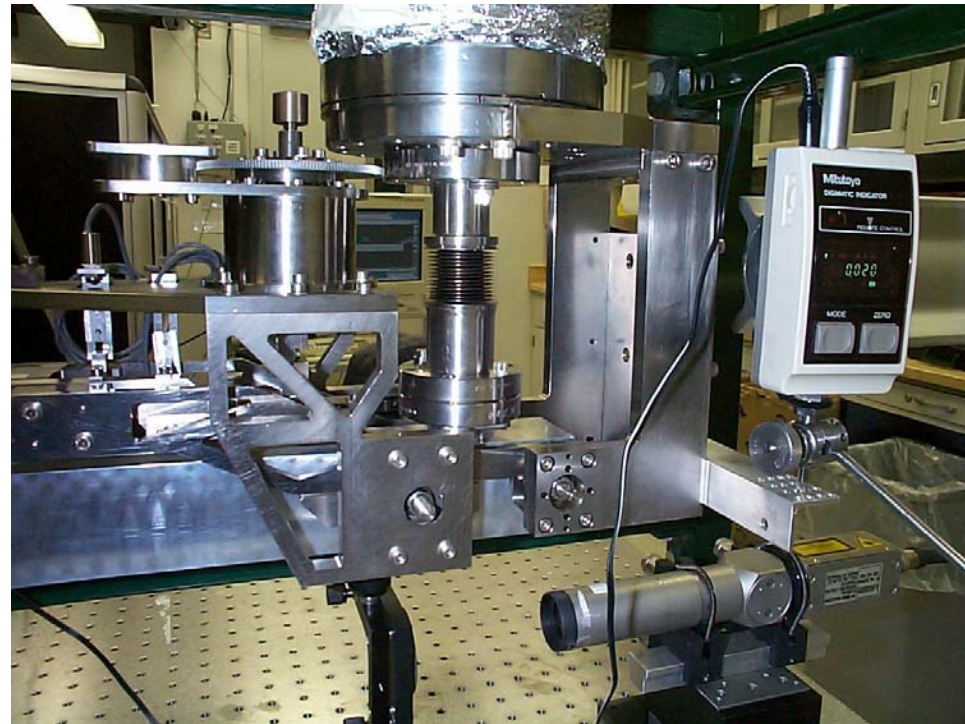
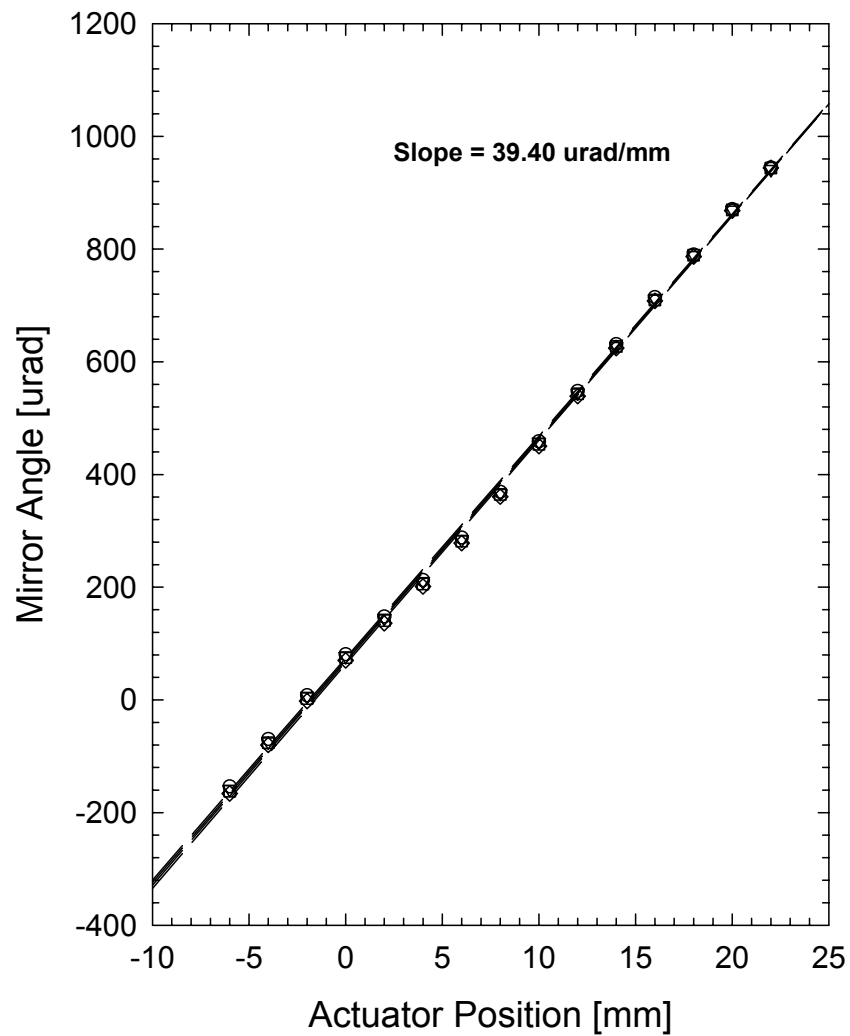


