



High Resolution Crystal Optics

For Inelastic X-ray Scattering

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Background

Experience based on both BL35XU & BL43LXU at SPring-8

BL35XU

- meV non-resonant IXS
- Operating beamline for IXS
 - Design & commissioning 2000 -

BL43LXU

- New non-resonant IXS beamline for meV and 10 meV Commissioning

- *BL43 overview > Friday talk by A. Baron*

Contents

- ① Progress for High-Resolution analyzers
- ② Improving resolution with a T gradient
- ③ Plans for 10 meV (Medium-Resolution) analyzers
- ④ Time Permitting: Mirror Performance

RIKEN Quantum Nano Dynamics Beamline

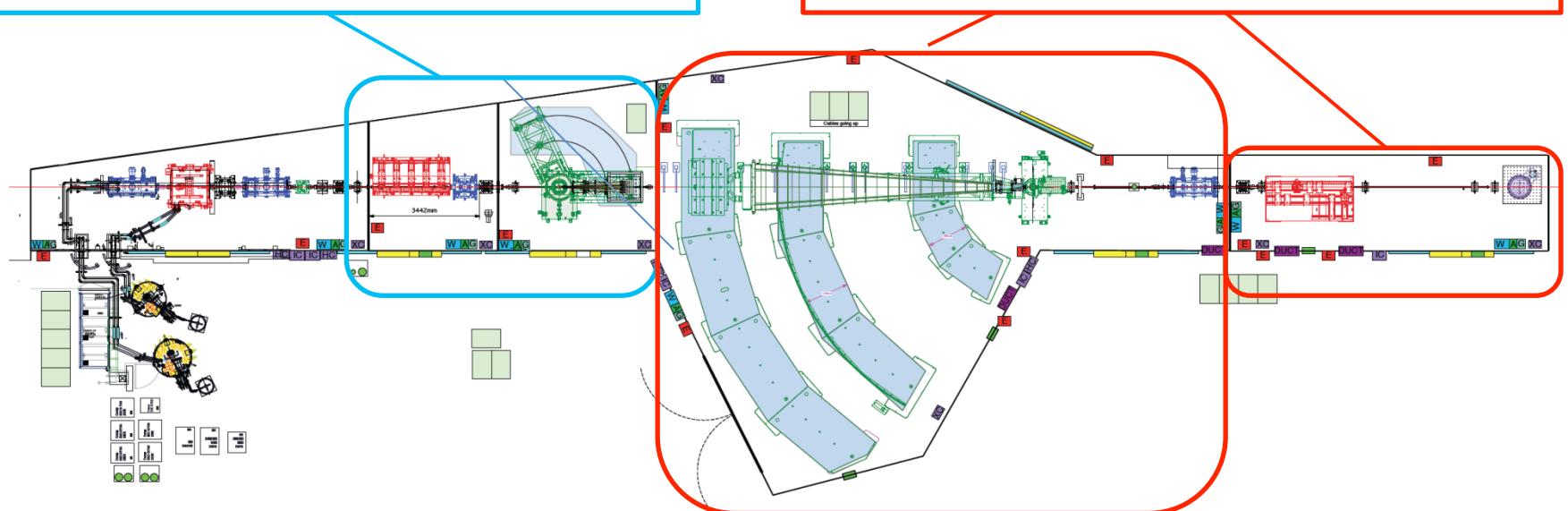
Non-Resonant Inelastic X-ray Scattering Beamline

Medium Resolution (MR) IXS

- Electronic excitation
- $\Delta E = 10 - 40$ meV
- $E - E_0 < 100$ eV
- $R = 1900$

High Resolution (HR) IXS

- Phonon (Electronic excitation)
- $\Delta E = 0.6 - 6.0$ meV
- $E - E_0 < 3$ eV
- $R = 9800$