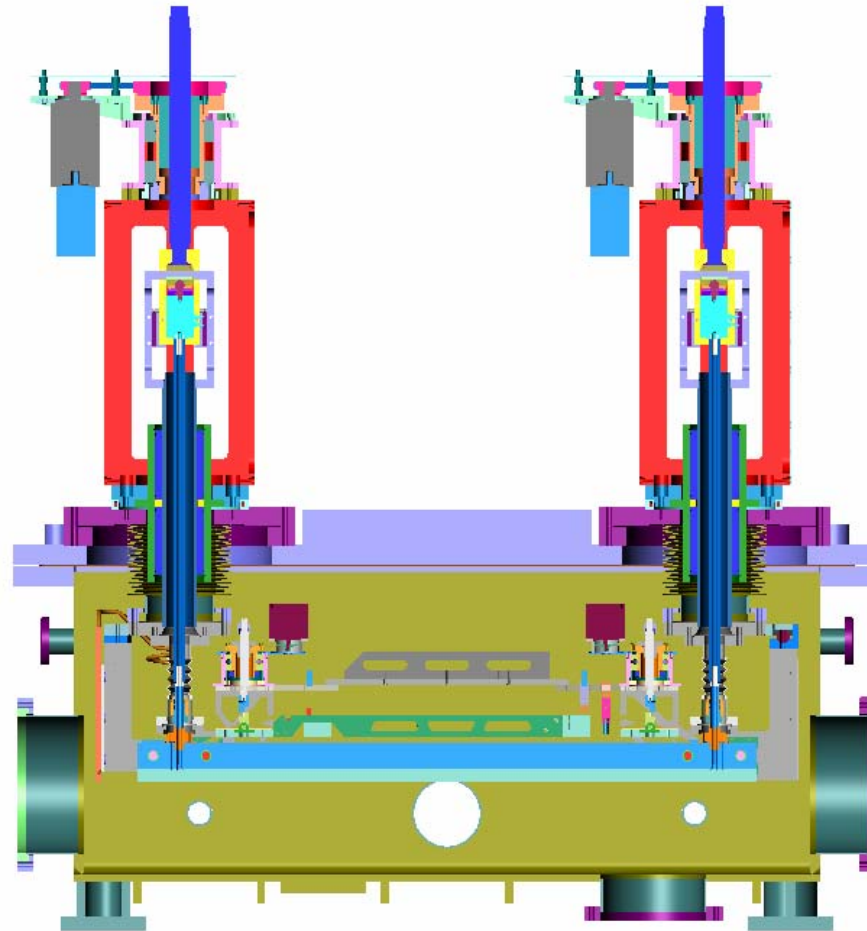


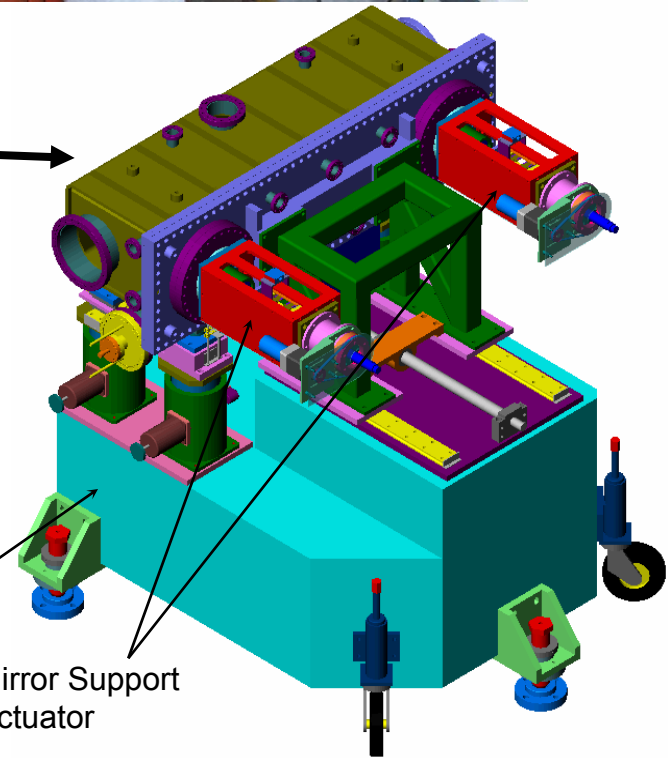
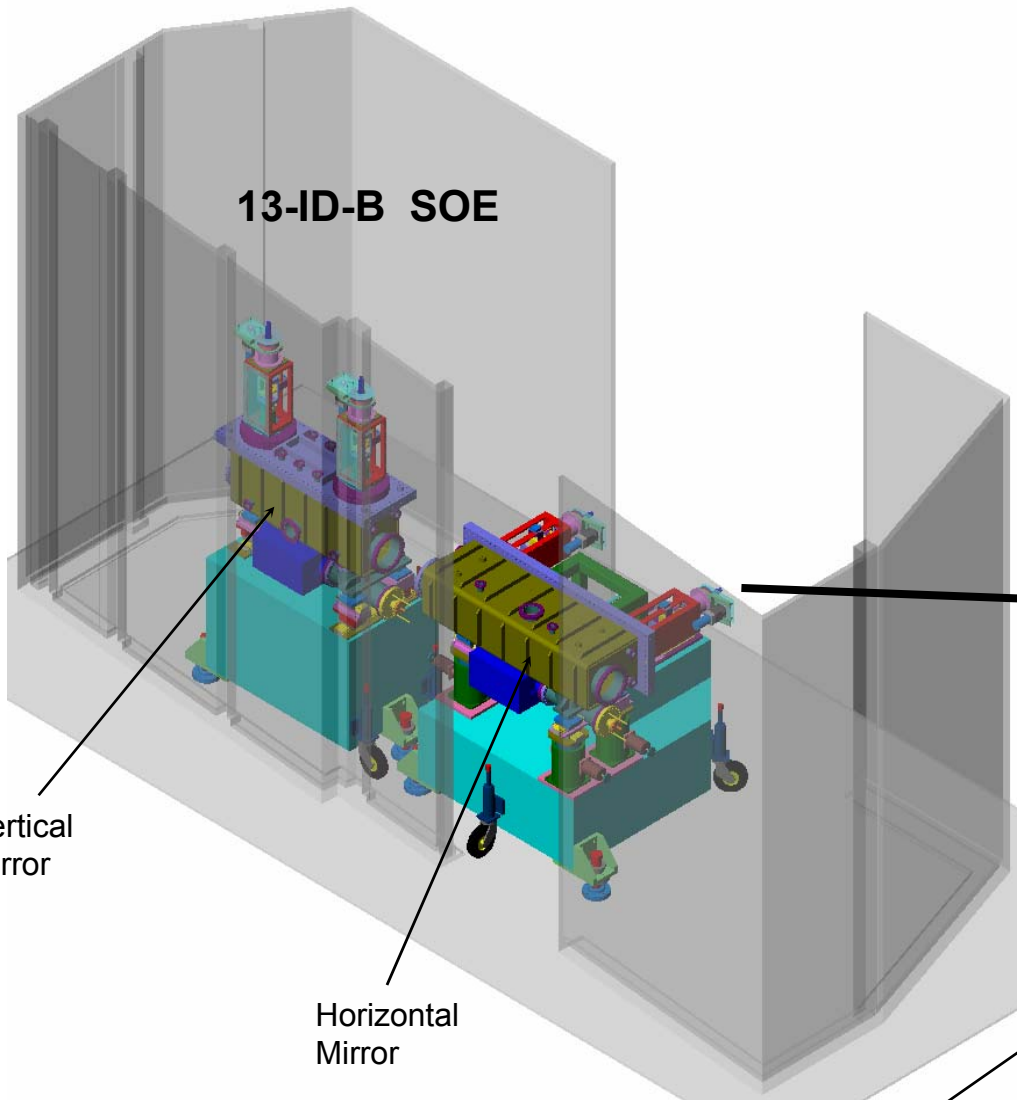




DS = US
Mirror in DS Position







Granite Block

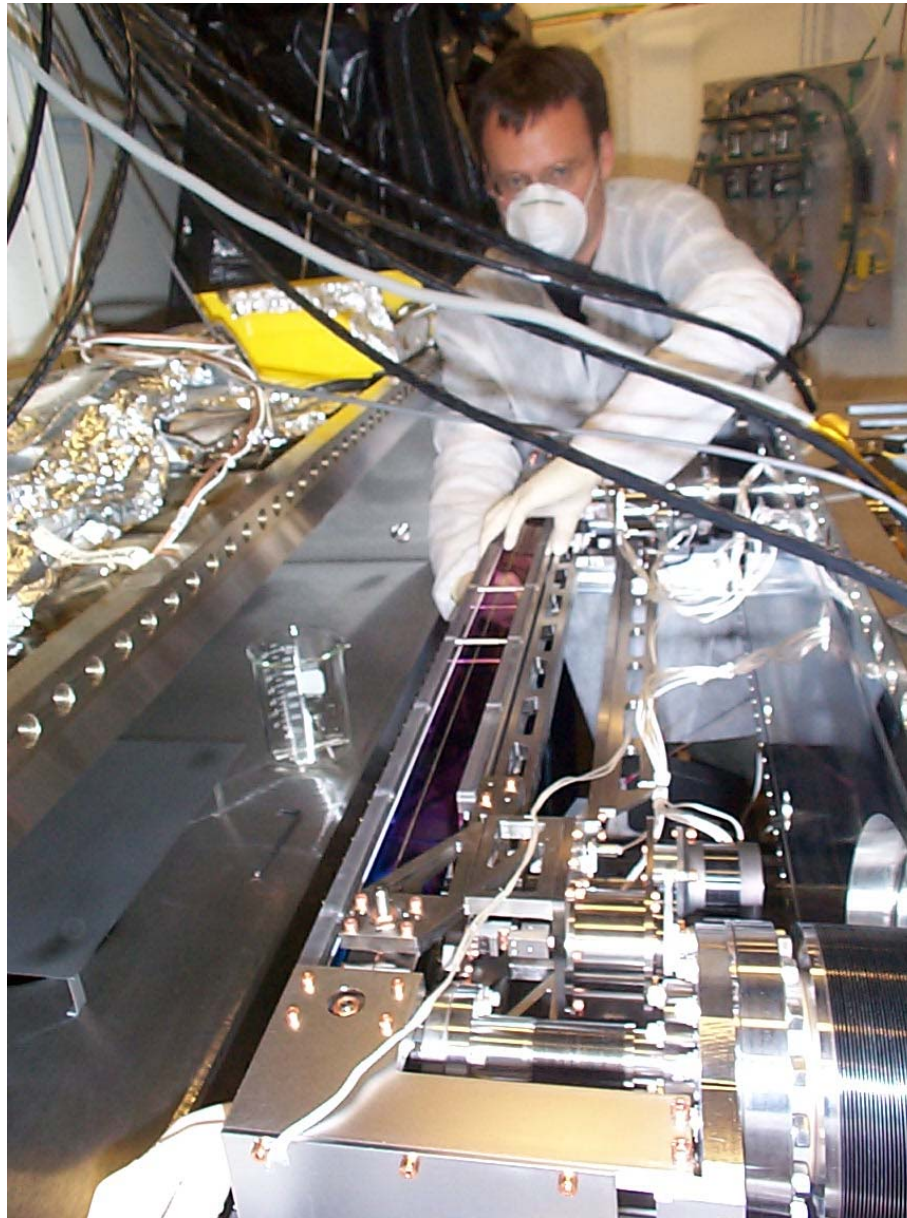