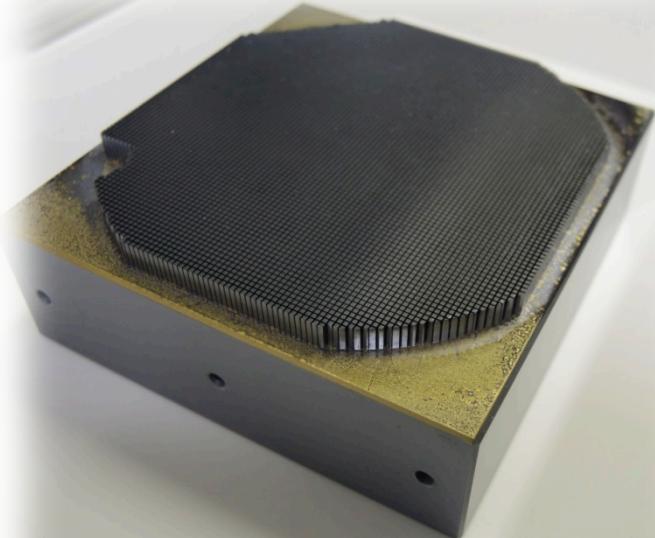




① HR analyzers

High-Resolution IXS

42 analyzer array



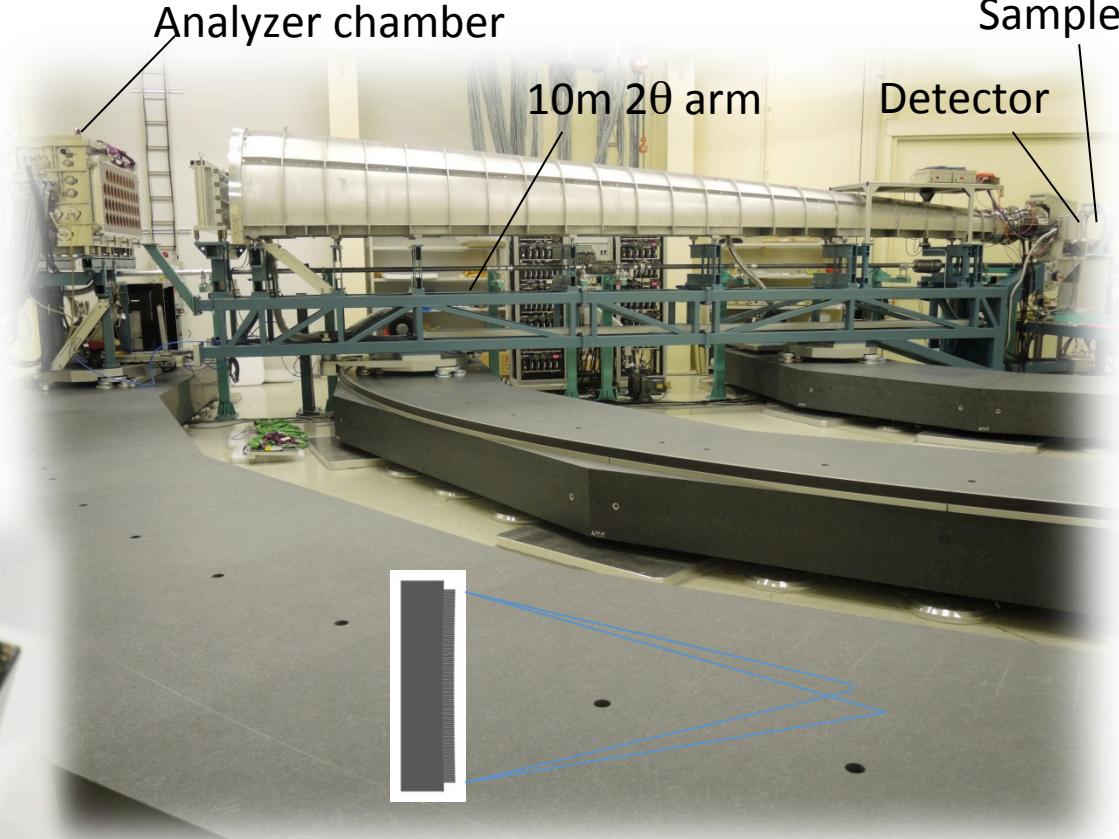
R9800 Analyzer

Analyzer chamber

10m 2θ arm

Sample

Detector



Arm 10 m

$\Delta E = 0.6\text{-}6 \text{ meV}$, $E = 15.8\text{-}25.7 \text{ keV}$

$E - E_0 < 3 \text{ eV}$, $Q < 15 \text{ \AA}^{-1}$

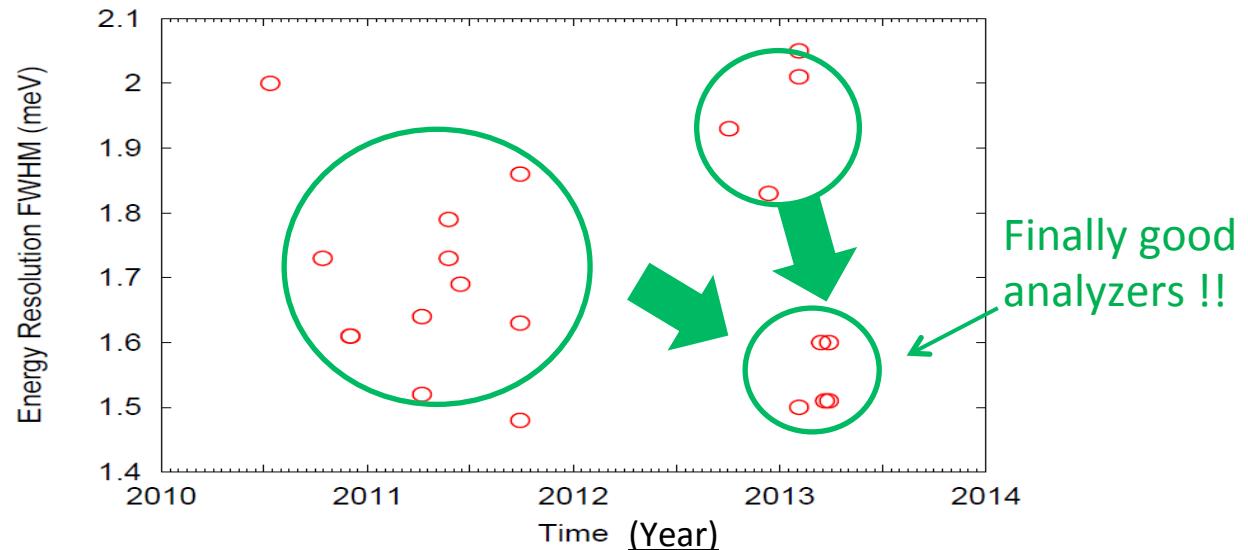
Phonon (Electronic excitation)

HR-Analyzers (R9800)

- NEC fabricated BL35XU analyzers, but they declined to make analyzers for BL43LXU
 - Technology Transfer from NEC to a new company (SARTONWORKS)
 - SARTONWORKS started from 2010 but first attempts failed.
Learning Needed.

Issues

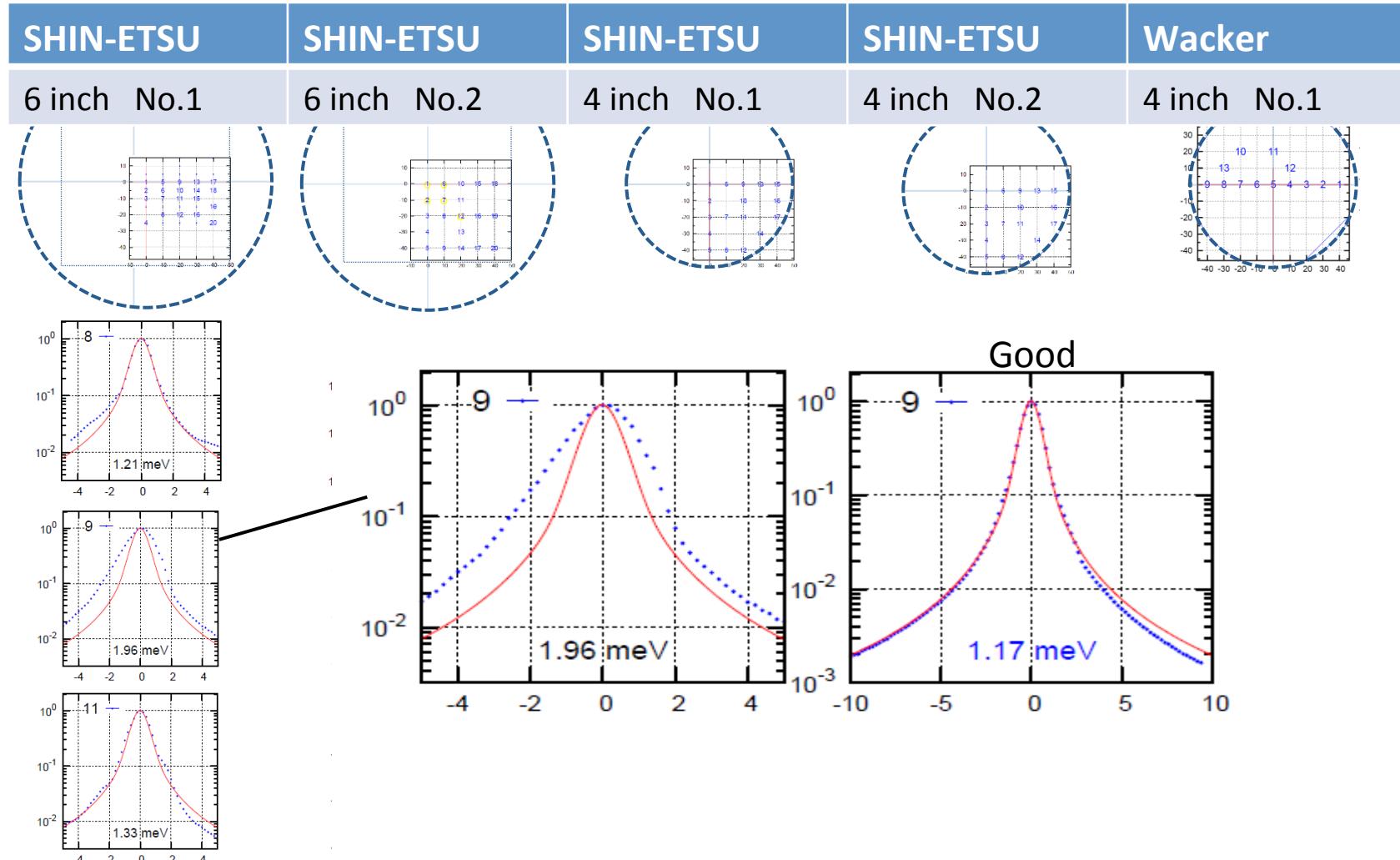
- Silicon Quality
 - Polishing
 - Etching (fast etching → slow etching)
 - Bonding



Silicon Quality Check

- Single crystal : $\phi 6'$, $\phi 4'$ FZ<111> INGOT
- SHIN-ETSU 6 inch ingot had a bad quality !

Silicon Ingots
made by SHI-ETSU HANDOTAI COMPANY. LTD.,
SilChem/Wacker Chemie AG



Some Bad Spots

Silicon Quality Check

SHIN-ETSU	SHIN-ETSU	SHIN-ETSU	SHIN-ETSU	Wacker
6 inch No.1	6 inch No.2	4 inch No.1	4 inch No.2	4 inch No.1

- First 6" Silicon -> Check the ends -> OK
- Problems: Check leftover -> Some bad points
- Another 6" Ingot: OK
- Went to 4" Wafers -> as all OK
- 2013: Return to known good 6" wafer

Expect Main Issue Probably polishing.

Issue with Initial Silicon Polish

- Company had some experience doing strain-free polishing.
- However, some local bad performance of other crystals -> Investigation

Silicon after a light etch



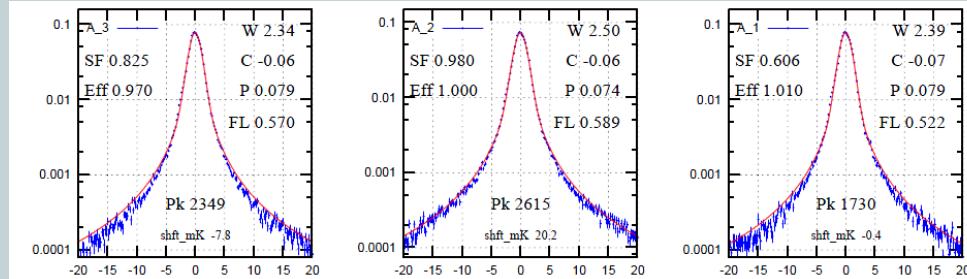
Polished Surface

Back

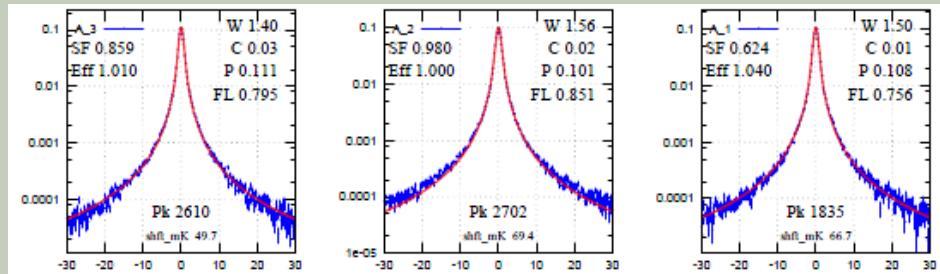
Mechanical = with abrasive powder

MCP = Mechano-Chemical Polishing (No abrasive powder)

Old: Etch & Mechanical & Some MCP



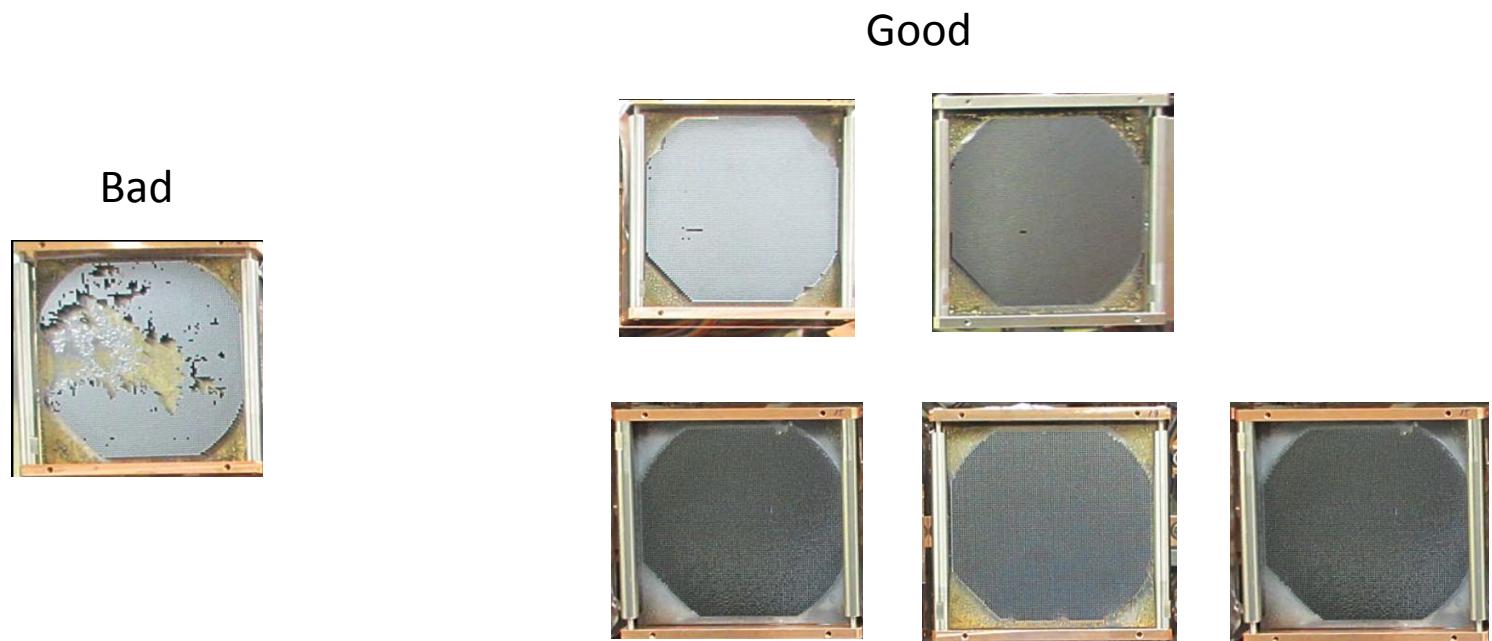
New: Etch & MCP (100um)



Now in progress: sufficiently flat MCP-> Now <6 urad rms

Bonding

- High Temperature Gold diffusion bond
(not SARTONWORKS)
- Not always stable
- Process variation. Not understood. About 1 in 5 analyzers fails.



Present status

- NEC. Delivered 6 crystals in 2013
 - 4 are 1.6 meV or better and good efficiency
 - 1 poor (1.6 meV and low reflectivity)
 - 1 Failed due to bonding -> replaced with reasonable crystal (1.5 meV)

- SARTONWORKS relatively reliable after learning period.
Note: very high transparency compared to NEC.