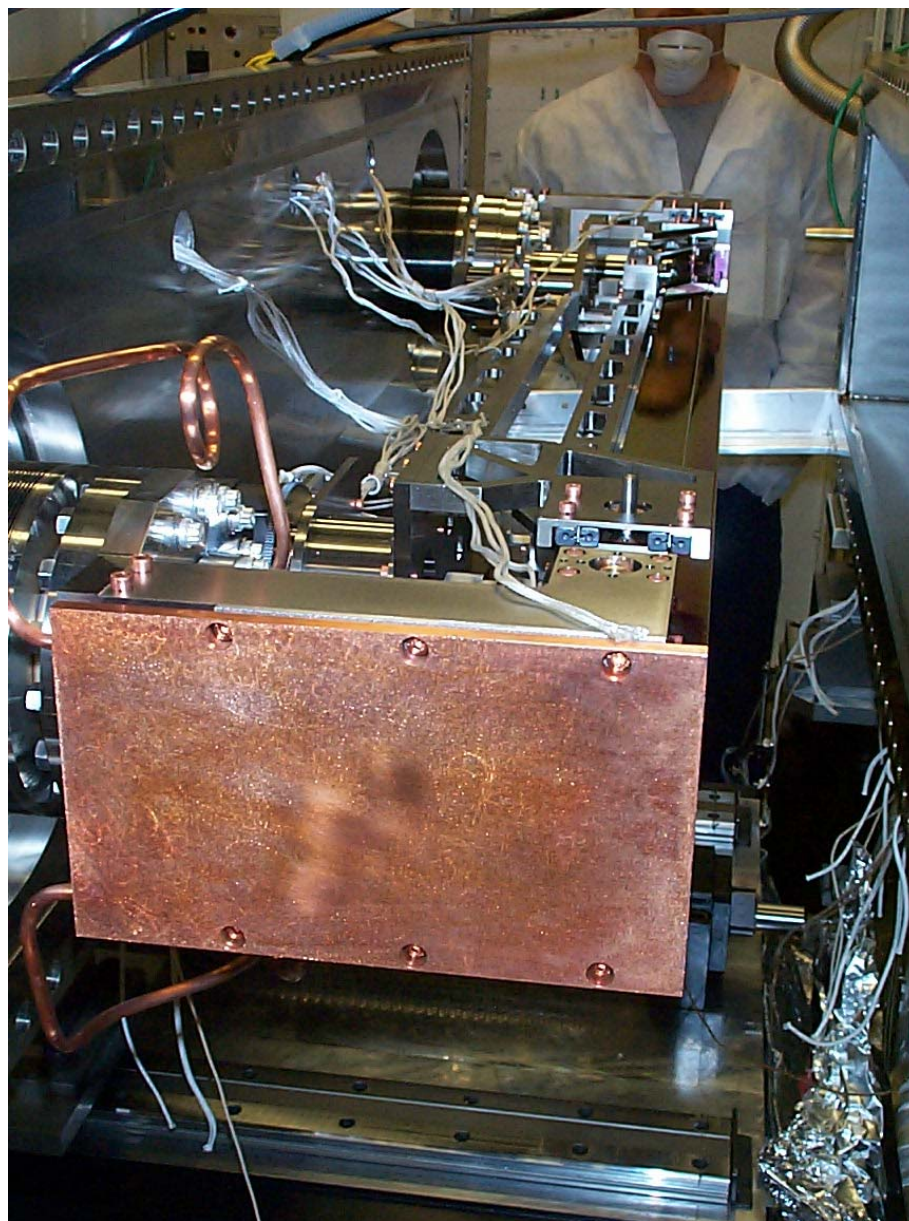
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