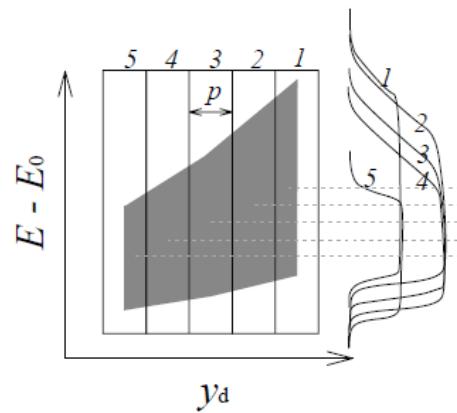
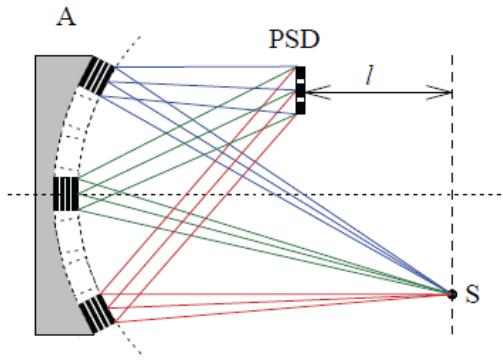


② Temperature-Gradient

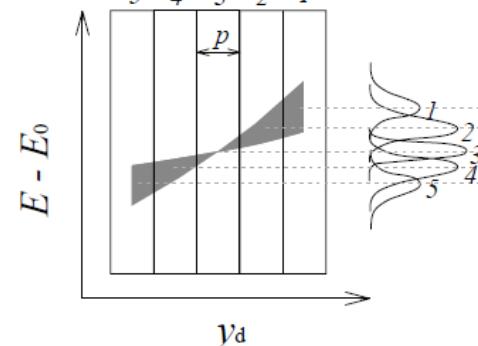
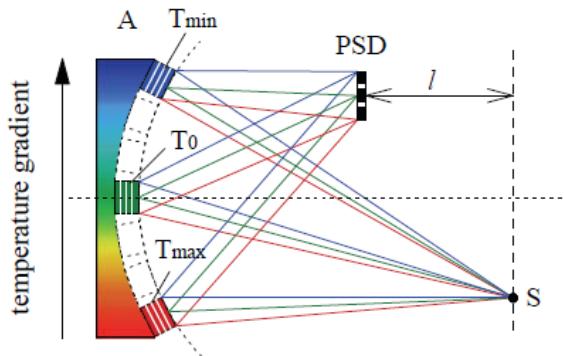
IXS Analyzer Geometries

Energy-Position Correlation

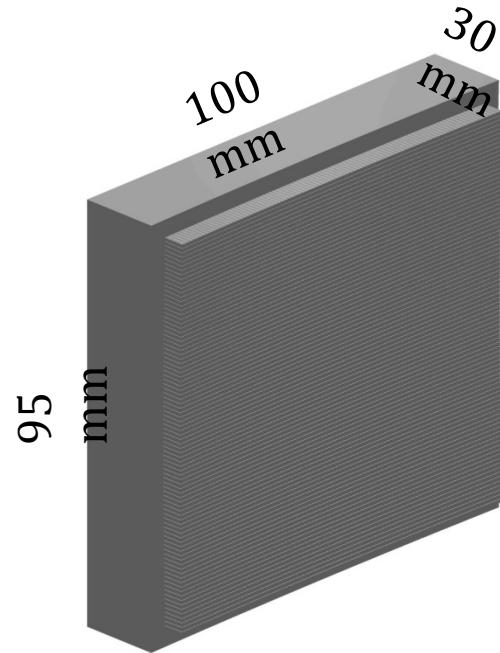
(a) Uniform Temperature of the Analyzer



(b) Temperature Gradient of the Analyzer



- T-gradient Idea -> mostly aimed at small radius 10 meV resolution but works large radius 1 meV resolution
- To obtain large sample area, detector must be moved away from sample
- Deviation from Rowland-condition causes chromatic aberration (demagnification contribution)
- T-gradient can correct Bragg angle of each crystallites and compensate energy-position correlation close to linear



$$Q = \lambda \cdot \Delta T \cdot S / l$$

- Q : Conductive *heat transfer*
- λ : *Thermal Conductivity*
- S : Heat transfer area
- l : *Heat transfer distance*
- ΔT : Temperature offset

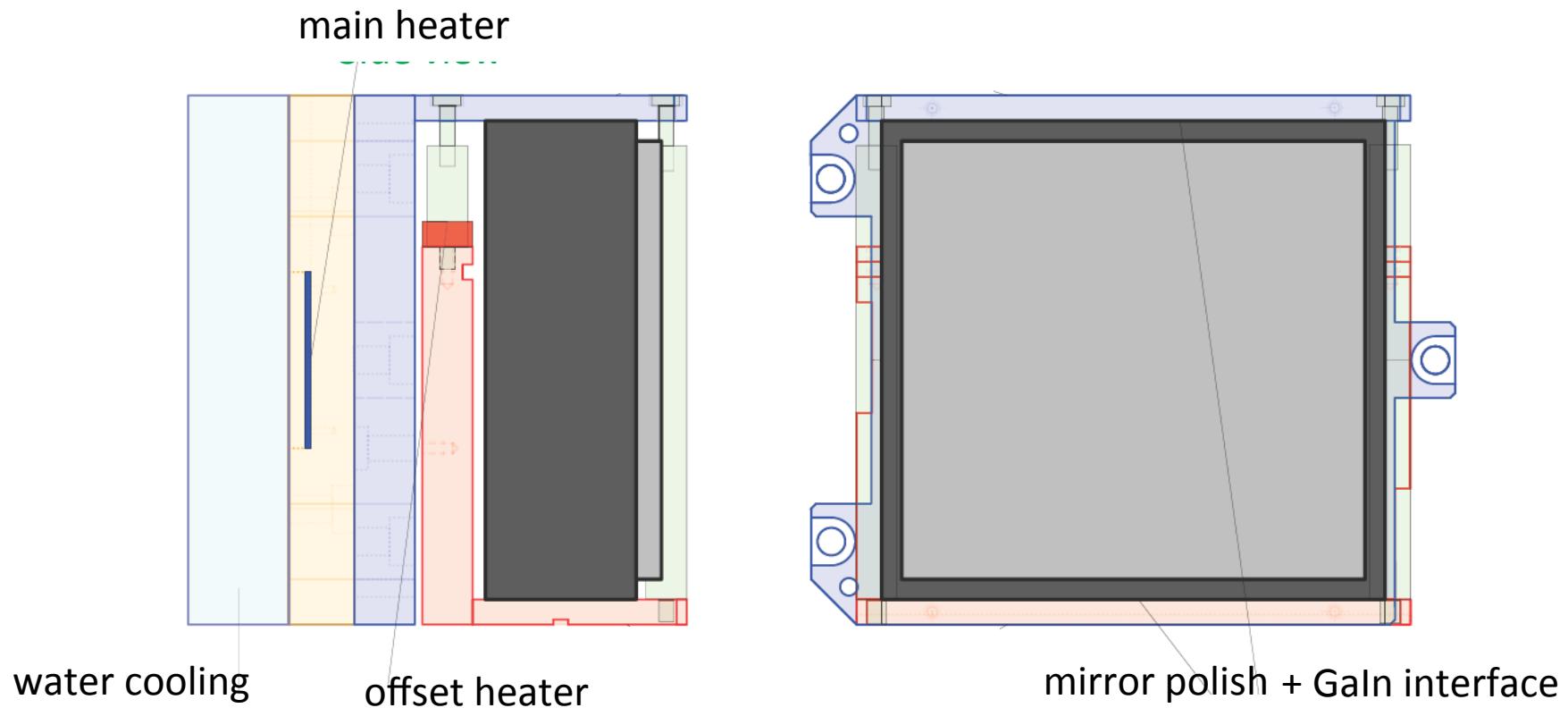
- One-dimensional temperature gradient
- Temperature offset $\Delta T = \sim 10 \text{ mK}$
- Required power $Q = \sim 50 \text{ mW}$

		Silicon
λ	[W/m·K]	148
S	[mm ²]	30 x 100
l	[mm]	95
ΔT	[mK]	10
R	[Ω]	50
V	[V]	1.5
Q	[W]	0.047

Analyzer Holder (thermal circuit)

➡ Heat flow

Temperature gradient

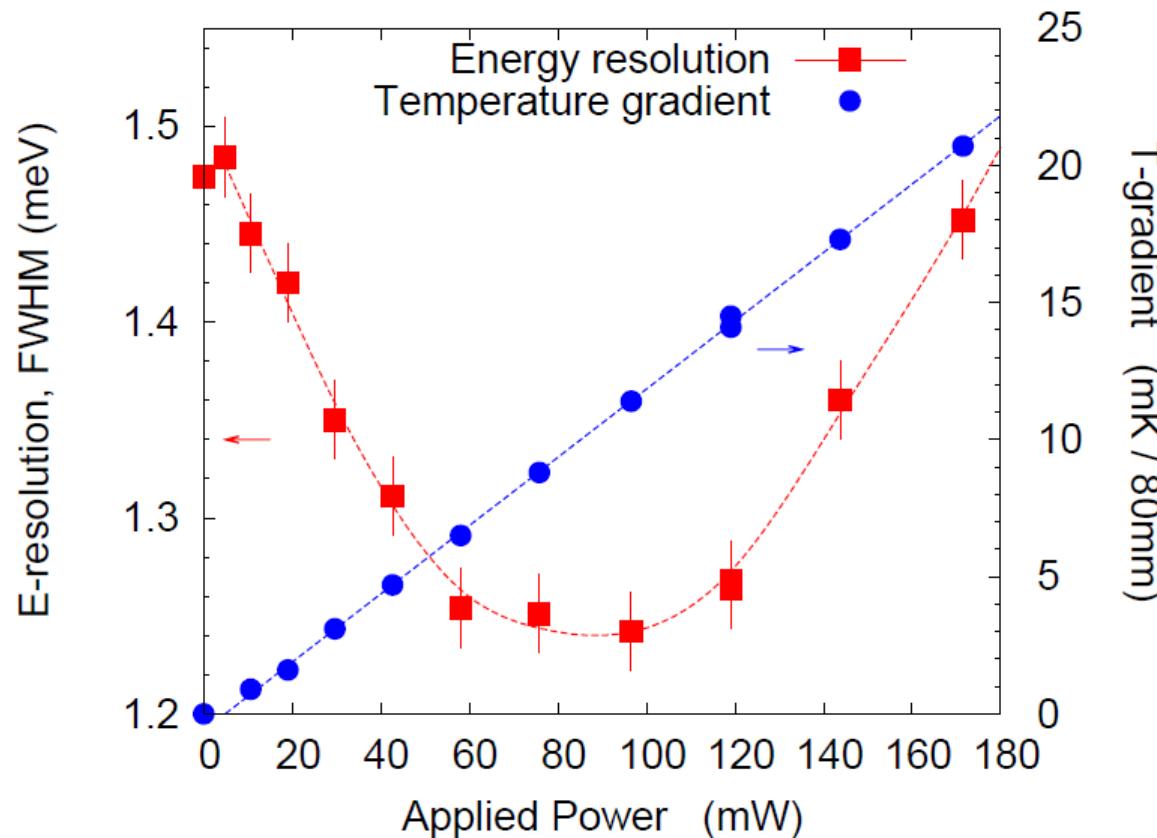


- Both uniform temperature and T-gradient are possible.
- Thermal circuit to do it practically
- After equilibrium state, temperature of each vertical position is fixed and stabilized

T-gradient Application

For High-Resolution Analyzer

- T-gradient can be applied proportionally to applied power
- Resolution has minimum
- Resolution improved from 1.5 to 1.25 meV <Si(11 11 11) reflection>
- For higher-order reflection T-gradient will be more important



③ Plans for MR analyzers

MR-IXS Spectrometer

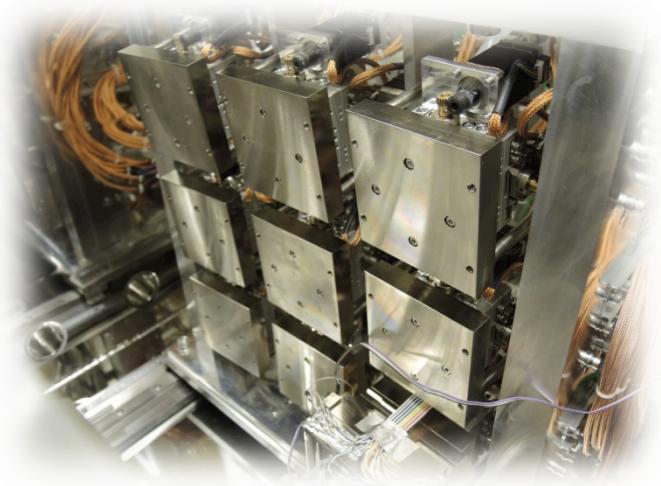
commissioning



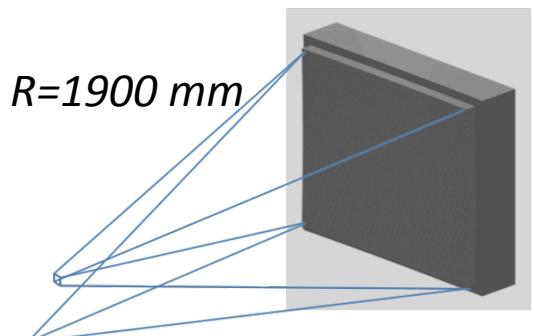
2 m - 2θ arm

$\Delta E = 10 \text{ meV}$, $E = 15.8 \text{ keV}$
 $E - E_0 < 100 \text{ eV}$, $Q < 15 \text{ \AA}^{-1}$