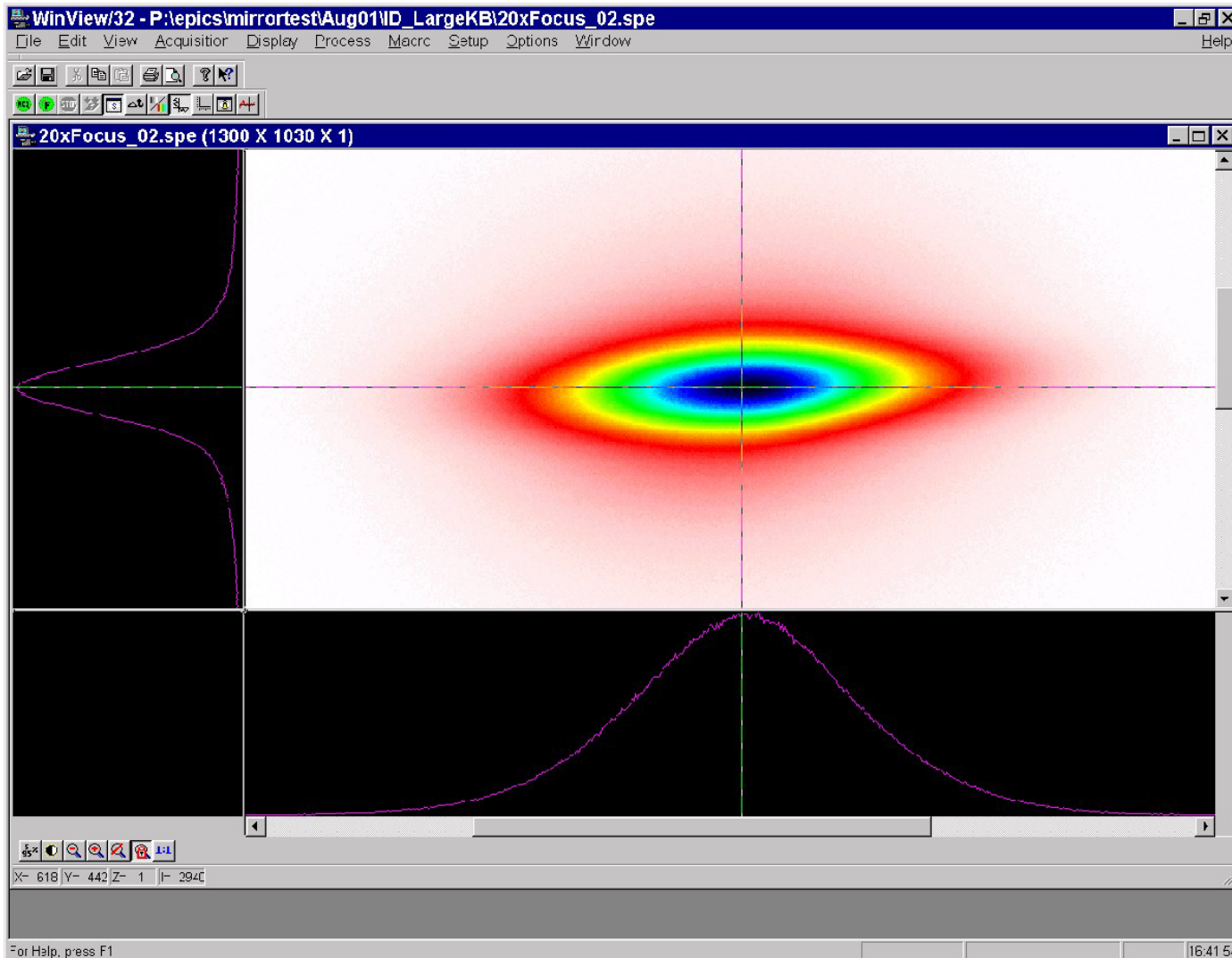


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