Electronic excitation

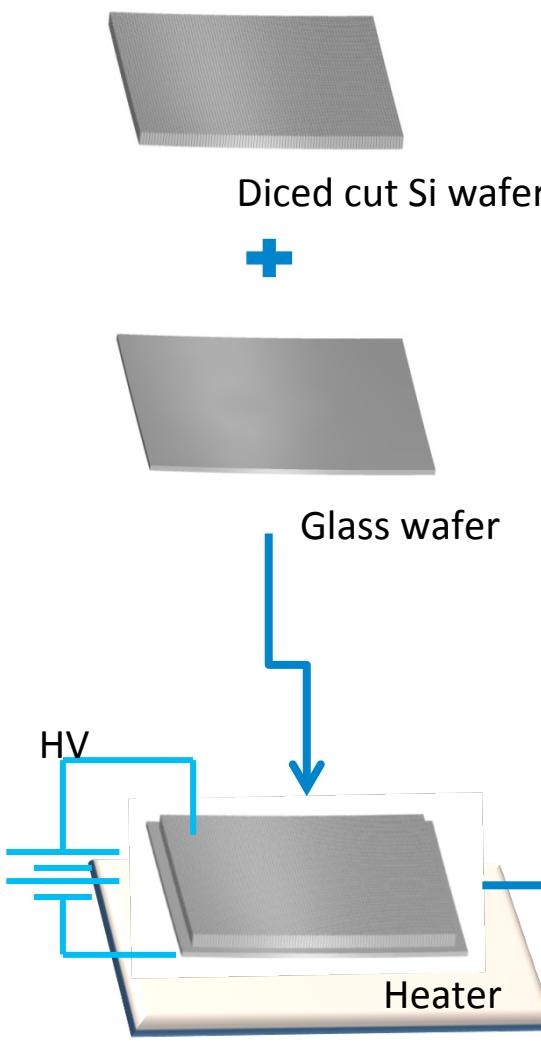


3 x 3 Analyzer array



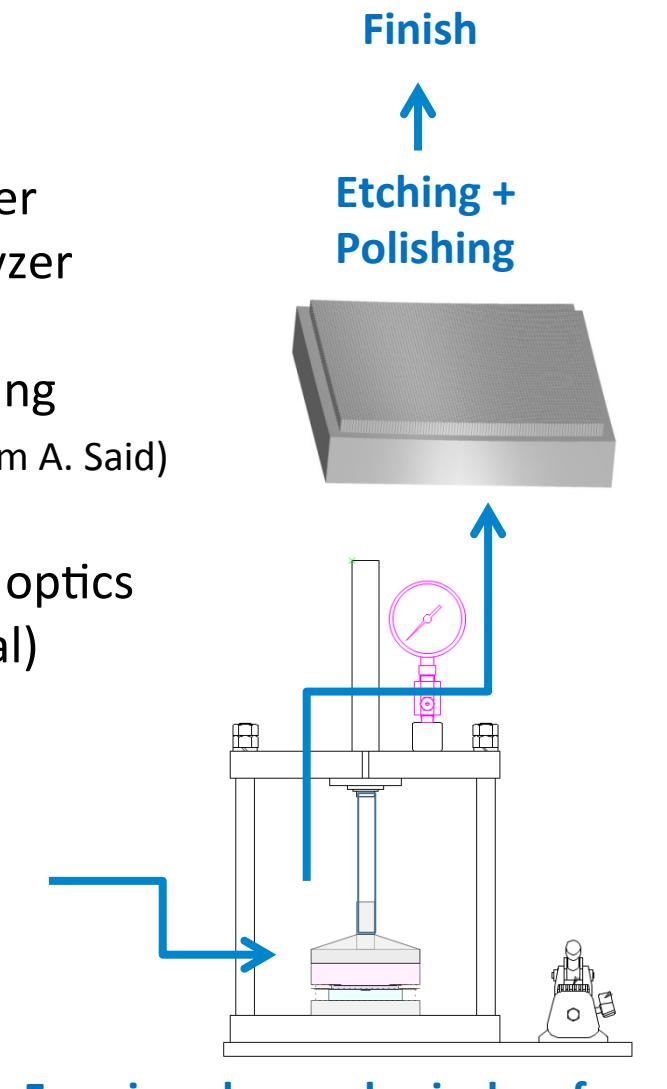
■ Under Development

Plans for MR-IXS analyzers

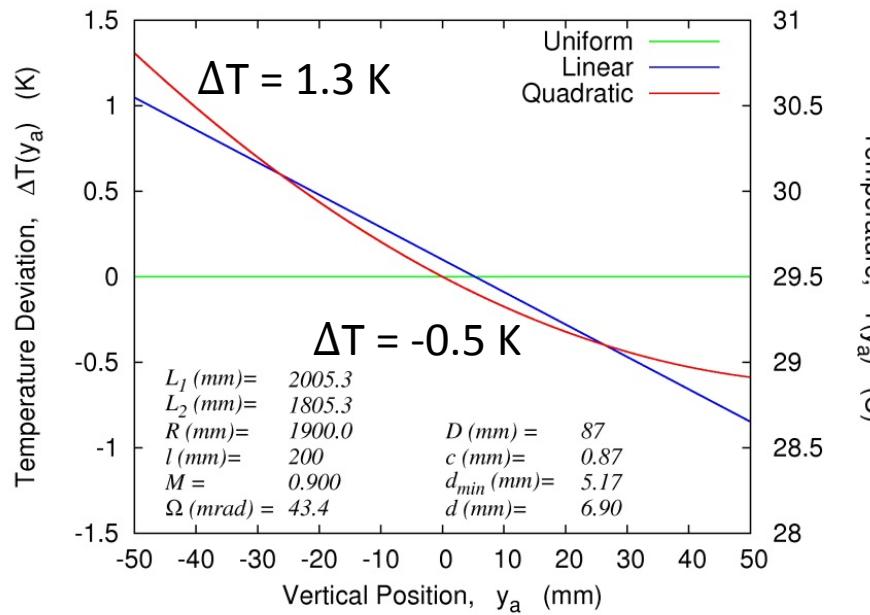


- SARTONWORKS failed
- **Move work in-house** after difficulties with HR-Analyzer
- **Anodic bonding:** Acquiring pieces to do it. (Advice from A. Said)
- Collaboration with JASRI optics group (Ohashi, Goto, et al)

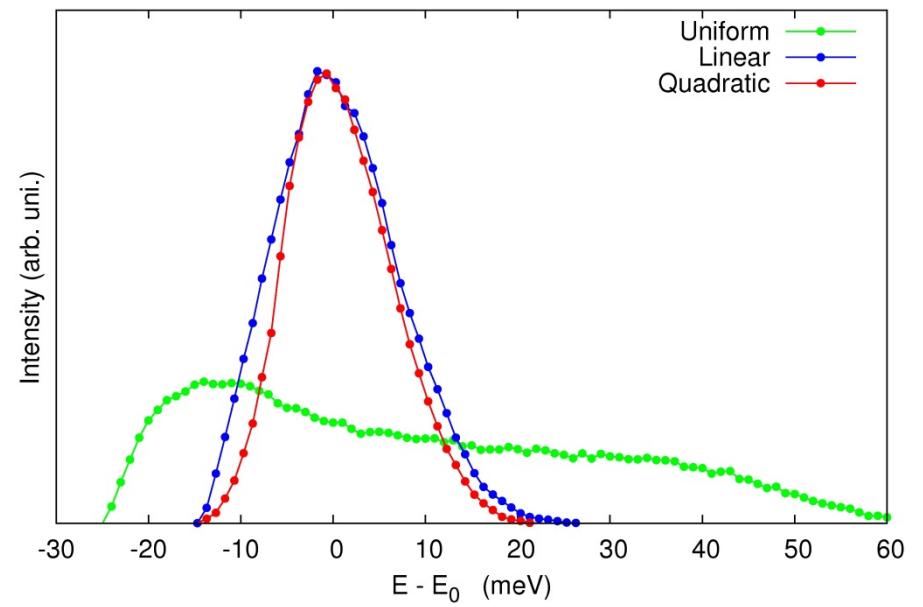
Spherical Analyzer substrate
Invar ($R=1900$)



Temperature Gradient

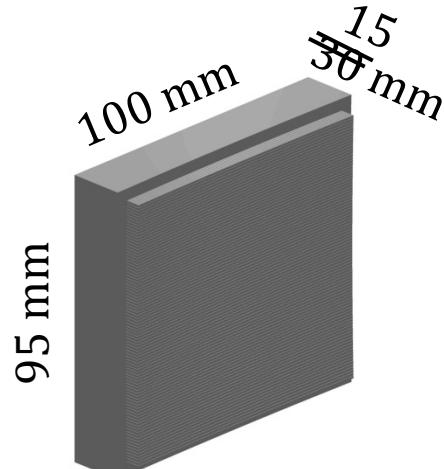


Resolution Function



- Uniform Temperature cannot obtain good energy resolution
- Linear T-gradient reduce energy resolution
- Quadratic T-gradient go to minimum and symmetric line-shape.

MR-IXS Analyzer Substrate



$$Q = \lambda \cdot \Delta T \cdot S / l$$

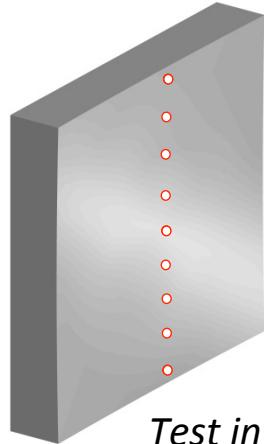
- Q : Conductive *heat transfer*
- λ : *Thermal Conductivity*
- S : Heat transfer area
- l : *Heat transfer distance*
- ΔT : Temperature offset

- $\Delta T = 1 \sim 6 \text{ K}$ (much higher than HR case)
- **Silicon substrate requires high power** to apply large T-gradient
- High power operation needs much cooling and may cause instability of temperature
- **Low thermal conductive material is needed**

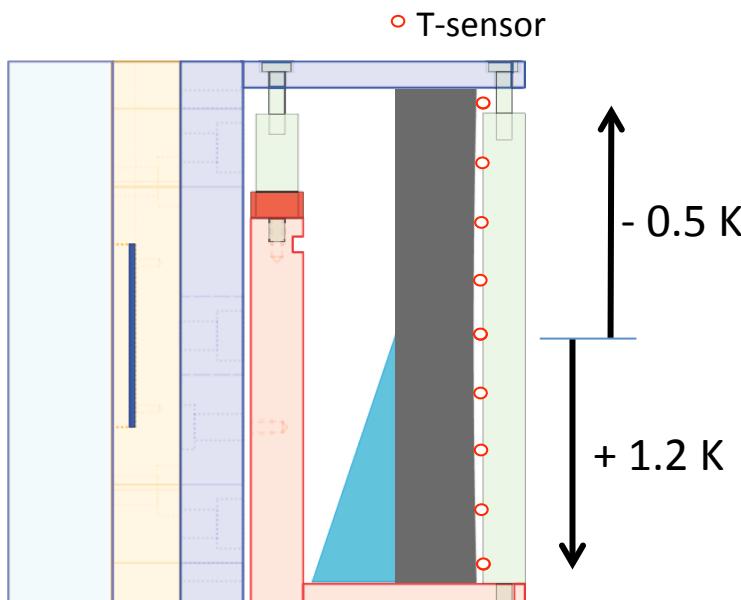
		Silicon	Invar
λ	[W/m·K]	148	13.4
S	[mm ²]	30 x 100	15 x 100
l	[mm]	95	95
ΔT	[K]	2	2
R	[Ω]	50	50
V	[V]	21	< 1/20 6
Q	[W]	9.3	→ 0.42

MR-IXS Analyzer T-control

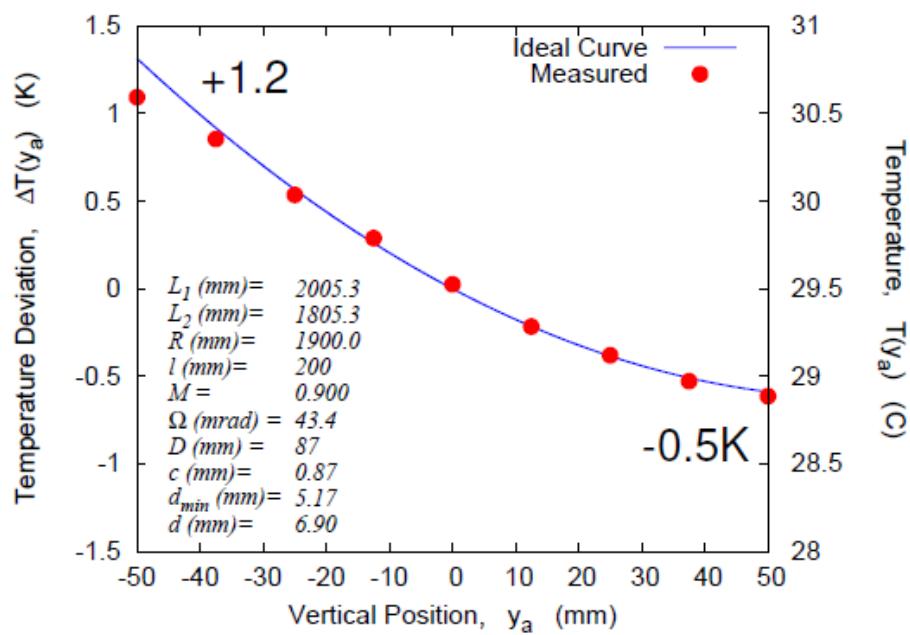
Off-Line test : linear and non-linear T-gradient



Test invar substrate
106 x 106 x 15 mm

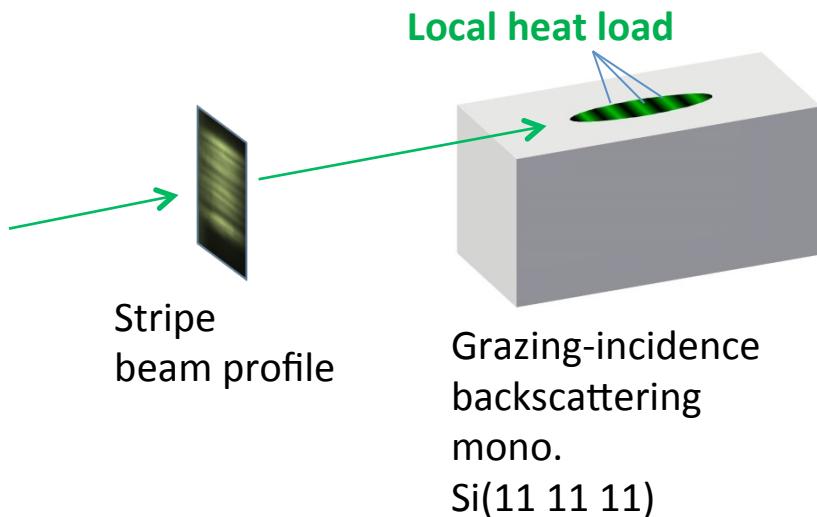
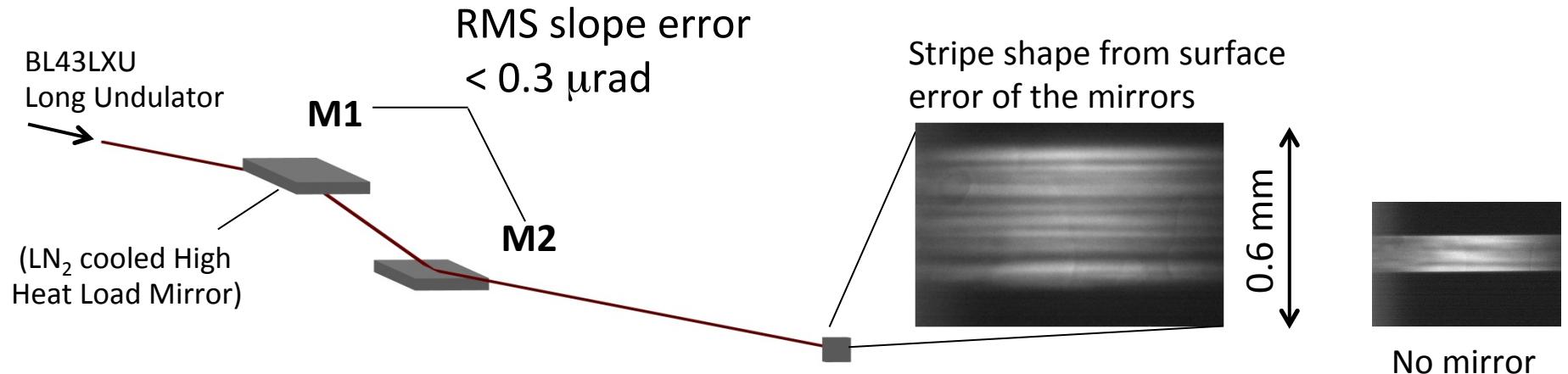