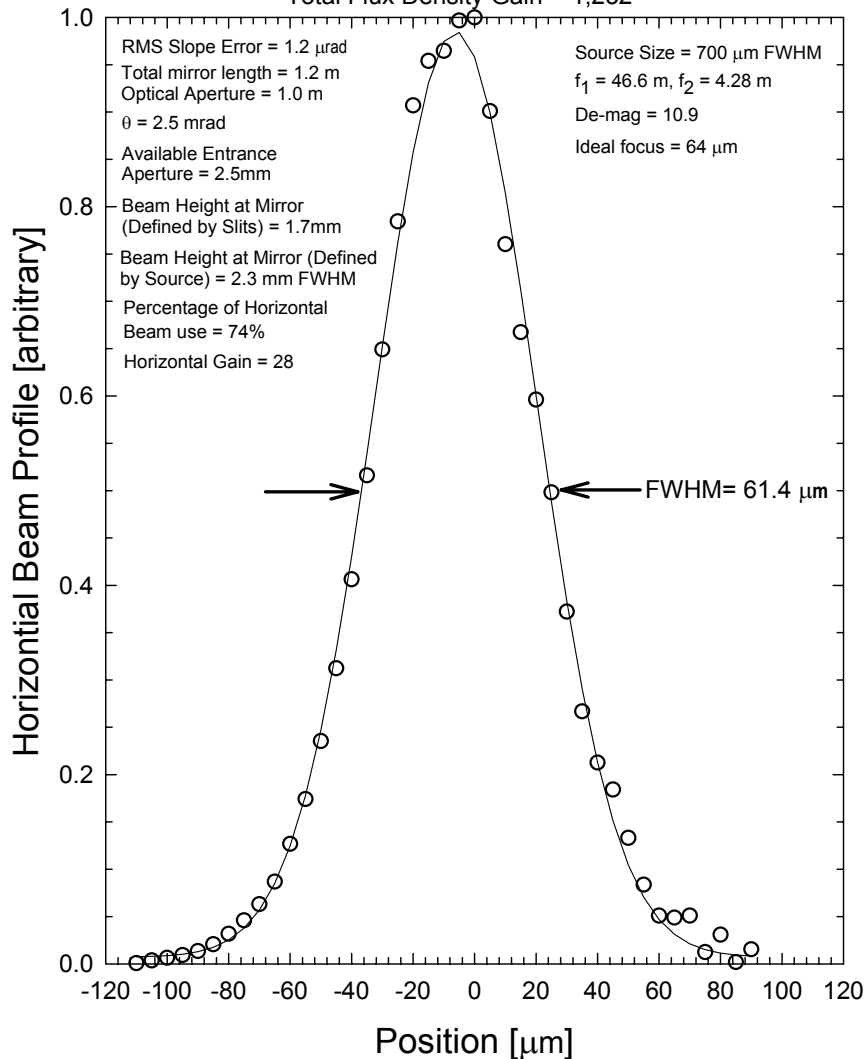
The image was produced by focusing the beam onto a thin YAG single crystal producing visible light that is imaged with a 20X objective coupled to 1k x 1k cooled CCD camera.