- Linear T-gradient $\Delta T = 1 \sim 6 \text{ K} / 100 \text{ mm}$ is possible
- In reality, quadratic T-gradient is more desirable.
- Non-linear T-gradient can be controlled by changing thermal flow rate



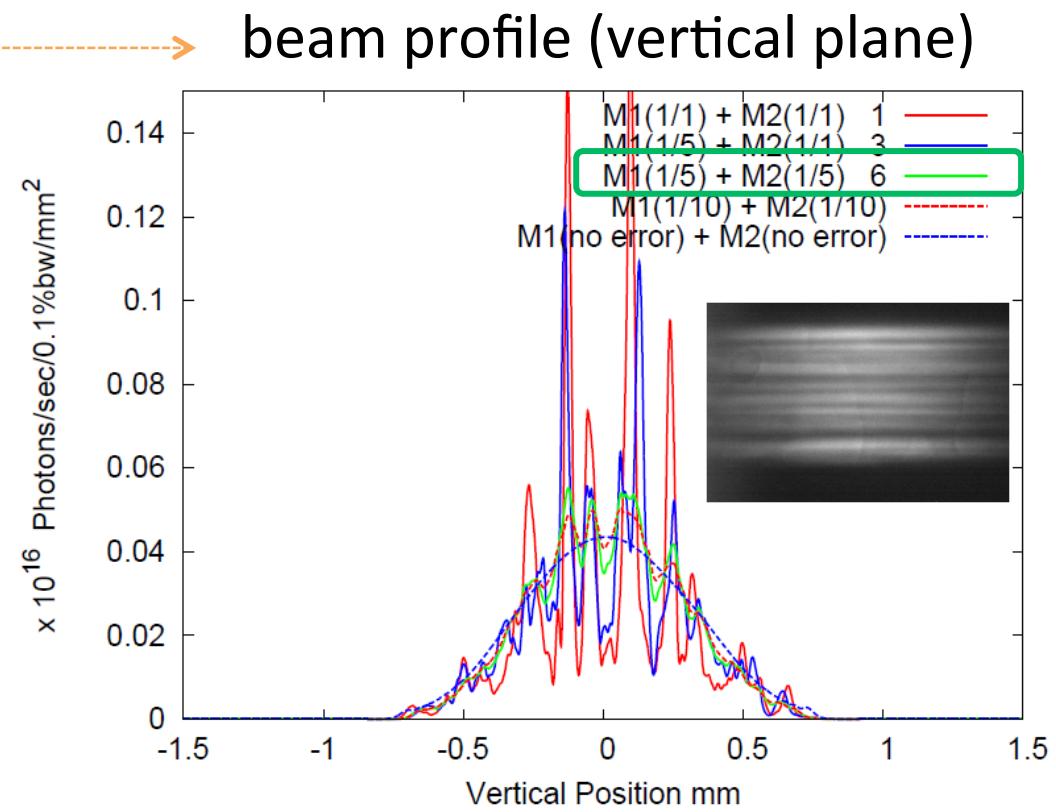
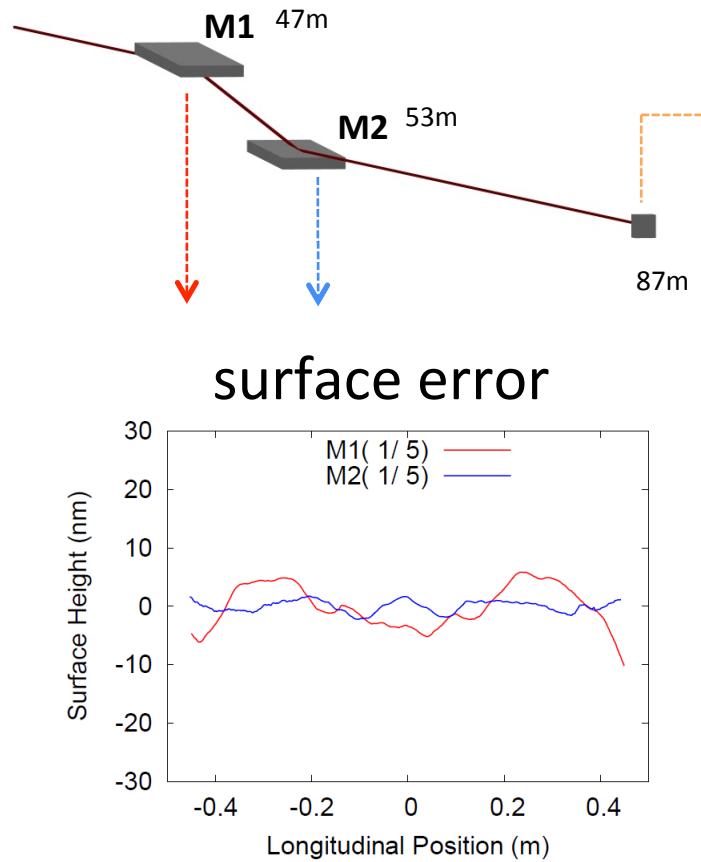
④ Heat Load from Mirrors

Heat Load from Mirrors



- For collimating mirrors, surface error is more severe than focusing mirror
- **Local heat load** makes resolution **worse !!**
 $1.5 \text{ meV} \rightarrow 1.7 - 3 \text{ meV (FWHM)}$
- To reduce heat load onto downstream optics (Backscatt. Mono.) grazing incidence is used, but it is not enough
- **Additional mirror polishing is needed**

- How much must I polish present mirrors ?
- Calculations by SRW were performed
- Both mirror must be polished



Used by SRW, Tchoubar, Oleg, Simulating emission and propagation of partially-coherent undulator radiation

Summary

BL43LXU High-Resolution Crystal Optics

- Present status of HR-Analyzer (R9800)
- Concept of T-gradient optics and it's application
- Plans of MR-Analyzer (R1900)
- Heat load on high-resolution monochromators coming from collimating mirrors

Collaborators

BL43LXU (RIKEN Quantum Nano Dynamics Beamline)

■ BL Commissioning

Materials Dynamics Laboratory, RIKEN SPring-8 Center

A. Q. R. Baron, H. Uchiyama

■ MR-Analyzer in-house fabrication

JASRI optics group

(H. Ohashi, S. Goto, H. Yamazaki, Y. Shimizu, T. Miura)

■ Mirror performance

JASRI optics group

(H. Ohashi, H. Yamazaki, Y. Senba)



Thank you for your attention.