The effective resolution is about $3 \mu\text{m}$.



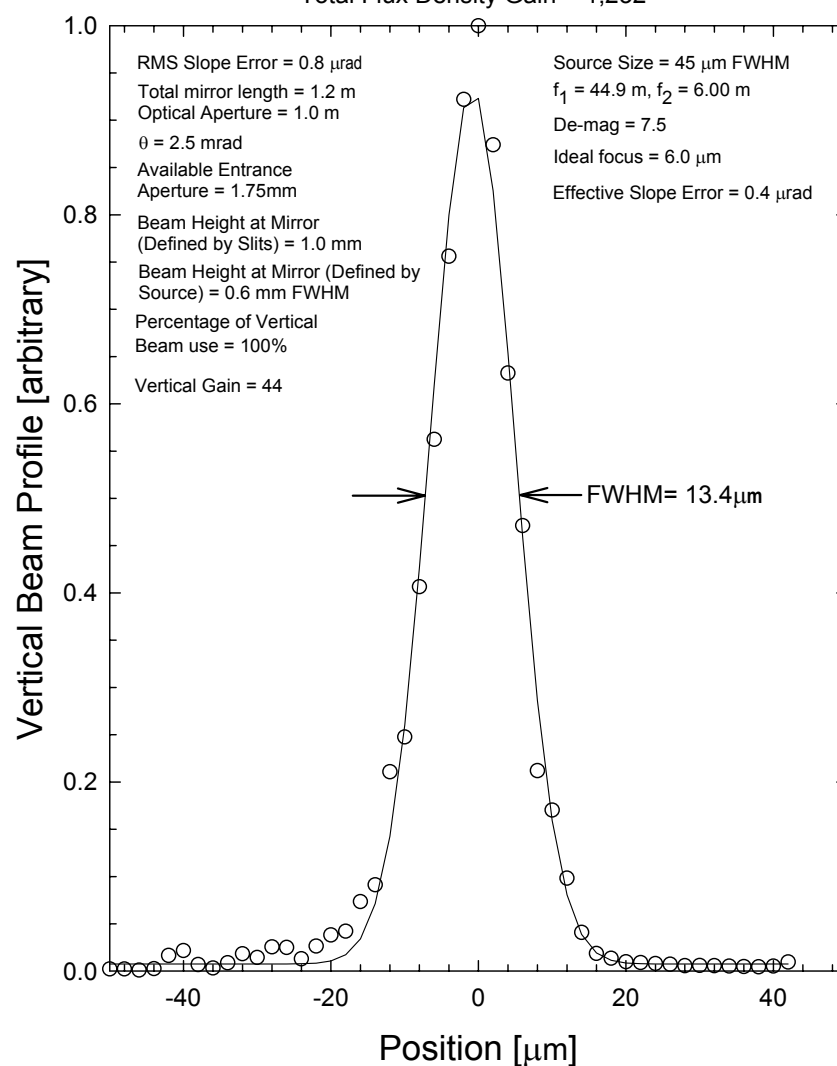
GSECARS Double Focused 12.7 keV
Undulator "A" Beam

Total Flux Density Gain = 1,232



GSECARS Double Focused 12.7 keV
Undulator "A" Beam

Total Flux Density Gain = 1,232



- **Paul Murray**
- **Clayton Pullins**
- **Patrick Dell**
- **Leo Gubenko**
- **Mike Jagger**
- **Jim Ciston**
- **Mathew Newville**
- **Mark L. Rivers**
- **Steve Sutton**
- **Yifei Jaski**

